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A distributed fault detection scheme in disturbed heterogeneous networked systems

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Abstract This paper deals with the problem of distributed fault detection and isolation in multi-agent systems with disturbed high-order dynamics subject to communication uncertainties and faults. Distributed finite-frequency mixed $\mathcal{H}_-/\mathcal{H}_\infty$ unknown input observers are designed to detect and distinguish actuator, sensor and communication faults. Furthermore, an agent is capable of detecting not only its own faults but also faults in its neighbouring agents. Sufficient conditions are then derived in terms of a set of linear matrix inequalities while adding additional design variables to reduce the conservatism. A numerical simulation is carried out in order to demonstrate the effectiveness of the proposed approach.

Keywords Fault detection and isolation · Attack detection · Multi-agent systems · Networked systems · Unknown input observers · Linear matrix inequalities

1 Introduction

During the past couple of decades, multi-agent systems have received considerable amount of attention from researchers thanks to their wide range of potential applications in different areas, such as formation control, constellations in satellite systems [1,2], cooperative unmanned aerial vehicles [3], transport systems [4], power grids and mobile robots [5–7], to mention a few.

The growing size and complexity of such systems render their safe operation and reliability critical topics of research. Indeed, in order to achieve their mission, the agents communicate between themselves over a given network. Hence, their vulnerability does not only stem from the fact that each agent can be faulty at any given time instant but also from the fact that the communication links between them can be faulty or subject to an attack. Indeed, on top of actuator and sensor faults, MASs can be subjected to multiple types of cyber-attacks [8–13].

In fact, many cyber-attacks have recently occurred around the world. Some examples include: multiple power blackouts in some countries like Brazil [14], the attack on the water distribution system in Australia [15], the Stuxnet attack that took control of actuators

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and sensors in an Iranian nuclear facility prompting the replacement of thousands of failed centrifuges [16], the cyber-attack against an Ukrainian power grid [17], etc. Clearly, these types of malicious attacks aim at degrading or interrupting the operation of connected systems, exploit their aforementioned vulnerabilities and can have extremely detrimental effects, not only from a process point of view but also from an environmental and financial one as well. It is shown in [18] that information security techniques such as adding encryption and authentication schemes can help make some attacks more difficult to succeed, but that they are far from being sufficient against cyber-attacks. Indeed, these malicious attacks may go unnoticed and lead to erroneous behaviours in the overall MAS's dynamics and compromising the mission. This makes understanding their effects on the MAS dynamics, modelling them, detecting them, identifying them as well as isolating them, important issues.

There is a multitude of ways to detect and isolate faults and cyber-attacks in MASs. The reader is referred to [19] for a recent comprehensive survey. Some works proposed centralised architectures to detect faults or attacks [20, 21], due to their simplicity, whereby the analysis of all data is done by a central unit. However, in order to avoid long-distance data transmissions, reduce complexity and improve scalability, namely in larger systems, the detection and isolation process should be distributed.

A great deal of existing works in the literature either focuses on linear MASs [22–29], do not consider the effect of disturbances [22, 30], or do not consider the effect of measurement and communication noise [23, 31, 32]. However, it is a well-known fact that disturbances and noise are practically inevitable. Furthermore, some works focus only actuator faults [23, 29, 31, 33] or on sensor faults [25–27].

In [26, 30, 31, 34], UIOs were used for fault detection. Nevertheless, most of the existing works on fault detection using UIOs consider that the generated residual signals are completely decoupled from the unknown input. Indeed, they usually require a strict rank condition to decouple the unknown input vector, which can be infeasible. In [31] for instance, an UIO residual-based scheme for nonlinear homogeneous MASs with actuator faults was proposed, where faults and disturbances were decoupled from the error dynamics assuming some rank conditions. In [26], UIOs were combined with the mixed $\mathcal{H}_-/\mathcal{H}_\infty$ method for fault detection

purpose where only sensor faults were considered. Furthermore, the \mathcal{H}_- performance index method proposed therein, as well as in [25, 27] for instance, is only applicable when the distribution matrix of the sensor faults is of full column rank. In our work, one contribution is to relax such condition using the finite-frequency approach introduced in [35]. Furthermore, in [27, 36] for instance, multiple faults cannot occur in the MAS, which is a drawback, especially in large-sized MASs.

In [23, 27–29, 31], information from neighbouring FDI filters was transmitted among agents, which may weaken the distributed property of the detection scheme. Indeed, if and when an observer fails to accurately give an estimate at a given instant for an agent, all surrounding observers in its neighbourhood are compromised, which in turn compromises their respective neighbours' observers, thus creating a destructive snowball effect that might lead to confusing results, trigger false alarms, etc. In our work, such drawback is removed since observers do not communicate between themselves.

Unlike [23, 28, 29, 31], where the topology is assumed to be undirected, a directed communication graph is considered in this work. Additionally, the proposed scheme in this paper does not require knowledge beyond its 1-hop neighbourhood and is independent on the graph topology of the overall MAS, making it more scalable. Furthermore, as opposed to the detection filters proposed in [23, 29, 31, 33] where their size increases as the graph topology grows, in the proposed scheme, the size of the filter is only limited to the size of the neighbourhood of each agent independently, hence improving the scalability and reducing the computational burdens.

Given the limitations discussed above with respect to the existing studies, the main contributions of this work are summarised as follows:

- A more general problem is studied where actuator, sensor and communication faults are considered in the robust detection and isolation process for Lipschitz nonlinear heterogeneous MASs with disturbances and communication parameter uncertainties, without global knowledge about the communication graph and under-directed graphs.
- A distributed finite-frequency mixed $\mathcal{H}_-/\mathcal{H}_\infty$ nonlinear UIO-based FDI scheme is designed such that actuator and sensor faults along with the communication faults are treated separately. Hence, the

rank condition on the measurement fault distribution matrix as required by [27, 28] for instance is relaxed. Additionally, the scheme is capable of detecting and distinguishing multiple faults and attacks at a given time instant.

- Sufficient conditions in terms of a set of LMIs are provided for the proposed finite-frequency $\mathcal{H}_-/\mathcal{H}_\infty$ UIO-based method, where the coupling between Lyapunov matrices and the observer matrices is avoided. This LMI characterisation enables to reduce conservatism by introducing additional design variables.

A brief comparison of the proposed method with some existing works in the literature is given in Table 1. To the best of the authors' knowledge, a distributed finite-frequency mixed $\mathcal{H}_-/\mathcal{H}_\infty$ nonlinear UIO-based scheme for FDI in heterogeneous networked MASs subject to disturbances, noise, actuator faults, sensor faults and communication attacks, is investigated for the first time in this paper.

The rest of the manuscript is organised as follows. Section 2 presents the problem formulation and some preliminaries. The proposed finite-frequency $\mathcal{H}_-/\mathcal{H}_\infty$ UIO-based method and the corresponding algorithms are laid out in Sect. 3. In Sect. 4, an illustrative example is given to show the effectiveness of the proposed scheme. Finally, some conclusions are inferred in Sect. 5.

Notations: Given a transfer function $T_{xy}(s)$ linking y to x , its \mathcal{H}_∞ norm is defined as

$$\|T_{xy}\|_\infty = \sup_\omega \bar{\sigma}(T_{xy}(j\omega)).$$

where $\bar{\sigma}$ is the maximum singular value of $T_{xy}(s)$. Its \mathcal{H}_- index is defined as

$$\|T_{xy}\|_- = \inf_\omega \underline{\sigma}(T_{xy}(j\omega)).$$

where $\underline{\sigma}$ is the minimum singular value of $T_{xy}(s)$. For a square matrix A , $\mathbf{He}(A) = A + A^*$ where the superscript A^* corresponds to the conjugate of A . $\text{tr}(A)$ is the trace of A . $\mathbf{1}_n$ and I_n refer to a column of all entries 1 and an identity matrix, respectively, and of dimensions n . $0_{m \times n}$ denotes a null matrix of dimension $m \times n$. $\text{diag}(a_1, a_2, \dots, a_n)$ denotes the diagonal matrix containing a_1, a_2, \dots, a_n on the diagonal. $\text{Blkdiag}(A_1, A_2, \dots, A_n)$ denotes the block diagonal matrix with matrices A_1, A_2, \dots, A_n on the diagonal. $\text{Col}(A_1, A_2, \dots, A_n)$ denotes the column block matrix $(A_1^T, A_2^T, \dots, A_n^T)^T$. Throughout this paper, for a real

square matrix $P \in \mathbb{R}^{n \times n}$, $P > 0$ implies that P is symmetric and positive-definite.

