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# Surface Plasmon Resonance-Based Silicon Dual-Core Photonic Crystal Fiber Polarization Beam Splitter at Mid-Infrared Spectral Region

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**Abstract:** In this paper, a novel silicon dual-core photonic crystal fiber (Si-DC-PCF) polarization beam splitter (PBS) based on surface plasmon resonance effect is proposed. The mode coupling characteristics between the X and Y-polarized even and odd modes and surface plasmon polariton mode are analyzed by using the finite element method and coupled-mode theory. The influences of the structure parameters of the Si-DC-PCF on the coupling length and coupling length ratio are investigated. The normalized output power of the X and Y-polarized modes in the cores A and B and the corresponding extinction ratio are also discussed. By optimizing the structure parameters of the Si-DC-PCF, the PBS length of 192  $\mu\text{m}$  and bandwidth of 830 and 730 nm in the cores A and B are achieved. It is believed that the proposed Si-DC-PCF PBS can find important applications in the mid-infrared laser and sensing systems.

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## 1. Introduction

Polarization beam splitter (PBS) is an important device in optical systems [1-5]. It can separate two beams of orthogonal polarized light into two different propagation paths [6], and have important applications in the fields of fiber laser, optical communication, and sensing [7-11]. With the development of the photonic crystal fiber (PCF), many researchers have focused on the PBS based on the dual-core PCF (DC-PCF) [12-16]. In 2010, Chiang et al. reported a DC-PCF PBS, whose fiber length and extinction ratio were 0.3 mm and 23 dB at wavelength 1.55  $\mu\text{m}$ , respectively [17]. In 2014, Jiang et al. proposed a novel DC-PCF PBS, whose fiber length was 119.1  $\mu\text{m}$  and bandwidth was 249 nm [18].

In recent years, the surface plasmon resonance (SPR) technology has gradually been becoming maturity [19-23]. Many investigations on the combination of the PCF and SPR effect for the optical devices have been reported [24-28]. Until now, researchers have designed some DC-PCF PBSs based on the mode coupling between the core mode of the DC-PCF and surface plasmon polariton (SPP) mode [29-33]. In 2019, Rahman et al. demonstrated a kind of DC-PCF PBS with the gold wire filled in the air hole, where the fiber length was only 56.33  $\mu\text{m}$  and bandwidth was up to 530 nm [34]. In 2019, Zhao et al. investigated a SPR-based DC-PCF PBS with the double elliptical air holes, where the fiber length was 104  $\mu\text{m}$  and bandwidth was up to 575 nm [35]. In the previous works, because the substrate materials of the DC-PCF PBS are the silica, the PBS can only be used in the

near-infrared optical systems. As the mid-infrared optics and photonics are developed, the fiber devices which are operated in the mid-infrared spectral region have been attracting great interest [36-40]. In 2018, Maes et al. designed a heavily doped holmium fluoride fiber laser which works at wavelength 3.92  $\mu\text{m}$  [41]. In 2020, we proposed a silicon PCF polarization filter with a bandwidth of 2.75 to 7.80  $\mu\text{m}$  [42]. Up to now, the research on the mid-infrared silicon DC-PCF (Si-DC-PCF) PBS has not been reported.

In this paper, we propose a novel Si-DC-PCF PBS based on the mode coupling theory and SPR effect. The coupling length in the X-polarized (X-pol) and Y-polarized (Y-pol) directions and the corresponding coupling length ratio are analyzed, and the normalized output power and extinction ratio of the cores A and B are also discussed. The PBS length of 192  $\mu\text{m}$  and bandwidth of 830 and 730 nm in the cores A and B are achieved.

## 2. Design of the Si-DC-PCF PBS

The cross-section structure and schematic diagram of the practical application in the optical system of the designed Si-DC-PCF PBS are shown in Figs. 1(a) and 1(b), respectively. From Fig. 1(a), the background material of the Si-DC-PCF is the pure silicon. The Si-DC-PCF is missing the two air holes in the X direction to form the cores A and B. The Si-DC-PCF includes four kinds of air holes with the different sizes. The diameter of the air hole between the cores A and B is  $d_1$ , and the gold film with a thickness of  $t$  is coated in this air hole. The diameter of the two small air holes on the left side of the core A and the right side of the core B is  $d_2$ . The diameter of the eight air holes above and below the cores A and B is  $d_3$ . The diameter of the other air holes is  $d_4$ , and the hole-to-hole pitch is  $\Lambda$ . The finite element method (FEM) is used. A perfect matching layer (PML) is set at the outermost layer of the designed Si-DC-PCF to absorb the radiation energy, and the refractive index of the PML is 0.03 higher than that of the pure silicon [43]. From Fig. 1(b), after passing through the designed Si-DC-PCF PBS, the orthogonal polarized light emitted from the light source is completely separated into the two beams of polarized light. The two beams of polarized light can be launched into the different optical systems, such as laser and sensor systems.

The material dispersion of the pure silicon is described by the Sellmeier equation [44]

$$n_{\text{Si}}(\lambda) = \varepsilon + \frac{A}{\lambda^2} + \frac{B\lambda_1^2}{\lambda^2 - \lambda_1^2}, \quad (1)$$

where  $\lambda_1=1.1071 \mu\text{m}$ ,  $\varepsilon=11.6858$ ,  $A=0.939816 \mu\text{m}^2$ , and  $B=8.10461 \times 10^{-3}$ .

The relative dielectric constant of the gold film can be described by the Drude-Lorentz model [45]

$$\varepsilon_m = \varepsilon_\infty - \frac{\omega_D^2}{\omega(\omega - j\gamma_D)} - \frac{\Delta\varepsilon \cdot \Omega_L^2}{(\omega^2 - \Omega_L^2) - j\Gamma_L\omega}, \quad (2)$$

where  $\varepsilon_\infty=5.9673$  and  $\Delta\varepsilon=1.09$  are the high frequency dielectric constant and weighted coefficient, respectively,  $\omega$ ,  $\omega_D$ , and  $\gamma_D$  are the angle frequency of the guided-wave, plasma frequency, and damping frequency, respectively,  $\Omega_L$  represents the frequency of the Lorentz oscillator, and  $\Gamma_L$  represents the bandwidth of the Lorentz oscillator. In this work,  $\omega_D/2\pi=2113.6 \text{ THz}$ ,  $\gamma_D/2\pi=15.92 \text{ THz}$ ,  $\Omega_L/2\pi=650.07 \text{ THz}$ , and  $\Gamma_L/2\pi=104.86 \text{ THz}$ .