2 Problem formulation

Consider a heterogeneous MAS composed of N agents labelled by $i \in \{1, \dots, N\}$ and described by the following uncertain dynamics

$$\begin{cases} \dot{x}_i(t) = A_i x_i(t) + B_{u_i} u_i(t) + B_{d_i} d_i(t) + B_{f_i} f_{a_i}(t) \\ \quad + \varphi_i(x_i(t)) \\ y_i(t) = C_i x_i(t) + D_{d_i} d_i(t) + D_{f_i} f_{s_i}(t) \end{cases}, \quad (1)$$

where $x_i \in \mathbb{R}^{n_x}$, $u_i \in \mathbb{R}^{n_u}$, $y_i \in \mathbb{R}^{n_y}$, $d_i \in \mathbb{R}^{n_d}$, $f_{a_i} \in \mathbb{R}^{n_{fa}}$, $f_{s_i} \in \mathbb{R}^{n_{fs}}$ are the state vector, the control input, the output, the L_2 -norm bounded disturbances and noise, the actuator fault and the sensor fault signals, respectively. Matrices $A_i \in \mathbb{R}^{n_x \times n_x}$, $B_{u_i} \in \mathbb{R}^{n_x \times n_u}$, $B_{d_i} \in \mathbb{R}^{n_x \times n_d}$, $B_{f_i} \in \mathbb{R}^{n_x \times n_{fa}}$, $C_i \in \mathbb{R}^{n_y \times n_x}$, $D_{d_i} \in \mathbb{R}^{n_y \times n_d}$, $D_{f_i} \in \mathbb{R}^{n_y \times n_{fs}}$ are known constant matrices. $\varphi_i(x_i(t)) \in \mathbb{R}^{n_x}$ is a known function representing the nonlinearity of agent i .

2.1 Graph theory and communication faults

The topology is represented by a directed graph $\mathcal{G} = (\mathcal{V}, \mathcal{E})$, where $\mathcal{V} = \{1, \dots, N\}$ is the node set and $\mathcal{E} \subseteq \mathcal{V} \times \mathcal{V}$ is the edge set. It is described by an adjacency matrix $\mathcal{A} \in \mathbb{R}^{N \times N}$ that contains positive weight entries. If information flows from node j to i , then $a_{ij} > 0$, otherwise $a_{ij} = 0$. The neighbouring set of node i , denoted by $\mathcal{N}_i \subseteq \mathcal{V}$, is the subset of nodes that node i can sense and interact with. Alternatively, one could note $\mathcal{N}_i = \{i_1, i_2, \dots, i_{N_i}\} \subseteq [1, N]$, where $N_i = |\mathcal{N}_i|$.

The measured outputs are exchanged between neighbouring agents. Hence, an agent i receives from each neighbour $j \in \mathcal{N}_i$ its output (resp. input), corrupted by parameter uncertainties associated with the communication link between i and j , $\Delta a_{ij}(t) \in \mathbb{R}$ and by faults due to link faults, packet losses or potential cyber-attacks denoted $f_{ij}^z(t) \in \mathbb{R}^{n_{fz_{ij}}}$ (resp. $f_{ij}^u(t) \in \mathbb{R}^{n_{fu}}$), i.e.

$$\begin{aligned} z_{ij}(t) &= a_{ij}(1 + \Delta a_{ij}(t))y_j(t) + D_{z_{ij}} f_{ij}^z(t), \\ u_{ij}(t) &= a_{ij}(1 + \Delta a_{ij}(t))u_j(t) + D_{u_{ij}} f_{ij}^u(t), \end{aligned} \quad (2)$$

with $z_{ii}(t) = y_i(t)$ and $u_{ii}(t) = u_i(t)$. $D_{z_{ij}} \in \mathbb{R}^{n_y \times n_{fz_{ij}}}$ and $D_{u_{ij}} \in \mathbb{R}^{n_u \times n_{fu}}$ are known constant

Table 1 Brief comparison with some existing works, where the following acronyms are used: P.S.: Proposed Scheme; D&N: Both Disturbances and Noise; A&S Faults: Both Actuator and

Sensor Faults; UTR: Undirected Topology Required; RISR: Relative Information Sensors Required; AGIR: Access to the Collective Input Required; GK: Global Knowledge

Reference	Linear	D&N	Heterogeneous	A&S Faults	Attacks	UTR	RISR	ACIR	GK
[22]	Yes	No	No	No	Yes	Yes	No	No	Yes
[23]	Yes	No	No	No	No	Yes	No	No	Yes
[27]	Yes	Yes	No	No	No	Yes	Yes	No	Yes
[30]	Yes	No	No	No	Yes	Yes	No	No	Yes
[26]	Yes	Yes	Yes	No	No	Yes	Yes	No	No
[34]	No	No	No	No	No	Yes	No	Yes	Yes
[37]	Yes	No	No	No	Yes	Yes	No	No	Yes
[38]	Yes	No	No	No	Yes	Yes	No	No	No
P. S.	No	Yes	Yes	Yes	Yes	No	No	No	No

matrices. It is also assumed that the parameter uncertainties $\Delta a_{ij}(t)$ satisfy $|\Delta a_{ij}(t)| < a_{ij}$.

Remark 1 It is worth noting that the considered faults cover a wide range of cyber-attacks that have been studied in the literature. For instance, assume that $\Delta a_{ij} = 0$ for the sake of clarity,

- In the case of a communication parametric fault [30] for i , affecting all its incoming information from agent j , one has

$$\begin{aligned} z_{ij}(t) &= (a_{ij} + f_{a_{ij}}(t))y_j(t) \\ &= a_{ij}y_j(t) + f_{a_{ij}}(t)y_j(t), \end{aligned}$$

where analogously to (2), one could note that $f_{ij}^z(t) = f_{a_{ij}}(t)y_j(t)$ and $D_{z_{ij}} = I_{n_y}$. $f_{a_{ij}}(t)$ represents a parametric fault affecting the communication parameter a_{ij} .

- In a denial of service attack situation affecting all incoming information from agent j , one has $f_{ij}^z(t) = -a_{ij}\delta(t - t_{ij})y_j(t)$ and $D_{z_{ij}} = I_{n_y}$ [39], where

$$\delta(t - t_{ij}) = \begin{cases} 1, & t \geq t_{ij} \\ 0, & \text{else} \end{cases},$$

and t_{ij} is the instant at which the attack occurs.

- Conversely, in a false data injection situation in the transmitted information, agent j transmits or agent i receives fake/invalid information, that is, $f_{ij}^z(t)$ contains the injected malicious information [12]. In the case where the malicious information $f_{ij}^z(t) \in \mathbb{R}$ affects all incoming transmitted data equally, then one could set $D_{z_{ij}} = \mathbf{1}_{n_y}$.

- Under replay attacks, the attacker intercepts the transmitted information and replays it with a delay instead of the actual information. In this case, one could write [10], $f_{ij}^z(t) = \delta_{ij}(t - t_{ij})(-a_{ij}y_j(t) + y_j(t - \mathcal{T}_{ij}))$ and $D_{z_{ij}} = I_{n_y}$, where

$$\delta_{ij}(t - t_{ij}) = \begin{cases} 1, & t \geq t_{ij} \\ 0, & \text{else} \end{cases},$$

and $t_{ij} > 0$ is the instant at which the attack occurs and $\mathcal{T}_{ij} \in \mathbb{R}$ is the time delay.

The same remarks could be made w.r.t. $u_{ij}(t)$. Contrary to agent/node attacks or faults in the form of the signals $f_{a_i}(t)$, $f_{s_i}(t)$, edge/communication attacks cannot be detected locally by an emitting agent j and thus need its neighbours to detect them. It is worth mentioning that the introduced problem can represent many potential practical applications to FDI in networked MASSs. As discussed in introduction section, such applications include electric power networks and micro-grids, multi-robot and multi-vehicle systems, etc. [37, 38, 40].

2.2 Concatenated local model

In this subsection, a concatenated model is developed for each agent. Let us first denote

$$\left\{ \begin{array}{l} x_{v_i} = [x_i^T, x_{i_1}^T, \dots, x_{i_{N_i}}^T]^T \in \mathbb{R}^{n_x^i}, \\ d_{v_i} = [d_i^T, d_{i_1}^T, \dots, d_{i_{N_i}}^T]^T \in \mathbb{R}^{n_d^i}, \\ f_{vs_i} = [f_{s_i}^T, f_{s_{i_1}}^T, \dots, f_{s_{i_{N_i}}}^T]^T \in \mathbb{R}^{n_{fs}^i}, \\ f_{va_i} = [f_{a_i}^T, f_{a_{i_1}}^T, \dots, f_{a_{i_{N_i}}}^T]^T \in \mathbb{R}^{n_{fa}^i}, \\ z_i = [(y_i - y_{i_1})^T, \dots, (y_i - y_{i_{N_i}})^T]^T \in \mathbb{R}^{n_z^i}, \\ y_{v_i} = [y_{i_1}^T, \dots, y_{i_{N_i}}^T]^T \in \mathbb{R}^{n_y^i}, \\ u_{v_i} = [u_{i_1}^T, \dots, u_{i_{N_i}}^T]^T \in \mathbb{R}^{n_u^i}, \end{array} \right. \quad (3)$$

the concatenated state, disturbance, fault signals, relative information, output and input of agent i ($i_j \in \mathcal{N}_i$), where $n_x^i = n_x(N_i + 1)$, $n_d^i = n_d(N_i + 1)$, $n_{fa}^i = n_{fa}(N_i + 1)$, $n_{fs}^i = n_{fs}(N_i + 1)$, $n_z^i = n_y N_i$ and $n_u^i = n_u N_i$. A virtual output is given as

$$z_{v_i} = Z^i \begin{pmatrix} y_i \\ z_i \end{pmatrix} + \Delta Z^i \begin{pmatrix} y_i \\ y_{v_i} \end{pmatrix} + D_{vz_i} f_i^z \in \mathbb{R}^{n_z^i}, \quad (4)$$

where

$$\left\{ \begin{array}{l} Z^i = \begin{pmatrix} I_{n_y} & 0_{n_y \times n_z^i} \\ 0_{n_z^i \times n_y} & \mathcal{A}_i \end{pmatrix} \in \mathbb{R}^{n_z^i \times n_z^i}, \\ \Delta Z^i = \begin{pmatrix} 0_{n_y \times n_y} & 0_{n_y \times n_z^i} \\ 0_{n_z^i \times n_y} & \mathcal{A}_i \Delta \mathcal{A}_i \end{pmatrix} \in \mathbb{R}^{n_z^i \times n_z^i}, \\ \Delta \mathcal{A}_i = \text{diag}(\underbrace{\Delta a_{ii1}, \dots, \Delta a_{ii1}}_{n_y \text{ times}}, \dots, \Delta a_{iiN_i}, \dots, \Delta a_{iiN_i}) \\ \in \mathbb{R}^{n_z^i \times n_z^i}, \\ \mathcal{A}_i = \text{diag}(\underbrace{a_{ii1}, \dots, a_{ii1}}_{n_y \text{ times}}, \dots, a_{iiN_i}, \dots, a_{iiN_i}) \\ \in \mathbb{R}^{n_z^i \times n_z^i}, \\ D_{vz_i} = \begin{pmatrix} 0_{n_y \times n_{fz}^i} \\ -\text{Blkdiag}[D_{zii1}, D_{zii2}, \dots, D_{ziiN_i}] \end{pmatrix} \\ \in \mathbb{R}^{n_z^i \times n_{fz}^i}, \\ z_{v_i} = [y_{i_1}^T, z_{ii1}^T, \dots, z_{iiN_i}^T]^T \in \mathbb{R}^{n_z^i}, \\ f_i^z = [f_{ii1}^z, f_{ii2}^z, \dots, (f_{iiN_i}^z)^T]^T \in \mathbb{R}^{n_{fz}^i}, \end{array} \right.$$

with $n_{fz}^i = \sum_{j \in \mathcal{N}_i} n_{fz_{ij}} \neq 0$, $n_z^i = n_y(N_i + 1)$. z_{v_i} and f_i^z are the concatenated measured vector available for agent i and the associated communication fault signals, respectively. $\tilde{\mathcal{A}}_i = \mathcal{A}_i + \Delta \mathcal{A}_i \in \mathbb{R}^{n_z^i \times n_z^i}$ is the actual local adjacency matrix of agent i which takes into account the parametric uncertainty associated with

the communication links. Replacing outputs and inputs with their respective values from (1) yields

$$\left\{ \begin{array}{l} \dot{x}_{v_i}(t) = \tilde{\mathcal{A}}_i x_{v_i}(t) + \tilde{\mathcal{B}}_{u_i} u_{v_i}(t) + \tilde{\mathcal{B}}_{u_i} u_i(t) + \tilde{\mathcal{B}}_{d_i} d_{v_i}(t) \\ \quad + \tilde{\mathcal{B}}_{f_i} f_{va_i}(t) + \varphi_{v_i}(x_{v_i}(t)), \\ z_{v_i}(t) = Z^i (\tilde{\mathcal{C}}_i x_{v_i}(t) + \tilde{\mathcal{D}}_{d_i} d_{v_i}(t) + \tilde{\mathcal{D}}_{f_i} f_{vs_i}(t)) \\ \quad + D_{vz_i} f_i^z(t) + \Delta Z^i \begin{pmatrix} y_i(t) \\ y_{v_i}(t) \end{pmatrix} \end{array} \right. \quad (5)$$

where

$$\left\{ \begin{array}{l} \varphi_{v_i}(x_{v_i}(t)) = \text{Col}(\varphi_i(x_i(t)), \dots, \varphi_{i_{N_i}}(x_{i_{N_i}}(t))), \\ \tilde{\mathcal{A}}_i = \text{Blkdiag}(\mathcal{A}_i, \mathcal{A}_{i_1}, \dots, \mathcal{A}_{i_{N_i}}), \\ \tilde{\mathcal{B}}_{u_i} = \text{Col}(\mathcal{B}_{u_i}, 0_{n_x \times n_u}, \dots, 0_{n_x \times n_u}), \\ \tilde{\mathcal{B}}_{u_i} = \text{Col}(0_{n_x \times n_u}, \text{Blkdiag}(\mathcal{B}_{u_{i_1}}, \dots, \mathcal{B}_{u_{i_{N_i}}}), \\ \tilde{\mathcal{B}}_{d_i} = \text{Blkdiag}(\mathcal{B}_{d_i}, \mathcal{B}_{d_{i_1}}, \dots, \mathcal{B}_{d_{i_{N_i}}}), \\ \tilde{\mathcal{B}}_{f_i} = \text{Blkdiag}(\mathcal{B}_{f_i}, \mathcal{B}_{f_{i_1}}, \dots, \mathcal{B}_{f_{i_{N_i}}}), \end{array} \right.$$

$\tilde{\mathcal{C}}_i$, $\tilde{\mathcal{D}}_{d_i}$ and $\tilde{\mathcal{D}}_{f_i}$ correspond to the following tilde notation

$$\tilde{\Theta}_i = \begin{bmatrix} \Theta_i & 0 & \dots & 0 \\ \Theta_i & -\Theta_{i_1} & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ \Theta_i & 0 & \dots & -\Theta_{i_{N_i}} \end{bmatrix},$$

with $\tilde{\mathcal{A}}_i \in \mathbb{R}^{n_x^i \times n_x^i}$, $\tilde{\mathcal{B}}_{u_i} \in \mathbb{R}^{n_x^i \times n_u^i}$, $\tilde{\mathcal{B}}_{f_i} \in \mathbb{R}^{n_x^i \times n_{fa}^i}$, $\tilde{\mathcal{C}}_i \in \mathbb{R}^{n_z^i \times n_x^i}$, $\tilde{\mathcal{D}}_{d_i} \in \mathbb{R}^{n_z^i \times n_d^i}$, $\tilde{\mathcal{D}}_{f_i} \in \mathbb{R}^{n_z^i \times n_{fs}^i}$. Let us make the following assumption on the parametric uncertainties

Assumption 1 There exist a time-varying matrix $v_i(t) \in \mathbb{R}^{n_z^i \times n_z^i}$ and known matrices \mathbf{X}_i and M_i with appropriate dimensions such that

$$\Delta Z^i = \mathbf{X}_i v_i(t) M_i, \quad (6)$$

with $\bar{\sigma}(v_i) \leq \delta_M$.

Remark 2 It is worth noting that this assumption stems from the definition of the graph topology in this paper and is standard for bounded uncertainties [41].

Under this assumption, one could rewrite system (5) as

$$\left\{ \begin{array}{l} \dot{x}_{v_i}(t) = \tilde{\mathcal{A}}_i x_{v_i}(t) + \tilde{\mathcal{B}}_{u_i} u_{v_i}(t) + \tilde{\mathcal{B}}_{u_i} u_i(t) + \tilde{\mathcal{B}}_{d_i} d_{v_i}(t) \\ \quad + \tilde{\mathcal{B}}_{f_i} f_{va_i}(t) + \varphi_{v_i}(x_{v_i}(t)), \\ z_{v_i}(t) = Z^i \tilde{\mathcal{C}}_i x_{v_i}(t) + Z^i \tilde{\mathcal{D}}_{d_i} d_{v_i}(t) + D_{\mathcal{F}_i} \mathcal{F}_i(t) \\ \quad - \mathbf{X}_i \phi_i(t), \end{array} \right. \quad (7)$$

where $\mathcal{F}_i(t) = \begin{pmatrix} f_{vs_i}(t) \\ f_{f_i}^z(t) \end{pmatrix}$, $D_{\mathcal{F}_i} = (Z^i \tilde{D}_{f_i} \ D_{vz_i})$,

$$\phi_i(t) = -v_i(t) D_{\phi_i} \begin{pmatrix} x_{v_i}(t) \\ d_{v_i}(t) \\ f_{vs_i}(t) \end{pmatrix},$$

$$D_{\phi_i} = M_i \begin{pmatrix} \text{Blkdiag}(C_i^T, \dots, C_{iN_i}^T) \\ \text{Blkdiag}(D_{d_i}^T, \dots, D_{d_{iN_i}}^T) \\ \text{Blkdiag}(D_{f_i}^T, \dots, D_{f_{iN_i}}^T) \end{pmatrix}^T.$$

Note that, in the case where $\tilde{D}_{f_i} = 0$, $D_{\mathcal{F}_i}$ is selected as $D_{\mathcal{F}_i} = D_{vz_i}$. The robust distributed FDI objective is the design of residual generators for each agent using locally exchanged information capable of detecting and isolating not only the agent's own faults but also the faults of its neighbours as well as attacks targeting incoming communication links.