The coupling length ( $CL$ ) in the different polarization directions can be calculated by [46]

$$CL_X = \frac{\lambda}{2|(n_{\text{even}}^X - n_{\text{odd}}^X)|}, \quad (3)$$

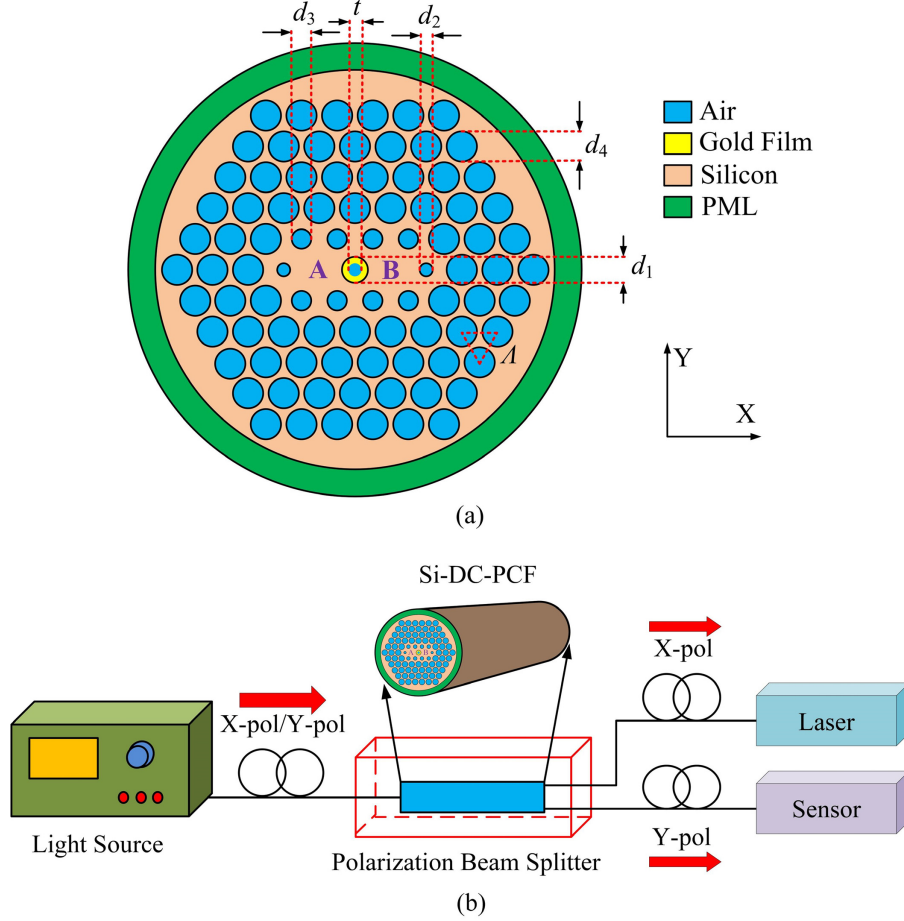
$$CL_Y = \frac{\lambda}{2|(n_{\text{even}}^Y - n_{\text{odd}}^Y)|}, \quad (4)$$

where  $CL_X$  and  $CL_Y$  are the coupling length of the X-pol and Y-pol, respectively,  $\lambda$  is the wavelength of the incident light, and  $n_X$  even,  $n_X$  odd,  $n_Y$  even and  $n_Y$  odd are the effective

refractive indices of the even and odd modes in the X-pol and Y-pol, respectively.  
The coupling length ratio ( $CLR$ ) can be described by [47]

$$CLR = \frac{CL_Y}{CL_X}, \quad (5)$$

When the  $CLR=2$  or  $1/2$ , the polarization splitting length is the optimum value.



**Fig. 1.** (a) The cross-section structure of the designed Si-DC-PCF PBS, and (b) the schematic diagram of the practical application in the optical systems.

The normalized output powers ( $P_{out}$ ) of the X-pol and Y-pol in the cores A and B can be described by [48]

$$P_{out,A}^{X,Y} = P_{in} \cos^2\left(\frac{\pi}{2} \frac{L_p}{CL_{X,Y}}\right), \quad (6)$$

$$P_{out,B}^{X,Y} = P_{in} \sin^2\left(\frac{\pi}{2} \frac{L_p}{CL_{X,Y}}\right), \quad (7)$$

where  $P_{in}$  is the input power and  $L_p$  is the propagation length of the designed Si-DC-PCF.