The following assumption and lemma are going to be used in the next section.

Assumption 2 The nonlinear functions $\varphi_i(x_i(t))$ are Lipschitz, with Lipschitz constant θ_i , $\forall i = \{1, 2, \dots, N\}$, i.e. $\forall x_i, \hat{x}_i \in \mathbb{R}^{n_x}$

$$\|\varphi_i(x_i) - \varphi_i(\hat{x}_i)\| \leq \theta_i \|x_i - \hat{x}_i\|.$$

Remark 3 It is worth noting that Assumption 2 restricts the class of considered nonlinearities in Eq. (1) and has been considered in many works [42].

Lemma 1 [43] *Given real matrices F_i and J_i of appropriate dimensions, then the following inequality holds for any strictly positive scalar ε_i :*

$$F_i J_i^T + J_i F_i^T \leq \varepsilon_i J_i J_i^T + \varepsilon_i^{-1} F_i F_i^T.$$

3 Distributed fault detection and isolation scheme

The aim here is to design robust residual generators which are sensitive to all types of faults in spite of the presence of uncertainties using UIOs. Consider the following observer

$$\begin{cases} \dot{q}_{vi}(t) = N_i q_{vi}(t) + G_{1i} u_i(t) + G_{2i} U_i(t) + L_i z_{v_i}(t) \\ \quad + T_i \varphi_{v_i}(\hat{x}_{v_i}(t)) \\ \hat{x}_{v_i}(t) = q_{vi}(t) - H_i z_{v_i}(t) \\ \hat{z}_{v_i}(t) = Z^i \tilde{C}_i \hat{x}_{v_i}(t) \end{cases} \quad (8)$$

where $U_i(t) = \text{Col}(u_{ii_1}(t), \dots, u_{ii_{N_i}}(t))$. The matrices N_i , G_{1i} , G_{2i} , L_i , T_i and H_i will be described

hereafter. Define the state estimation error as $e_{v_i}(t) = x_{v_i}(t) - \hat{x}_{v_i}(t)$. Then

$$e_{v_i}(t) = (I + H_i Z^i \tilde{C}_i) x_{v_i}(t) - q_{vi}(t) + H_i V_{v_i} v_i(t),$$

where $\mathcal{D}_i(t) = \begin{pmatrix} d_{v_i}(t) \\ \phi(t) \end{pmatrix}$, $V_{v_i} = (Z^i \tilde{D}_{d_i} - X_i \ D_{\mathcal{F}_i})$

and $v_i(t) = \begin{pmatrix} \mathcal{D}_i(t) \\ \mathcal{F}_i(t) \end{pmatrix}$. Therefore, its dynamics is expressed as

$$\begin{aligned} \dot{e}_{v_i}(t) &= N_i e_{v_i}(t) + (T_i \tilde{A}_i - S_i Z^i \tilde{C}_i - N_i) x_{v_i}(t) + T_i \varphi_{v_i}^{e_{v_i}} \\ &\quad + (T_i \tilde{B}_{u_i} - G_{1i}) u_i(t) + S_i X_i \phi_i(t) - S_i D_{\mathcal{F}_i} \mathcal{F}_i(t) \quad (9) \\ &\quad + (T_i \tilde{B}_{d_i} - S_i Z^i \tilde{D}_{d_i}) d_{v_i}(t) + T_i \tilde{B}_{f_i} f_{va_i}(t) \\ &\quad + T_i \tilde{B}_{u_i} u_{v_i}(t) - G_{2i} ((\mathcal{A}_{u,i} \Delta \mathcal{A}_{u,i} + \mathcal{A}_{u,i}) u_{v_i}(t) \\ &\quad + D_{u_i} f_{u_i}(t)) + H_i V_{v_i} v_i(t) \end{aligned}$$

where

$$T_i = I + H_i Z^i \tilde{C}_i, \quad (10a)$$

$$S_i = L_i + N_i H_i, \quad (10b)$$

$\varphi_{v_i}^{e_{v_i}}(t) = \varphi_{v_i}(x_{v_i}(t)) - \varphi_{v_i}(\hat{x}_{v_i}(t))$, and

$$\begin{cases} f_{u_i}(t) = \text{Col}(f_{ii_1}^u(t), \dots, f_{ii_{N_i}}^u(t)), \\ D_{u_i} = \text{Blkdiag}(D_{u_{ii_1}}, \dots, D_{u_{ii_{N_i}}}), \\ \Delta \mathcal{A}_{u,i} = \text{diag}(\underbrace{\Delta a_{ii_1}, \dots, \Delta a_{ii_1}}_{n_u \text{ times}}, \dots, \Delta a_{ii_{N_i}}, \dots, \Delta a_{ii_{N_i}}), \\ \mathcal{A}_{u,i} = \text{diag}(\underbrace{a_{ii_1}, \dots, a_{ii_1}}_{n_u \text{ times}}, \dots, a_{ii_{N_i}}, \dots, a_{ii_{N_i}}). \end{cases}$$

with $v_i(t) = \Delta \mathcal{A}_i$. By imposing the following

$$H_i V_{v_i} = 0, \quad (11a)$$

$$T_i \tilde{A}_i - S_i Z^i \tilde{C}_i = N_i, \quad (11b)$$

$$T_i \tilde{B}_{u_i} - G_{1i} = 0, \quad (11c)$$

$$T_i \tilde{B}_{u_i} - G_{2i} \mathcal{A}_{u,i} = 0, \quad (11d)$$

(9) becomes

$$\begin{aligned} \dot{e}_{v_i}(t) &= N_i e_{v_i}(t) + (T_i \tilde{B}_{d_i} - S_i Z^i \tilde{D}_{d_i}) d_{v_i}(t) \\ &\quad + T_i \tilde{B}_{f_i} f_{va_i}(t) - S_i D_{\mathcal{F}_i} \mathcal{F}_i(t) + S_i X_i \phi_i(t) \\ &\quad - T_i \tilde{B}_{u_i} (\mathcal{A}_{u,i}^{-1} \Delta \mathcal{A}_{u,i}) u_{v_i}(t) \\ &\quad - T_i \tilde{B}_{u_i} \mathcal{A}_{u,i}^{-1} D_{u_i} f_{u_i}(t) + T_i \varphi_{v_i}^{e_{v_i}}(t). \end{aligned} \quad (12)$$

By setting new concatenated uncertainties vector as $\underline{\phi}_i(t) = \begin{pmatrix} \phi_i(t) \\ \Delta \mathcal{A}_{u,i} u_{v_i}(t) \end{pmatrix}$, the error dynamics becomes

$$\begin{aligned} \dot{e}_{v_i}(t) = & N_i e_{v_i}(t) + (T_i \tilde{B}_{d_i} - S_i Z^i \tilde{D}_{d_i}) d_{v_i}(t) \\ & + T_i \varphi_{v_i}^{e_{v_i}}(t) \\ & - S_i D_{\mathcal{F}_i} \mathcal{F}_i(t) + (S_i \underline{\mathbf{X}}_i - T_i \tilde{\mathbf{X}}_i) \underline{\phi}_i(t) \\ & - T_i \mathcal{B}_i \underline{\mathcal{F}}_i(t), \end{aligned} \quad (13)$$

where $\mathcal{B}_i = \begin{pmatrix} -\tilde{B}_{f_i} & \tilde{B}_{u_i} \mathcal{A}_{u,i}^{-1} D_{u_i} \end{pmatrix}$, $\underline{\mathcal{F}}_i(t) = \begin{pmatrix} f_{a_i}(t) \\ f_{u_i}(t) \end{pmatrix}$, $\underline{\mathbf{X}}_i = \begin{pmatrix} \mathbf{X}_i & 0_{n_z^i \times (n_u \cdot N_i)} \end{pmatrix}$, $\tilde{\mathbf{X}}_i = \begin{pmatrix} 0_{n_z^i \times n_z^i} & -\tilde{B}_{u_i} \end{pmatrix}$.