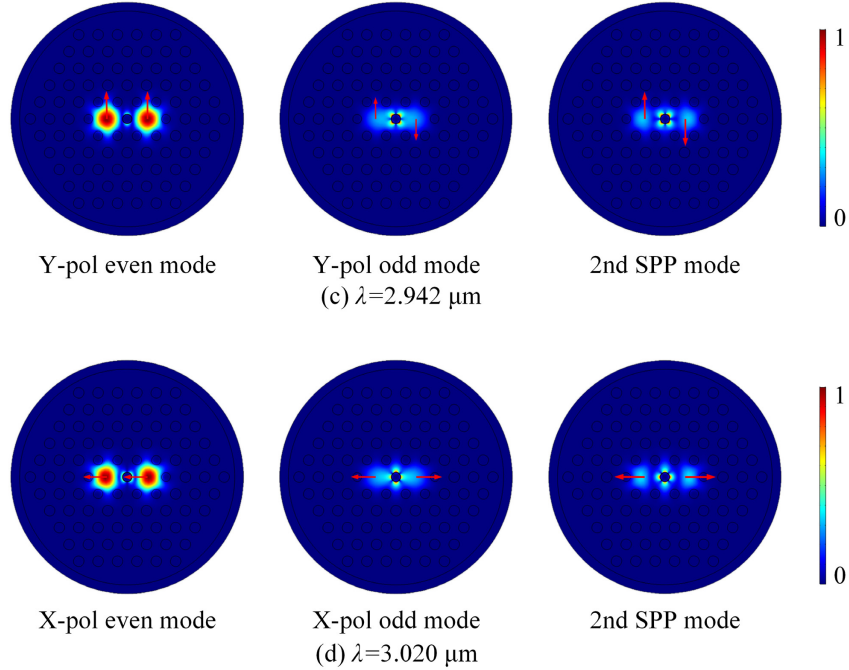
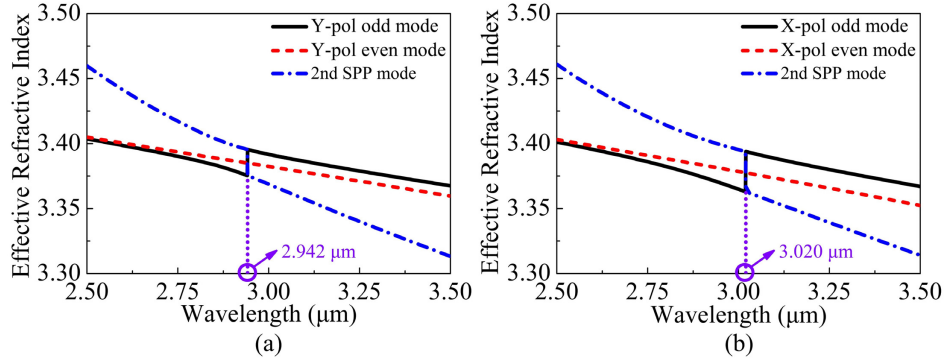
The extinction ratio ( $ER$ ) of the cores A and B as an important parameter to determine the splitter quality can be expressed as [49]

$$ER_A = 10 \log_{10} \frac{P_{out,A}^X}{P_{out,A}^Y}, \quad (8)$$

$$ER_B = 10 \log_{10} \frac{P_{out,B}^Y}{P_{out,B}^X}, \quad (9)$$

The wavelength range with the  $ER$  larger than 20 dB can be considered as the splitting bandwidth of the PBS. Because the cores A and B of the designed Si-DC-PCF have the same structure and symmetry, we only need to consider the change of  $P_{out}$  along the X-pol and Y-pol directions and  $ER$  in the cores A and B when the input light is propagated in the core A at the initial stage.

### 3. Simulation results and discussion

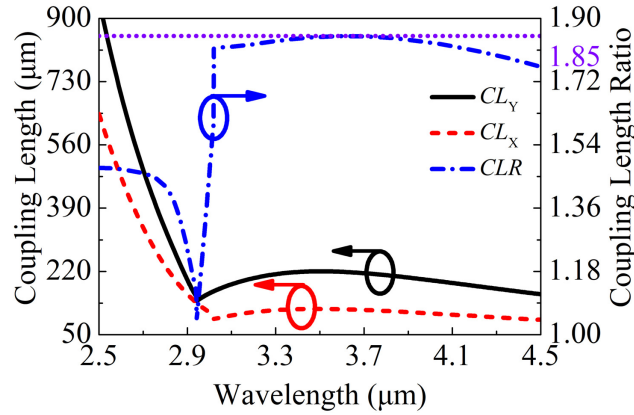


**Fig. 2.** The effective refractive indices of (a) Y-pol and (b) X-pol even and odd modes and 2nd SPP mode, and the mode field distributions of (c) the Y-pol even and odd modes and 2nd SPP mode at wavelength 2.942  $\mu\text{m}$  and (d) the X-pol even and odd modes and 2nd SPP mode at wavelength 3.020  $\mu\text{m}$ .

When the initial structure parameters of the designed Si-DC-PCF are set as  $d_1=1.08 \mu\text{m}$ ,

$d_2=1.00 \mu\text{m}$ ,  $d_3=1.05 \mu\text{m}$ ,  $d_4=1.20 \mu\text{m}$ ,  $A=2.2 \mu\text{m}$ , and  $t=45 \text{ nm}$ , the effective refractive indices of the Y-pol and X-pol even and odd modes and 2nd SPP mode calculated by the FEM are shown in Figs. 2(a) and 2(b), respectively. From Fig. 2(a), the effective refractive indices of the Y-pol odd mode and 2nd SPP mode have a resonant point at wavelength  $2.942 \mu\text{m}$ , while the effective refractive indices of the Y-pol even mode and 2nd SPP mode don't have resonant point. From Fig. 2(b), the effective refractive indices of the X-pol odd mode and 2nd SPP mode have a resonant point at wavelength  $3.020 \mu\text{m}$ , while the effective refractive indices of the X-pol even mode and 2nd SPP mode don't have resonant point. According to the coupled-mode theory [50, 51], the complete coupling between the Y-pol and X-pol odd modes and 2nd SPP mode occur at wavelengths  $2.942$  and  $3.020 \mu\text{m}$ , respectively, while there are no mode coupling between the Y-pol and X-pol even modes and 2nd SPP within the wavelength range considered. The mode field distributions of the Y-pol and X-pol modes and 2nd SPP mode are shown in Figs. 2(c) and 2(d), respectively. From Figs. 2(c) and 2(d), the mode field energy of the Y-pol and X-pol even modes does not change at wavelengths  $2.942$  and  $3.020 \mu\text{m}$ . However, the mode field energy of the Y-pol and X-pol odd modes and 2nd SPP mode occurs to strongly transfer at wavelengths  $2.942$  and  $3.020 \mu\text{m}$ . Therefore, it is further confirmed that the complete coupling between the Y-pol and X-pol odd modes and 2nd SPP mode occur at wavelengths  $2.942$  and  $3.020 \mu\text{m}$ .

The  $CL$  of the Y-pol ( $CL_Y$ ) and X-pol ( $CL_X$ ) and  $CLR$  of the designed Si-DC-PCF are shown in Fig. 3. It can be seen from Fig. 3 that the  $CL_Y$  and  $CL_X$  have mutation inflection points at wavelengths  $2.942$  and  $3.020 \mu\text{m}$ , respectively, which correspond to the resonant points of the effective refractive indices of the Y-pol and X-pol odd modes. This results in the sudden changes of the effective refractive index differences between the Y-pol and X-pol odd and even modes. After wavelengths  $2.942$  and  $3.020 \mu\text{m}$ , the changes of the  $CL_Y$  and  $CL_X$  keep stable as the wavelength increases. After wavelength  $3.020 \mu\text{m}$ , the  $CLR$  remains  $\sim 1.85$  as the wavelength increases. In order to obtain the optimized polarization splitting length ( $CLR=2$ ), we will analyze the influences of the structure parameters of the designed Si-DC-PCF on the  $CL_Y$ ,  $CL_X$ , and  $CLR$ .



**Fig. 3.** The  $CL$  of the Y-pol ( $CL_Y$ ) and X-pol ( $CL_X$ ) and  $CLR$  of the designed Si-DC-PCF.

Figs. 4(a), 4(b), and 4(c) show the relationships between the  $CL_Y$ ,  $CL_X$ , and  $CLR$  and  $d_1$ , respectively. From Figs. 4(a) and 4(b), with the increase of  $d_1$ , the  $CL_Y$  and  $CL_X$  decrease gradually at the shorter wavelength at the same time, but the relative decrease of the  $CL_Y$  is smaller than that of the  $CL_X$ . Moreover, the  $CL_Y$  and  $CL_X$  change less at the longer wavelength, and the mutation inflection point shifts towards the long wavelength. Consequently, with the increase of  $d_1$ , the mutation inflection point of the  $CLR$  shifts towards the long wavelength gradually, and the  $CLR$  after the mutation inflection point increases stably, as shown in Fig. 4(c).

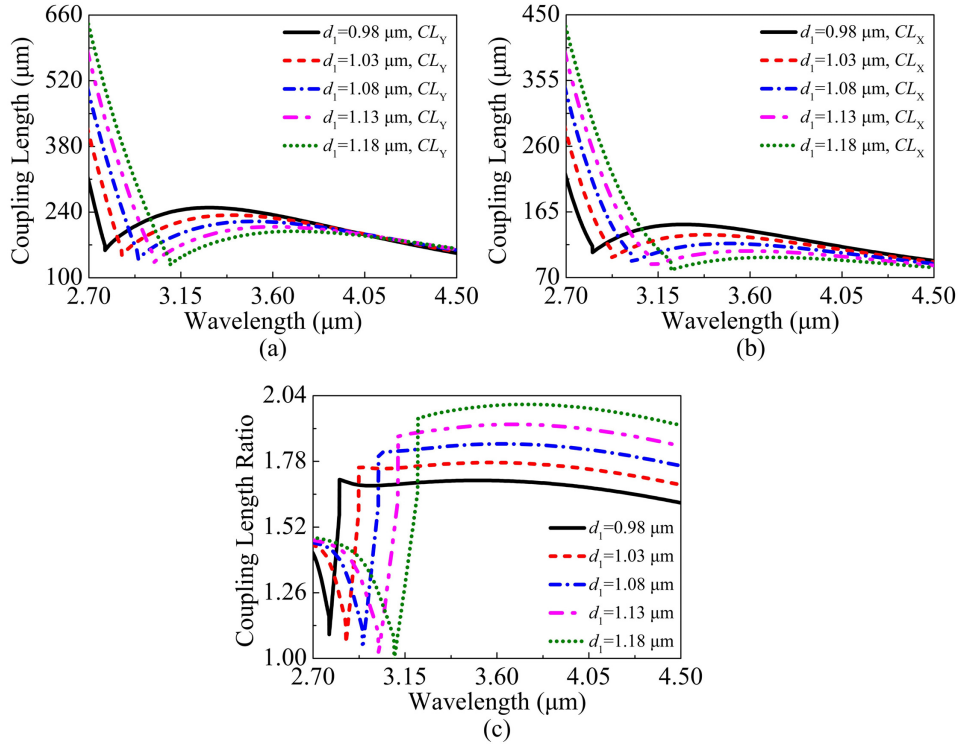


Fig. 4. The relationships between the CL of (a) Y-pol and (b) X-pol and (c) CLR and  $d_1$ .

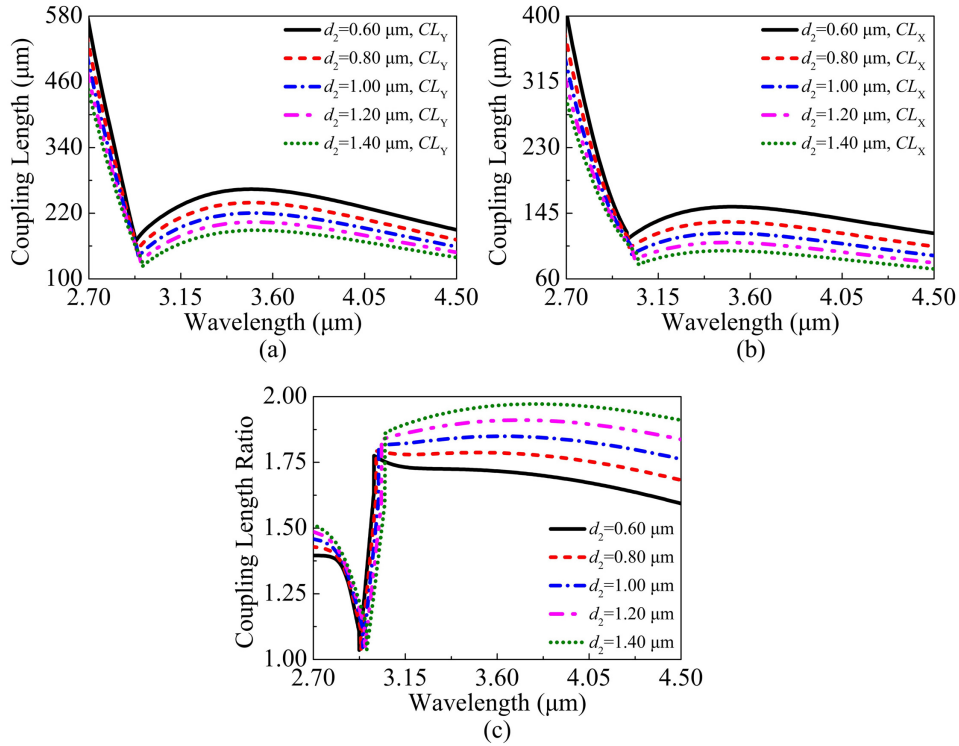


Fig. 5. The relationships between the CL of (a) Y-pol, (b) X-pol, and (c) CLR and  $d_2$ .