On the other hand, define the following residual vector

$$r_i(t) = W_i(z_{v_i}(t) - \hat{z}_{v_i}(t)), \quad (14)$$

where W_i is a pre-set post-residual gain matrix used to highlight the effects of the faults on the residual signals. In this work, since it does not directly affect the residual signals, it is considered that $\underline{\mathcal{F}}_i(t)$ affects the residual signals over a finite-frequency domain, which can be uniformly expressed as [44]

$$\Omega_{\underline{\mathcal{F}}_i} := \{\omega_f \in \mathbb{R} \mid \kappa(\omega_f - \omega_{f_1})(\omega_f - \omega_{f_2}) \leq 0\} \quad (15)$$

where $\kappa \in \{1, -1\}$, ω_{f_1} and ω_{f_2} are given positive scalars characterizing the frequency range of the fault vector $\underline{\mathcal{F}}_i$. Indeed, if one selects

– $\kappa = 1$ and $\omega_{f_1} < \omega_{f_2}$, then the set $\Omega_{\underline{\mathcal{F}}_i}$ corresponds to the middle frequency range

$$\Omega_{\underline{\mathcal{F}}_i} := \{\omega_f \in \mathbb{R} \mid \omega_{f_1} \leq \omega_f \leq \omega_{f_2}\}.$$

– $\kappa = 1$ and $-\omega_{f_1} = \omega_{f_2} = \omega_{f_l}$, then the set $\Omega_{\underline{\mathcal{F}}_i}$ corresponds to the low-frequency range

$$\Omega_{\underline{\mathcal{F}}_i} := \{\omega_f \in \mathbb{R} \mid |\omega_f| \leq \omega_{f_l}\}.$$

– $\kappa = -1$ and $-\omega_{f_1} = \omega_{f_2} = \omega_{f_h}$, then the set $\Omega_{\underline{\mathcal{F}}_i}$ corresponds to the high-frequency range

$$\Omega_{\underline{\mathcal{F}}_i} := \{\omega_f \in \mathbb{R} \mid |\omega_f| \geq \omega_{f_h}\}.$$

The objective here is to simultaneously achieve local state estimation (asymptotic stability of the error dynamics) and fault/attack detection. Theorems 1, 2 and 3 are proposed in this section to solve this problem through a set of matrix inequalities using the \mathcal{H}_∞ , \mathcal{H}_- performance indexes. Hence, to summarise, the proposed fault/attack detection scheme is obtained through simultaneously satisfying the following, for some performance scalar variables γ_i , $\varrho_i \beta_i$ and $\eta_i \forall i \in \{1, \dots, N\}$.

(i) To guarantee asymptotic stability of error dynamics (13).

(ii) To ensure a reasonable sensitivity of the residuals to the possible output attacks/faults over all frequency ranges, by satisfying

$$\|T_{r_{\mathcal{F}_i} \mathcal{F}_i}\|_- > \gamma_i, \quad (16)$$

where $r_{\mathcal{F}_i}$ is the residual signal defined for the case with no disturbance $d_{v_i} = 0$, no uncertainty $\underline{\phi}_i = 0$ and no fault $\underline{\mathcal{F}}_i = 0$.

(iii) To ensure a reasonable sensitivity of the residuals to the possible input attacks/faults over a finite-frequency range defined in the set $\Omega_{\underline{\mathcal{F}}_i}$, by satisfying

$$\|T_{r_{\underline{\mathcal{F}}_i} \underline{\mathcal{F}}_i}\|_- > \varrho_i, \quad (17)$$

for all solutions of (13) such that,

$$\int_0^\infty \left(\kappa(\omega_{f_1} e_{v_i}(t) + j \dot{e}_{v_i}(t))(\omega_{f_2} e_{v_i}(t) - j \dot{e}_{v_i}(t))^T \right) dt \leq 0, \quad (18)$$

where κ , ω_{f_1} , ω_{f_2} are as defined in $\Omega_{\underline{\mathcal{F}}_i}$, and $r_{\underline{\mathcal{F}}_i}$ is the residual signal defined for the case with no disturbance $d_{v_i} = 0$, no uncertainty $\underline{\phi}_i = 0$ and no fault $\mathcal{F}_i = 0$.

(iv) To guarantee a good disturbances and uncertainties rejection performance w.r.t. to the residual signals over all frequency ranges, i.e.

$$\|T_{r_{\mathcal{D}_i} d_{v_i}}\|_\infty < \eta_i, \quad \|T_{r_{\mathcal{D}_i} \underline{\phi}_i}\|_\infty < \beta_i, \quad (19)$$

where $r_{\mathcal{D}_i}$ is the residual signal defined without fault $\mathcal{F}_i = 0$ and $\underline{\mathcal{F}}_i = 0$.

For the rest of the manuscript, the time argument is omitted where it is not needed for clarity.

Theorem 1 For $d_{v_i} = 0$, $\underline{\phi}_i = 0$, $\underline{\mathcal{F}}_i = 0$, $\mathcal{F}_i \neq 0$, let γ_i , θ_{m_i} , σ_{1i} and ε_i be strictly positive scalars, error dynamics (13) is asymptotically stable and performance index (16) is guaranteed if $\forall i \in \{1, \dots, N\}$, there exist symmetric positive definite matrices P_i , matrices U_i , R_i and unstructured nonsingular matrices Y_i such that the following optimisation problem is solved

$$\begin{aligned} & \max_{P_i, Y_i, U_i, R_i} \gamma_i \\ & \text{subject to} \\ & \begin{pmatrix} \Psi_i^1 & \Psi_i^2 & \Psi_i^3 & \Psi_i^4 \\ * & \Psi_i^5 & 0 & \Psi_i^6 \\ * & * & -\varepsilon_i I & \Psi_i^7 \\ * & * & * & \Psi_i^8 \end{pmatrix} < 0, \end{aligned} \quad (20)$$

$$U_i V_{v_i} = 0, \quad (21)$$

where

$$\begin{aligned} \Psi_i^1 &= Y_i \tilde{A}_i + U_i Z^i \tilde{C}_i \tilde{A}_i - R_i Z^i \tilde{C}_i \\ &\quad + \tilde{A}_i^T Y_i^T + \tilde{A}_i^T (Z^i \tilde{C}_i)^T U_i^T - (Z^i \tilde{C}_i)^T R_i^T \\ &\quad + \varepsilon_i \theta_{m_i} I - (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i, \\ \Psi_i^2 &= -R_i D_{\mathcal{F}_i} - (Z^i \tilde{C}_i)^T W_i^T W_i D_{\mathcal{F}_i}, \\ \Psi_i^3 &= Y_i + U_i Z^i \tilde{C}_i, \\ \Psi_i^4 &= -Y_i + P_i + \sigma_{1i} \tilde{A}_i^T Y_i^T + \sigma_{1i} \tilde{A}_i^T (Z^i \tilde{C}_i)^T U_i^T \\ &\quad - \sigma_{1i} (Z^i \tilde{C}_i)^T R_i^T, \\ \Psi_i^5 &= -D_{\mathcal{F}_i}^T W_i^T W_i D_{\mathcal{F}_i} + \gamma_i^2 I, \\ \Psi_i^6 &= -\sigma_{1i} D_{\mathcal{F}_i}^T R_i^T, \\ \Psi_i^7 &= \sigma_{1i} Y_i^T + \sigma_{1i} (Z^i \tilde{C}_i)^T U_i^T, \\ \Psi_i^8 &= -\sigma_{1i} (Y_i + Y_i^T), \end{aligned}$$

and the observer gains are specified as

$$\begin{aligned} S_i &= Y_i^{-1} R_i, \\ H_i &= Y_i^{-1} U_i, \\ N_i &= (I + Y_i^{-1} U_i Z^i \tilde{C}_i) \tilde{A}_i - Y_i^{-1} R_i Z^i \tilde{C}_i, \\ G_{1i} &= (I + Y_i^{-1} U_i Z^i \tilde{C}_i) \tilde{B}_{u_i}, \\ G_{2i} &= (I + Y_i^{-1} U_i Z^i \tilde{C}_i) \tilde{B}_{u_i} A_{u_i}^{-1}, \\ L_i &= Y_i^{-1} R_i - N_i Y_i^{-1} U_i. \end{aligned} \quad (22)$$

Proof Performance index (16) corresponds to the following function

$$\mathcal{J}_{\mathcal{F}_i} = \int_0^\infty (r_{\mathcal{F}_i}^T r_{\mathcal{F}_i} - \gamma_i^2 \mathcal{F}_i^T \mathcal{F}_i) dt > 0. \quad (23)$$

Let us select the candidate Lyapunov function $V_i(e_{v_i}) = e_{v_i}^T P_i e_{v_i}$, then

$$\begin{aligned} \dot{V}(e_{v_i}) &= e_{v_i}^T (N_i^T P_i + P_i N_i) e_{v_i} + (\varphi_{v_i}^{e_{v_i}})^T T_i^T P_i e_{v_i} \\ &\quad + e_{v_i}^T P_i T_i \varphi_{v_i}^{e_{v_i}} + \mathcal{F}_i^T (-S_i D_{\mathcal{F}_i})^T P_i e_{v_i} \\ &\quad + e_{v_i}^T P_i (-S_i D_{\mathcal{F}_i}) \mathcal{F}_i. \end{aligned} \quad (24)$$

On the other hand, (23) can be expressed as

$$\begin{aligned} \mathcal{J}_{\mathcal{F}_i} &= \int_0^\infty ([e_{v_i}^T(t) (Z^i \tilde{C}_i)^T + \mathcal{F}_i^T(t) D_{\mathcal{F}_i}^T] W_i^T W_i \\ &\quad \times (Z^i \tilde{C}_i e_{v_i}(t) + D_{\mathcal{F}_i} \mathcal{F}_i(t)) \\ &\quad - \gamma_i^2 \mathcal{F}_i^T \mathcal{F}_i - \dot{V}(e_{v_i})) dt \\ &\quad + \int_0^\infty (\dot{V}(e_{v_i})) dt > 0. \end{aligned} \quad (25)$$

According to Assumption 2, it can be shown that

$$\begin{aligned} (\varphi_{v_i}^{e_{v_i}})^T \varphi_{v_i}^{e_{v_i}} &= \|\varphi_{v_i}^{e_{v_i}}\|^2 \leq \theta_i^2 \|x_i(t) - \hat{x}_i(t)\|^2 \\ &\quad + \theta_{i_1}^2 \|x_{i_1}(t) - \hat{x}_{i_1}(t)\|^2 + \dots \\ &\quad + \theta_{i_{N_i}}^2 \|x_{i_{N_i}}(t) - \hat{x}_{i_{N_i}}(t)\|^2 \\ &\leq \theta_{M_i} e_{v_i}^T e_{v_i}, \end{aligned} \quad (26)$$

where $\theta_{M_i} = \max(\theta_i^2, \theta_{i_1}^2, \dots, \theta_{i_{N_i}}^2)$.