The relationships between the  $CL_Y$ ,  $CL_X$ , and  $CLR$  and  $d_2$  are shown in Figs. 5(a), 5(b), and 5(c), respectively. In Figs. 5(a) and 5(b), as  $d_2$  increases, the  $CL_Y$  and  $CL_X$  decrease gradually at the shorter wavelength, but the relative decrease of the  $CL_Y$  is smaller than that of the  $CL_X$ . Moreover, the mutation inflection point slightly shifts towards the long wavelength. As a result, when  $d_2$  increases, the mutation inflection point of the  $CLR$  slightly shifts towards the long wavelength, and the  $CLR$  after the mutation inflection point increases gradually, as shown in Fig. 5(c).

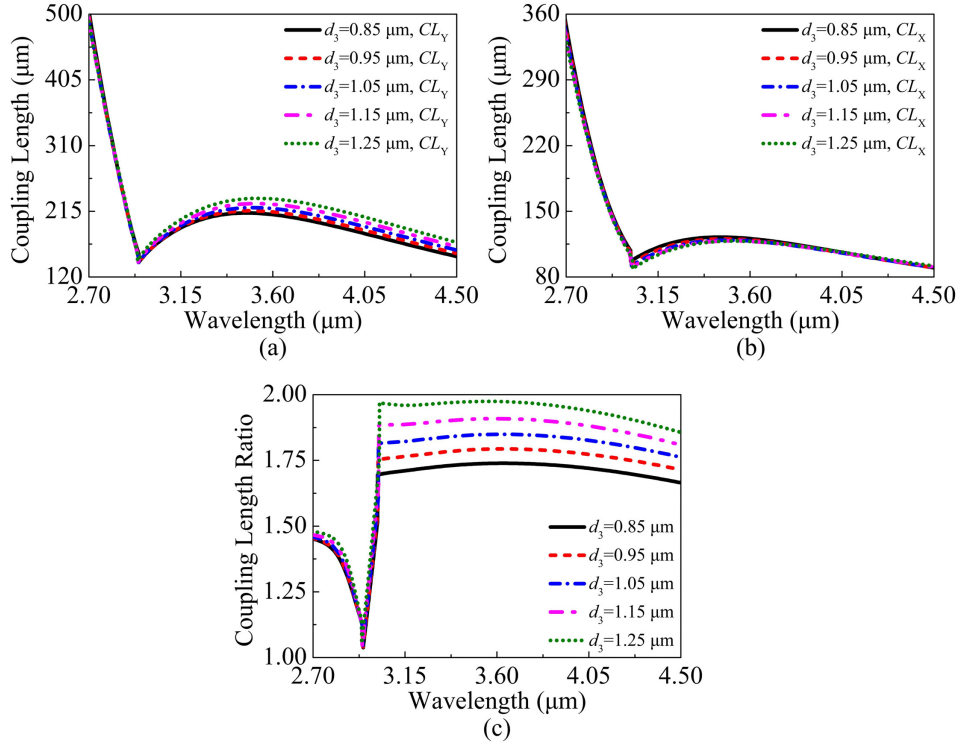


Fig. 6. The relationships between the  $CL$  of (a) Y-pol, (b) X-pol, and (c)  $CLR$  and  $d_3$ .

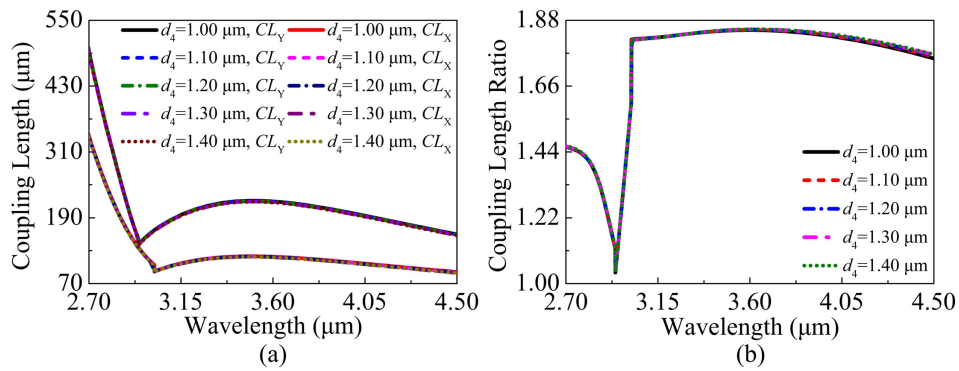


Fig. 7. The relationships between (a) the  $CL$  of the Y-pol and X-pol, (b)  $CLR$  and  $d_4$ .

Figs. 6(a), 6(b), and 6(c) show the relationships between the  $CL_Y$ ,  $CL_X$ , and  $CLR$  and  $d_3$ , respectively. It can be seen from Figs. 6(a) and 6(b) that the  $CL_Y$  increases gradually, but the  $CL_X$  changes slightly when  $d_3$  increases. And the mutation inflection point remains nearly unchanged. Thus, as  $d_3$  increases, the mutation inflection point of the  $CLR$  remains nearly



unchanged, and the  $CLR$  after the mutation inflection point retains a relatively stable increase, as shown in Fig. 6(c).

Figs. 7(a) and 7(b) show the relationships between the  $CL_Y$ ,  $CL_X$ , and  $CLR$  and  $d_4$ , respectively. From Fig. 7(a), the  $CL_Y$  and  $CL_X$  change slightly when  $d_4$  increases. The main reason is considered that the influences of  $d_4$  on the effective refractive indices of the even and odd modes of the Y-pol and X-pol have reached an approximate convergence. Therefore, the  $CLR$  remains nearly unchanged with the increase of  $d_4$ , as seen from Fig. 7(b).

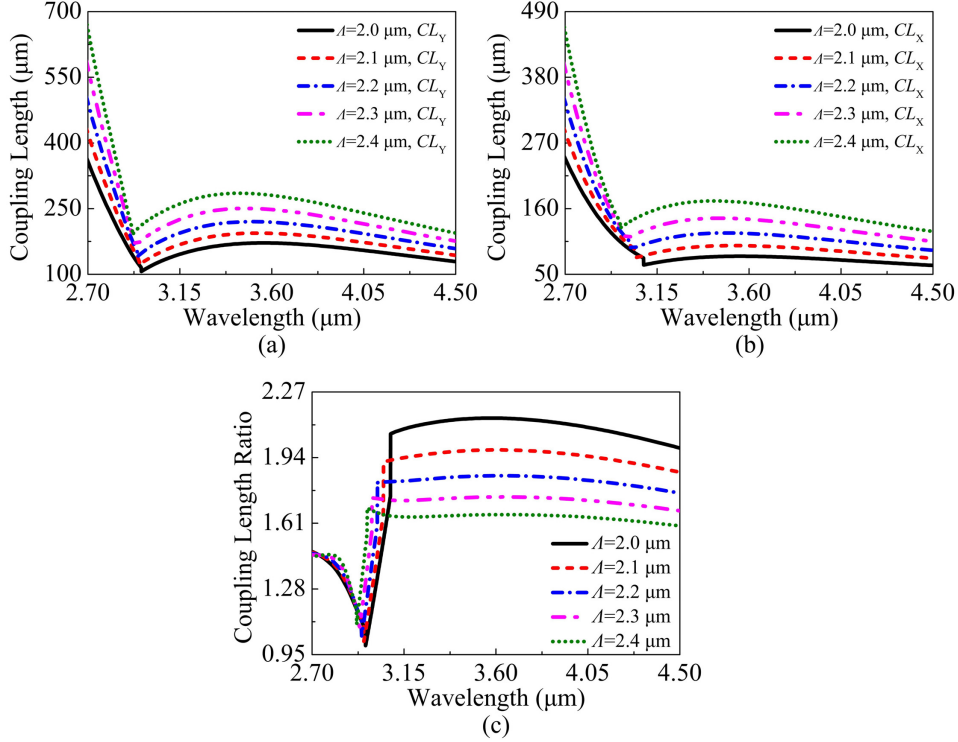


Fig. 8. The relationships between the  $CL$  of (a) Y-pol, (b) X-pol, and (c)  $CLR$  and  $A$ .

The relationships between the  $CL_Y$ ,  $CL_X$ , and  $CLR$  and  $A$  are shown in Figs. 8(a), 8(b), and 8(c), respectively. In Figs. 8(a) and 8(b), with the increase of  $A$ , the  $CL_Y$  and  $CL_X$  increase gradually, but the relative increase of the  $CL_Y$  is smaller than that of the  $CL_X$ . In addition, the mutation inflection point occurs to slightly shift towards the short wavelength. Hence, with the increase of  $A$ , the mutation inflection point of the  $CLR$  has a little shift towards the short wavelength, and the  $CLR$  after the mutation inflection point maintains a relatively stable decrease, as seen from Fig. 8(c).

Figs. 9(a), 9(b), and 9(c) show the relationships between the  $CL_Y$ ,  $CL_X$ , and  $CLR$  and  $t$ , respectively. From Figs. 9(a) and 9(b), as  $t$  increases, the  $CL_Y$  and  $CL_X$  increase gradually at the shorter wavelength, but the relative increase of the  $CL_Y$  is smaller than that of the  $CL_X$ . In addition, although the  $CL_Y$  and  $CL_X$  decrease gradually at the longer wavelength, the relative decrease of the  $CL_Y$  is larger than that of the  $CL_X$ , and the mutation inflection point shifts towards the short wavelength. It can also be seen from Figs. 9(a) and 9(b) that the values of the  $CL_Y$  and  $CL_X$  change in a relatively small range. As a result, with the increase of  $t$ , the mutation inflection point shifts towards the short wavelength, and the  $CLR$  after the mutation inflection point decreases gradually in a small range, as seen from Fig. 9(c).

According to the above results, the influences of the structure parameters of the Si-DC-PCF on the  $CL_Y$ ,  $CL_X$ , and  $CLR$  can be found. Thus, the optimization process of

designing the Si-DC-PCF can be summarized as following. First, the  $CLR=2$  could be achieved by adjusting  $A$ ,  $d_1$ , and  $d_3$ . Second, a suitable mutation inflection point at the short wavelength can be obtained by adjusting  $t$ . Third, the flatness of the  $CLR$  can be changed by adjusting  $d_2$  and  $d_4$ . Finally, the structure parameters of the designed Si-DC-PCF are optimized as follows:  $d_1=1.25 \mu\text{m}$ ,  $d_2=1.00 \mu\text{m}$ ,  $d_3=1.00 \mu\text{m}$ ,  $d_4=1.20 \mu\text{m}$ ,  $A=2.25 \mu\text{m}$ , and  $t=50 \text{ nm}$ . At this time, the corresponding  $CL_Y$ ,  $CL_X$ ,  $CLR$ , and  $CLR$  in the wavelength range from 3.35 to 4.35  $\mu\text{m}$  are shown in Figs. 10(a) and 10(b), respectively. From Fig. 10(a), the  $CL_Y$  and  $CL_X$  have a mutation inflection point at wavelengths 3.124 and 3.255  $\mu\text{m}$ , respectively. After 3.255  $\mu\text{m}$ , the value of the  $CLR$  remains  $\sim 2$  in a wide wavelength range. From Fig. 10(b), the value of the  $CLR$  remains in the range of 1.96  $\sim$  2.01 in the wavelength range from 3.35 to 4.35  $\mu\text{m}$ .