Since $V(e_{v_i}) = e_{v_i}^T P_i e_{v_i} \geq 0$ and using Lemma 1 and equation (26), (25) can be shown to be equivalent to

$$\begin{pmatrix} \gamma_i - P_i S_i D_{\mathcal{F}_i} - (Z^i \tilde{C}_i)^T W_i^T W_i D_{\mathcal{F}_i} \\ \star & -D_{\mathcal{F}_i}^T W_i^T W_i D_{\mathcal{F}_i} + \gamma_i^2 I \end{pmatrix} < 0, \quad (27)$$

where $\gamma_i = N_i^T P_i + P_i N_i + \varepsilon_i \theta_{M_i} I + \varepsilon_i^{-1} P_i T_i T_i^T P_i - (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i$. Using the Schur complement, (27) can be re-written as

$$\mathcal{T}_{1i} + \mathcal{V}_{1i} \mathcal{S}_{1i} + \mathcal{S}_{1i}^T \mathcal{V}_{1i}^T < 0, \quad (28)$$

with

$$\mathcal{T}_{1i} = \begin{pmatrix} \varepsilon_i \theta_{M_i} I - (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i & -(Z^i \tilde{C}_i)^T W_i^T W_i D_{\mathcal{F}_i} & 0 \\ \star & -D_{\mathcal{F}_i}^T W_i^T W_i D_{\mathcal{F}_i} + \gamma_i^2 I & 0 \\ \star & \star & -\varepsilon_i I \end{pmatrix},$$

$$\mathcal{S}_{1i} = (N_i \quad -S_i D_{\mathcal{F}_i} \quad T_i), \quad \mathcal{V}_{1i} = \begin{pmatrix} P_i \\ 0 \\ 0 \end{pmatrix}.$$

Using the congruence transformation $(I \quad \mathcal{T}_{1i}^T)$, (28) is equivalent to

$$\begin{pmatrix} \mathcal{T}_{1i} + \mathcal{K}_{1i} \mathcal{S}_{1i} + \mathcal{S}_{1i}^T \mathcal{K}_{1i}^T - \mathcal{K}_{1i} + \mathcal{V}_{1i} + \mathcal{S}_{1i}^T \mathcal{Y}_{1i}^T \\ \star & -(\mathcal{Y}_{1i} + \mathcal{Y}_{1i}^T) \end{pmatrix} < 0, \quad (29)$$

for new general matrices \mathcal{K}_{1i} and \mathcal{Y}_{1i} . Hence, by selecting

$$\mathcal{K}_{1i}^T = (Y_i^T \quad 0 \quad 0), \quad \mathcal{Y}_{1i} = \sigma_{1i} Y_i,$$

for a scalar σ_{1i} and a nonsingular general matrix Y_i , one can obtain the following sufficient condition

$$\begin{pmatrix} \Pi_i^1 & \Pi_i^2 & Y_i T_i & \Pi_i^3 \\ \star & \Pi_i^4 & 0 & \Pi_i^5 \\ \star & \star & -\varepsilon_i I & \sigma_{1i} T_i^T Y_i^T \\ \star & \star & \star & -\sigma_{1i} (Y_i + Y_i^T) \end{pmatrix} < 0,$$

with

$$\begin{aligned} \Pi_i^1 &= Y_i N_i + N_i^T Y_i^T + \varepsilon_i \theta_{M_i} I \\ &\quad - (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i, \\ \Pi_i^2 &= -Y_i S_i D_{\mathcal{F}_i} - (Z^i \tilde{C}_i)^T W_i^T W_i D_{\mathcal{F}_i}, \\ \Pi_i^3 &= -Y_i + P_i + \sigma_{1i} N_i^T Y_i^T, \\ \Pi_i^4 &= -D_{\mathcal{F}_i}^T W_i^T W_i D_{\mathcal{F}_i} + \gamma_i^2 I, \\ \Pi_i^5 &= -\sigma_{1i} D_{\mathcal{F}_i}^T S_i^T Y_i^T. \end{aligned}$$

Replacing N_i and T_i with their respective values, and applying the linearising change of variables $U_i = Y_i H_i$, $R_i = Y_i S_i$, (20) is obtained. Furthermore, pre-multiplying (11a) with Y_i yields (21). Therefore, solving (20) under imposed constraints (21) and using observer gains (22) guarantees residual performance index (16) and the asymptotic stability of error dynamics (9). \square

Theorem 2 For $d_{v_i} = 0$, $\phi_i = 0$, $\mathcal{F}_i = 0$, $\mathcal{F}_i \neq 0$, let ϱ_i , θ_{M_i} , σ_{2i} and ε_i be strictly positive scalars, an arbitrary design matrix K_i , error dynamics (13) is asymptotically stable and performance index (17) is guaranteed if $\forall i \in \{1, \dots, N\}$ over a finite-frequency domain defined in (15), there exist symmetric positive definite matrices X_i , symmetric matrices \mathcal{X}_i , matrices U_i , R_i and unstructured nonsingular matrices Y_i such that the following optimisation problem is solved

$$\begin{aligned} & \max_{X_i, \mathcal{X}_i, Y_i, U_i, R_i} \varrho_i \\ & \text{subject to} \\ & \begin{pmatrix} \Sigma_i^1 & \Sigma_i^2 & \Sigma_i^3 & \Sigma_i^4 \\ * & \Sigma_i^5 & \Sigma_i^6 & \Sigma_i^7 \\ * & * & -\varepsilon_i I & \Sigma_i^8 \\ * & * & * & \Sigma_i^9 \end{pmatrix} < 0, \\ & \kappa \mathcal{X}_i \geq 0, \end{aligned} \quad (30)$$

where

$$\begin{aligned} \Sigma_i^1 &= Y_i \tilde{A}_i + U_i Z^i \tilde{C}_i \tilde{A}_i - R_i Z^i \tilde{C}_i + \tilde{A}_i^T Y_i^T \\ &+ (Z^i \tilde{C}_i \tilde{A}_i)^T U_i^T - (Z^i \tilde{C}_i)^T R_i^T - \omega_{f_1} \omega_{f_2} \mathcal{X}_i \\ &+ \varepsilon_i \theta_{M_i} I - (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i, \\ \Sigma_i^2 &= -U_i Z^i \tilde{C}_i \tilde{B}_i + \tilde{A}_i^T Y_i^T K_i^T \\ &+ (Z^i \tilde{C}_i \tilde{A}_i)^T U_i^T K_i^T - (Z^i \tilde{C}_i)^T R_i^T K_i^T, \\ \Sigma_i^3 &= Y_i + U_i Z^i \tilde{C}_i, \\ \Sigma_i^4 &= -Y_i + X_i - j \omega_{f_a} \mathcal{X}_i + \sigma_{2i} \tilde{A}_i^T Y_i^T \\ &+ \sigma_{2i} (Z^i \tilde{C}_i \tilde{A}_i)^T U_i^T - \sigma_{2i} (Z^i \tilde{C}_i)^T R_i^T, \\ \Sigma_i^5 &= \varrho_i^2 I - K_i Y_i \tilde{B}_i - K_i U_i Z^i \tilde{C}_i \tilde{B}_i \\ &- \mathcal{B}_i^T Y_i^T K_i^T - \mathcal{B}_i^T (Z^i \tilde{C}_i)^T U_i^T K_i^T, \\ \Sigma_i^6 &= K_i Y_i + K_i U_i Z^i \tilde{C}_i, \\ \Sigma_i^7 &= -K_i Y_i - \sigma_{2i} \mathcal{B}_i^T Y_i^T - \sigma_{2i} \mathcal{B}_i^T (Z^i \tilde{C}_i)^T U_i^T, \\ \Sigma_i^8 &= \sigma_{2i} Y_i^T + \sigma_{2i} (Z^i \tilde{C}_i)^T U_i^T, \\ \Sigma_i^9 &= -(\mathcal{X}_i + \sigma_{2i} Y_i + \sigma_{2i} Y_i^T), \end{aligned}$$

and $\mathcal{B}_i = (-\tilde{B}_{f_i} \tilde{B}_{u_i} A_{u_i}^{-1} D_{u_i})$. The observer gains are then computed as in (22).

Proof Let us select the candidate Lyapunov function $V_i(e_{v_i}) = e_{v_i}^T X_i e_{v_i}$, then

$$\begin{aligned} \dot{V}(e_{v_i}) &= e_{v_i}^T (N_i^T X_i + X_i N_i) e_{v_i} + (\varphi_{v_i}^{e_{v_i}})^T T_i^T X_i e_{v_i} \\ &+ e_{v_i}^T X_i T_i \varphi_{v_i}^{e_{v_i}} - \mathcal{F}_i^T (T_i \mathcal{B}_i)^T X_i e_{v_i} \\ &- e_{v_i}^T X_i (T_i \mathcal{B}_i) \mathcal{F}_i. \end{aligned} \quad (31)$$

To solve (17) over a finite-frequency domain as defined in (15), one could define the following function

$$\begin{aligned} \mathcal{J}_{\mathcal{F}_i} &= \int_0^\infty \left(\varrho_i^2 \mathcal{F}_i^T \mathcal{F}_i - r_{\mathcal{F}_i}^T r_{\mathcal{F}_i} - \text{tr}(\mathbf{He}(\mathcal{W}_i) \mathcal{X}_i) \right. \\ &\left. + \dot{V}(e_{v_i}) \right) dt < 0, \end{aligned} \quad (32)$$

where $\mathcal{W}_i = (\omega_{f_1} e_{v_i} + j \dot{e}_{v_i})(\omega_{f_2} e_{v_i} + j \dot{e}_{v_i})^*$ and \mathcal{X}_i is a symmetric matrix. From (18), one gets

$$\int_0^\infty \kappa \mathcal{W}_i dt \leq 0.$$

Moreover, it can be shown through the Parseval's theorem [45] that

$$\begin{aligned} \int_0^\infty \mathcal{W}_i dt &= \frac{1}{2\pi} \int_{-\infty}^{+\infty} \left((\omega_{f_1} - \omega)(\omega_{f_2} \right. \\ &\left. - \omega) \check{\mathbf{e}}_i(\omega) \check{\mathbf{e}}_i^T(\omega) \right) d\omega, \end{aligned}$$

where $\check{\mathbf{e}}_i(\omega)$ is the Fourier transform of $e_{v_i}(t)$. Choosing \mathcal{X}_i such that $\kappa \mathcal{X}_i \geq 0$, it yields

$$\text{tr}((\int_0^\infty \mathcal{W}_i dt)^* \mathcal{X}_i) + \text{tr}((\int_0^\infty \mathcal{W}_i dt) \mathcal{X}_i) \leq 0,$$

or equivalently, $\text{tr}(\mathbf{He}(\mathcal{W}_i) \mathcal{X}_i) \leq 0$. Therefore, (17) is guaranteed for all solutions of (13) satisfying (18), if

$$\varrho_i^2 \mathcal{F}_i^T \mathcal{F}_i - r_{\mathcal{F}_i}^T r_{\mathcal{F}_i} + \dot{V}(e_{v_i}) - \text{tr}(\mathbf{He}(\mathcal{W}_i) \mathcal{X}_i) < 0 \quad (33)$$

By setting $\omega_{f_a} = \frac{\omega_{f_1} + \omega_{f_2}}{2}$, then

$$\begin{aligned} & -\text{tr}(\mathbf{He}(\mathcal{W}_i) \mathcal{X}_i) \\ &= -e_{v_i}^T \omega_{f_1} \omega_{f_2} \mathcal{X}_i e_{v_i} - \dot{e}_{v_i}^T \mathcal{X}_i \dot{e}_{v_i} - e_{v_i}^T j \omega_{f_a} \mathcal{X}_i \dot{e}_{v_i} \\ &+ \dot{e}_{v_i}^T j \omega_{f_a} \mathcal{X}_i e_{v_i} \\ &= -e_{v_i}^T \omega_{f_1} \omega_{f_2} \mathcal{X}_i e_{v_i} - e_{v_i}^T N_i^T \mathcal{X}_i N_i e_{v_i} \\ &- (\varphi_{v_i}^{e_{v_i}})^T T_i^T \mathcal{X}_i N_i e_{v_i} + \mathcal{F}_i^T \mathcal{B}_i^T T_i^T \mathcal{X}_i N_i e_{v_i} \\ &- e_{v_i}^T N_i^T \mathcal{X}_i T_i \varphi_{v_i}^{e_{v_i}} - (\varphi_{v_i}^{e_{v_i}})^T T_i^T \mathcal{X}_i T_i \varphi_{v_i}^{e_{v_i}} \\ &+ \mathcal{F}_i^T \mathcal{B}_i^T T_i^T \mathcal{X}_i T_i \varphi_{v_i}^{e_{v_i}} + e_{v_i}^T N_i^T \mathcal{X}_i T_i \mathcal{B}_i \mathcal{F}_i \\ &+ (\varphi_{v_i}^{e_{v_i}})^T T_i^T \mathcal{X}_i T_i \mathcal{B}_i \mathcal{F}_i - \mathcal{F}_i^T \mathcal{B}_i^T T_i^T \mathcal{X}_i T_i \mathcal{B}_i \mathcal{F}_i \\ &- e_{v_i}^T j \omega_{f_a} \mathcal{X}_i T_i \varphi_{v_i}^{e_{v_i}} + e_{v_i}^T j \omega_{f_a} \mathcal{X}_i T_i \mathcal{B}_i \mathcal{F}_i \\ &- e_{v_i}^T j \omega_{f_a} N_i e_{v_i} \\ &+ e_{v_i}^T N_i^T j \omega_{f_a} \mathcal{X}_i e_{v_i} + (\varphi_{v_i}^{e_{v_i}})^T T_i^T j \omega_{f_a} \mathcal{X}_i e_{v_i} \\ &- \mathcal{F}_i^T \mathcal{B}_i^T T_i^T j \omega_{f_a} \mathcal{X}_i e_{v_i}. \end{aligned} \quad (34)$$

On the other hand, using Lemma 1 and (26), one has

$$\begin{aligned} \dot{V}(e_{v_i}) &< e_{v_i}^T (N_i^T X_i + X_i N_i + \varepsilon_i \theta_{M_i} I \\ &\quad + \varepsilon_i^{-1} X_i T_i T_i^T X_i) e_{v_i} - \underline{\mathcal{F}}_i^T (T_i \mathcal{B}_i)^T X_i e_{v_i} \\ &\quad - e_{v_i}^T X_i (T_i \mathcal{B}_i) \underline{\mathcal{F}}_i. \end{aligned} \quad (35)$$

Replacing (34) and (35) into (33) gives

$$\begin{pmatrix} \mathcal{E}_{1i}^1 & \mathcal{E}_{1i}^2 & \mathcal{E}_{1i}^3 \\ * & \mathcal{E}_{1i}^4 & \mathcal{E}_{1i}^5 \\ * & * & \mathcal{E}_{1i}^6 \end{pmatrix} < 0, \quad (36)$$

where

$$\begin{aligned} \mathcal{E}_{1i}^1 &= -\omega_{f_1} \omega_{f_2} \mathcal{X}_i - N_i^T \mathcal{X}_i N_i - j \omega_{f_a} \mathcal{X}_i N_i \\ &\quad + j \omega_{f_a} N_i^T \mathcal{X}_i \\ &\quad + N_i^T X_i + X_i N_i + \varepsilon_i \theta_{M_i} I \\ &\quad - (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i, \\ \mathcal{E}_{1i}^2 &= N_i^T \mathcal{X}_i T_i \mathcal{B}_i + j \omega_{f_a} \mathcal{X}_i T_i \mathcal{B}_i - X_i T_i \mathcal{B}_i, \\ \mathcal{E}_{1i}^3 &= -N_i^T \mathcal{X}_i T_i - j \omega_{f_a} \mathcal{X}_i T_i + X_i T_i, \\ \mathcal{E}_{1i}^4 &= -\mathcal{B}_i^T T_i^T \mathcal{X}_i T_i \mathcal{B}_i + \varrho_i^2 I, \\ \mathcal{E}_{1i}^5 &= \mathcal{B}_i^T T_i^T \mathcal{X}_i T_i, \\ \mathcal{E}_{1i}^6 &= -T_i^T \mathcal{X}_i T_i - \varepsilon_i I. \end{aligned}$$

It can be re-written as

$$\mathcal{T}_{2i} + \mathcal{V}_{2i} \mathcal{S}_{2i} + \mathcal{S}_{2i}^T \mathcal{V}_{2i}^T - \mathcal{S}_{2i}^T \mathcal{X}_i \mathcal{S}_{2i} < 0, \quad (37)$$

with

$$\mathcal{T}_{2i} = \begin{pmatrix} -\omega_{f_1} \omega_{f_2} \mathcal{X}_i + \varepsilon_i \theta_{M_i} I - (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i & 0 & 0 \\ * & \varrho_i^2 I & 0 \\ * & * & -\varepsilon_i I \end{pmatrix},$$

$$\mathcal{S}_{2i} = (N_i - T_i \mathcal{B}_i \ T_i), \quad \mathcal{V}_{2i} = \begin{pmatrix} X_i - j \omega_{f_a} \mathcal{X}_i \\ 0 \\ 0 \end{pmatrix}.$$