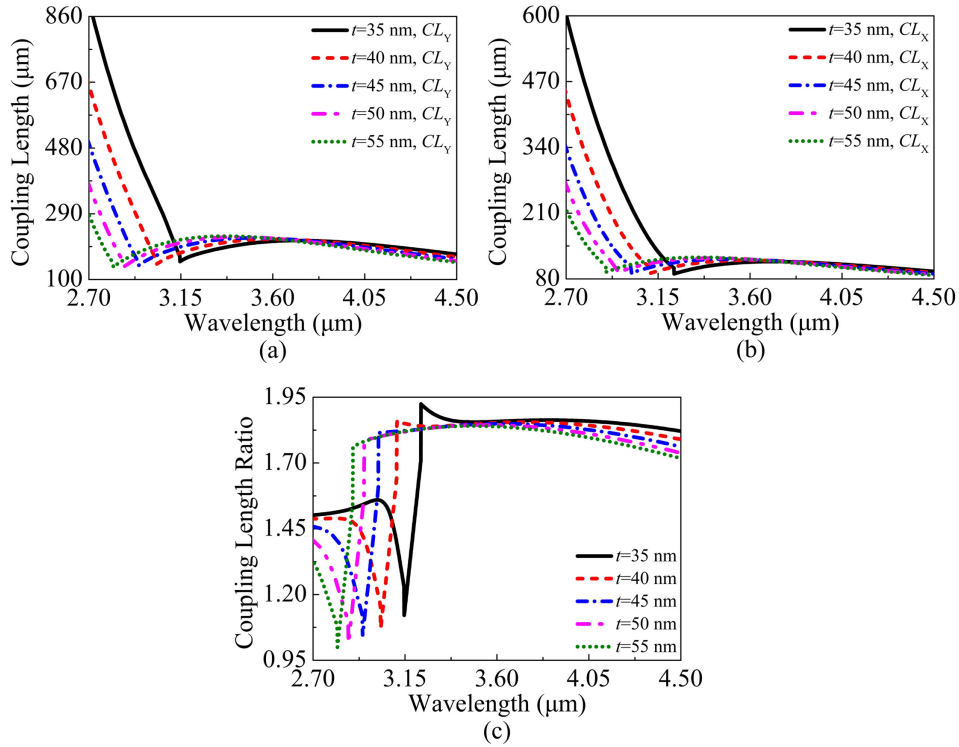


Fig. 9. The relationships between the  $CL$  of (a) Y-pol, (b) X-pol, and (c)  $CLR$  and  $t$ .

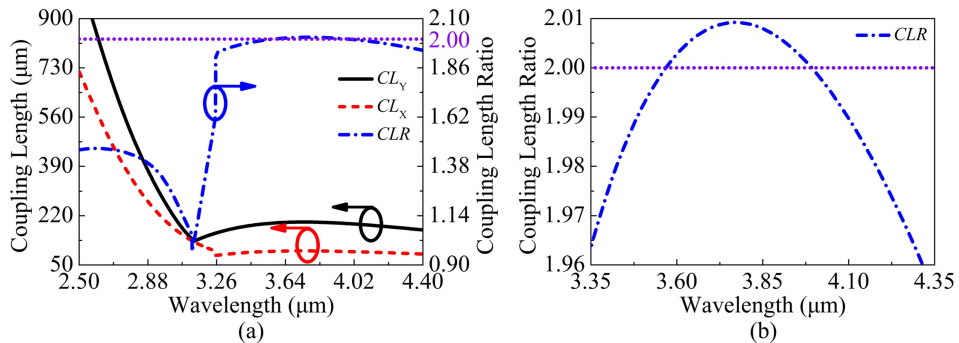
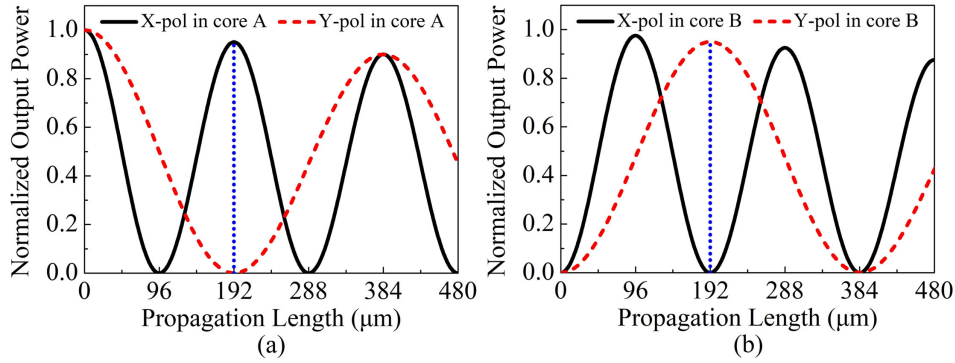
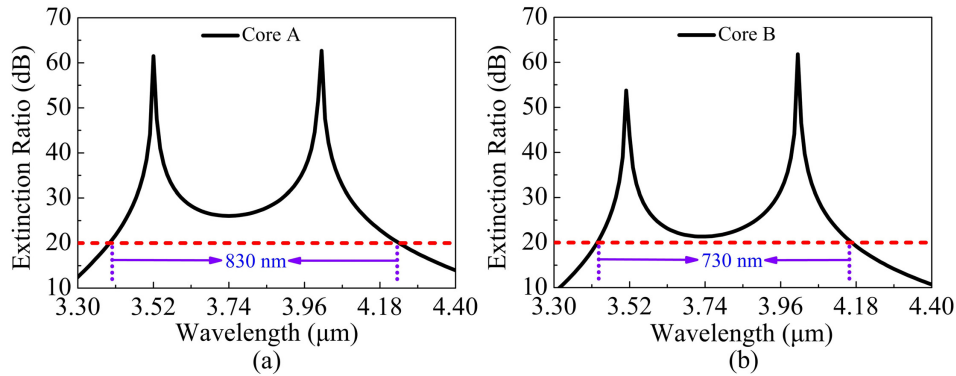


Fig. 10. (a) The final  $CL$  of the Y-pol and X-pol and  $CLR$ , and (b) the  $CLR$  in the wavelength range from 3.35 to 4.35  $\mu\text{m}$ .

It is assumed that the input light is launched into the core A. When the wavelength of the input light is located at 4  $\mu\text{m}$ , the  $CLR$  is exactly equal to 2. The relationships between  $P_{\text{out}}$  of the X-pol and Y-pol in the cores A and B and propagation length of the designed Si-DC-PCF at wavelength 4  $\mu\text{m}$  are shown in Figs. 11(a) and 11(b), respectively. From Fig. 11(a), when the propagation length is 192  $\mu\text{m}$ ,  $P_{\text{out}}$  of the X-pol in the core A reaches the maximum once again, while  $P_{\text{out}}$  of the Y-pol in the core A becomes 0 for the first time, which indicates that only the X-pol light remains in the core A at this time. From Fig. 11(b), when the propagation length is 192  $\mu\text{m}$ ,  $P_{\text{out}}$  of the Y-pol in the core B reaches the maximum for the first time, but  $P_{\text{out}}$  of the X-pol in the core B becomes 0 once again, which indicates that only the Y-pol light remains in the core B at this time. Therefore, the polarization splitting length of the designed Si-DC-PCF is 192  $\mu\text{m}$ . In addition, it can also be observed from Figs. 11(a) and 11(b) that the normalized output power decreases slightly with the increase of the propagation length, which is mainly induced by the ohmic loss of the gold film since a fraction of energy is propagated on the gold film surface [52]. Then, when the polarization splitting length is 192  $\mu\text{m}$ , the  $ER$  of the cores A and B as functions of the wavelength are shown in Figs. 12(a) and 12(b), respectively. From Fig. 12(a), the  $ER$  of the core A achieves 61.48 and 62.69 dB at wavelengths 3.52 and 4.01  $\mu\text{m}$ , respectively, and the corresponding bandwidth with the  $ER$  larger than 20 dB in the core A is 830 nm (3.40 ~ 4.23  $\mu\text{m}$ ). The  $ER$  of the core B achieves 53.74 and 61.78 dB at wavelengths 3.51 and 4.01  $\mu\text{m}$ , respectively, and the corresponding bandwidth with the  $ER$  larger than 20 dB in the core B is 730 nm (3.4 ~ 4.16  $\mu\text{m}$ ), as shown in Fig. 12(b).



**Fig. 11.** The relationships between the normalized output power  $P_{\text{out}}$  of the X-pol and Y-pol in the (a) core A and (b) core B and propagation length of the designed Si-DC-PCF at wavelength 4  $\mu\text{m}$ .



**Fig. 12.** The  $ER$  of (a) core A and (b) core B as functions of the wavelength.

Table 1 shows the comparison results between the proposed Si-DC-PCF PBS and reported

DC-PCF PBS. From Table 1, although the length of the proposed Si-DC-PCF PBS is slightly longer than that in Refs [48] and [34], the proposed fiber structure is a traditional hexagonal lattice, which is easy to fabricate. In addition, the proposed Si-DC-PCF PBS has the two large bandwidths at mid-infrared spectral region. The bandwidths with the *ER* above 20 dB in the cores A and B can be up to 830 and 730 nm, respectively.

**Table 1. Comparison results between the proposed Si-DC-PCF PBS and reported DC-PCF PBS.**

Reference	Additional materials or other structures	PBS length	Bandwidth of <i>ER</i> above 20 dB in core A	Bandwidth of <i>ER</i> above 20 dB in core B
[30] 2015	Gold film	542 $\mu\text{m}$	210 nm ( $\sim$ E+S+C+L)	220 nm ( $\sim$ E+S+C+L)
[13] 2016	Liquid crystal (E7)	890.5 $\mu\text{m}$	$\sim$ 150 nm ( $\sim$ S+C+L)	Not mentioned
[14] 2017	Gold wire	1079 $\mu\text{m}$	70 nm	Not mentioned
[16] 2017	magnetic fluids	8130 $\mu\text{m}$	Not mentioned	Not mentioned
[48] 2018	Rectangular lattice	103 $\mu\text{m}$	177 nm (1.458 $\sim$ 1.635 $\mu\text{m}$ )	79 nm (1.508 $\sim$ 1.587 $\mu\text{m}$ )
[34] 2019	Gold film and Rectangular lattice	104 $\mu\text{m}$	575 nm (1.35 $\sim$ 1.925 $\mu\text{m}$ )	Not mentioned
This work	Gold film	192 $\mu\text{m}$	830 nm (3.40 $\sim$ 4.23 $\mu\text{m}$ )	730 nm (3.43 $\sim$ 4.16 $\mu\text{m}$ )

At present, the proposed Si-DC-PCF can be fabricated by the stack and draw technology combined with the magnesium thermal reduction or femtosecond laser drilling method [53, 54]. The gold film can be deposited by the high pressure microfluidic chemical deposition [57-60].

#### 4. Conclusions

In summary, a novel Si-DC-PCF PBS based on the SPR effect is proposed. By optimizing the structure parameters of the Si-DC-PCF, the *CLR* remains in the range of 1.96  $\sim$  2.01 in the wavelength range from 3.35 to 4.35  $\mu\text{m}$ . When the polarization splitting length is chosen as 192  $\mu\text{m}$ , only the X-pol light remains in the core A, and the corresponding Y-pol light remains in the core B. The *ERs* of the cores A and B achieve 61.48 and 62.69 dB, and 53.74 and 61.78 dB at wavelengths 3.52 and 4.01  $\mu\text{m}$ , and 3.51 and 4.01  $\mu\text{m}$ , respectively. The bandwidths with the *ER* larger than 20 dB in the cores A and B can be up to 830 nm (3.40  $\sim$  4.23  $\mu\text{m}$ ) and 730 nm (3.43  $\sim$  4.16  $\mu\text{m}$ ), respectively. The proposed Si-DC-PCF PBS has the ultra-short polarization splitting length and ultra-wide splitting bandwidth, so it can be applied in the different mid-infrared optical systems. For example, it can be applied in the holmium-doped fluoride fiber laser system [41].

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## Disclosures

The authors declare no conflicts of interest.

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