Similar to Theorem 1, (37) can be shown to be equivalent to

$$\begin{pmatrix} \mathcal{T}_{2i} + \mathcal{K}_{2i} \mathcal{S}_{2i} + \mathcal{S}_{2i}^T \mathcal{K}_{2i}^T - \mathcal{K}_{2i} + \mathcal{V}_{2i} + \mathcal{S}_{2i}^T \mathcal{Y}_{2i}^T \\ * & -(\mathcal{X}_i + \mathcal{Y}_{2i} + \mathcal{Y}_{2i}^T) \end{pmatrix} < 0, \quad (38)$$

for new general matrices \mathcal{K}_{2i} and \mathcal{Y}_{2i} . Hence, by selecting

$$\mathcal{K}_{2i}^T = (Y_i^T \ Y_i^T K_i^T \ 0), \quad \mathcal{Y}_{2i} = \sigma_{2i} Y_i,$$

for a scalar σ_{2i} , an arbitrary matrix K_i and a nonsingular general matrix Y_i , one can obtain the following

sufficient condition

$$\begin{pmatrix} \mathcal{E}_{2i}^1 & \mathcal{E}_{2i}^2 & Y_i T_i & \mathcal{E}_{2i}^3 \\ * & \mathcal{E}_{2i}^4 & K_i Y_i T_i & \mathcal{E}_{2i}^5 \\ * & * & -\varepsilon_i I & \sigma_{2i} T_i^T Y_i^T \\ * & * & * & \mathcal{E}_{2i}^6 \end{pmatrix} < 0,$$

with

$$\begin{aligned} \mathcal{E}_{2i}^1 &= Y_i N_i + N_i^T Y_i^T - \omega_{f_1} \omega_{f_2} \mathcal{X}_i + \varepsilon_i \theta_{M_i} I \\ &\quad - (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i, \\ \mathcal{E}_{2i}^2 &= -Y_i T_i \mathcal{B}_i + N_i^T Y_i^T K_i^T, \\ \mathcal{E}_{2i}^3 &= -Y_i + X_i - j \omega_{f_a} \mathcal{X}_i + \sigma_{2i} N_i^T Y_i^T, \\ \mathcal{E}_{2i}^4 &= \varrho_i^2 I - K_i Y_i T_i \mathcal{B}_i - \mathcal{B}_i^T T_i^T Y_i^T K_i^T, \\ \mathcal{E}_{2i}^5 &= -K_i Y_i - \sigma_{2i} \mathcal{B}_i^T T_i^T Y_i^T, \\ \mathcal{E}_{2i}^6 &= -(\mathcal{X}_i + \sigma_{2i} Y_i + \sigma_{2i} Y_i^T). \end{aligned}$$

By replacing N_i and T_i with their respective values, and applying the linearising change of variables $U_i = Y_i H_i$, $R_i = Y_i S_i$, (30) is obtained. This guarantees residual performance index (17) and the asymptotic stability of error dynamics (9). \square

Remark 4 Given that LMIs (30) $\forall i$ are in the complex domain, most solvers cannot directly handle them. Hence, the following equivalent statements are used for a complex Hermitian matrix $L(x)$

1. $L(x) < 0$.
2. $\begin{pmatrix} \text{Re}(L(x)) & \text{Im}(L(x)) \\ -\text{Im}(L(x)) & \text{Re}(L(x)) \end{pmatrix} < 0$.

where $\text{Re}(L(x))$ represents the real part of $L(x)$ and $\text{Im}(L(x))$ its imaginary part. More details can be found in [46].

Theorem 3 For $\mathcal{F}_i = 0$, $\underline{\mathcal{F}}_i = 0$, $d_{v_i} \neq 0$, $\phi_i \neq 0$, let β_i , η_i , θ_{M_i} , σ_{3i} and ε_i be strictly positive scalars, error dynamics (13) is asymptotically stable and performance indexes (19) are guaranteed if $\forall i \in \{1, \dots, N\}$, there exist symmetric positive definite matrices \mathcal{Q}_i , matrices U_i , R_i and unstructured nonsingular matrices Y_i such that for all possible uncertainties, under imposed constraint (21)

$$\min_{\mathcal{Q}_i, Y_i, U_i, R_i} \beta_i + \eta_i$$

subject to

$$\begin{pmatrix} \Phi_i^1 & \Phi_i^2 & \Phi_i^3 & \Phi_i^4 & \Phi_i^5 \\ * & \Phi_i^6 & \Phi_i^7 & 0 & \Phi_i^8 \\ * & * & \Phi_i^9 & 0 & \Phi_i^{10} \\ * & * & * & -\varepsilon_i I & \Phi_i^{11} \\ * & * & * & * & \Phi_i^{12} \end{pmatrix} < 0, \quad (39)$$

where

$$\begin{aligned}
\Phi_i^1 &= Y_i \tilde{A}_i + U_i Z^i \tilde{C}_i \tilde{A}_i - R_i Z^i \tilde{C}_i + \tilde{A}_i^T Y_i^T \\
&\quad + \varepsilon_i \theta_{M_i} I + (Z^i \tilde{C}_i \tilde{A}_i)^T U_i^T - (Z^i \tilde{C}_i)^T R_i^T \\
&\quad + (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i, \\
\Phi_i^2 &= Y_i \tilde{B}_{d_i} + U_i Z^i \tilde{C}_i \tilde{B}_{d_i} - R_i Z^i \tilde{D}_{d_i} \\
&\quad + Z^i \tilde{C}_i W_i^T W_i Z^i \tilde{D}_{d_i}, \\
\Phi_i^3 &= R_i \underline{X}_i - Y_i \tilde{X}_i \\
&\quad - U_i Z^i \tilde{C}_i \tilde{X}_i - (Z^i \tilde{C}_i)^T W_i^T W_i \underline{X}_i, \\
\Phi_i^4 &= Y_i + Y_i H_i Z^i \tilde{C}_i, \\
\Phi_i^5 &= -Y_i + Q_i + \sigma_{3i} \tilde{A}_i^T Y_i^T + \sigma_{3i} (Z^i \tilde{C}_i \tilde{A}_i)^T U_i^T \\
&\quad - \sigma_{3i} (Z^i \tilde{C}_i)^T R_i^T, \\
\Phi_i^6 &= (Z^i \tilde{D}_{d_i})^T W_i^T W_i Z^i \tilde{D}_{d_i} - \eta_i^2 I, \\
\Phi_i^7 &= -\underline{X}_i^T W_i^T W_i Z^i \tilde{D}_{d_i}, \\
\Phi_i^8 &= \sigma_{3i} \tilde{B}_{d_i}^T Y_i^T \\
&\quad + \sigma_{3i} \tilde{B}_{d_i}^T (Z^i \tilde{C}_i)^T U_i^T - \sigma_{3i} Z^i \tilde{D}_{d_i}^T R_i^T, \\
\Phi_i^9 &= \underline{X}_i^T W_i^T W_i \underline{X}_i - \beta_i^2 I, \\
\Phi_i^{10} &= \sigma_{3i} \underline{X}_i^T R_i^T - \sigma_{3i} \tilde{X}_i^T Y_i^T - \sigma_{3i} \tilde{X}_i^T (Z^i \tilde{C}_i)^T U_i^T, \\
\Phi_i^{11} &= \sigma_{3i} Y_i^T + \sigma_{3i} (Z^i \tilde{C}_i)^T U_i^T, \\
\Phi_i^{12} &= -\sigma_{3i} (Y_i + Y_i^T).
\end{aligned}$$

The observer gains are then computed as in (22).

Proof Let us select the candidate Lyapunov function $V_i(e_{v_i}) = e_{v_i}^T Q_i e_{v_i}$, then

$$\begin{aligned}
\dot{V}(e_{v_i}) &= e_{v_i}^T (N_i^T Q_i + Q_i N_i) e_{v_i} + (\varphi_{v_i}^{e_{v_i}})^T T_i^T Q_i e_{v_i} \\
&\quad + e_{v_i}^T Q_i T_i \varphi_{v_i}^{e_{v_i}} + \phi_i^T(t) (S_i \underline{X}_i - T_i \tilde{X}_i)^T Q_i e_{v_i} \\
&\quad + e_{v_i}^T Q_i (S_i \underline{X}_i - T_i \tilde{X}_i) \phi_i(t) \\
&\quad + d_{v_i}^T (T_i \tilde{B}_{d_i} - S_i Z^i \tilde{D}_{d_i})^T Q_i e_{v_i} \\
&\quad + e_{v_i}^T Q_i (T_i \tilde{B}_{d_i} - S_i Z^i \tilde{D}_{d_i}) d_{v_i}(t).
\end{aligned} \quad (40)$$

The performance index is equivalent to

$$\mathcal{J}_{\mathcal{D}_i} = \int_0^\infty (r_{\mathcal{D}_i}^T r_{\mathcal{D}_i} - \beta_i^2 \phi_i^T \phi_i - \eta_i^2 d_{v_i}^T d_{v_i}) dt < 0. \quad (41)$$

Combining the two yields

$$\begin{aligned}
\mathcal{J}_{\mathcal{D}_i} &= \int_0^\infty ([e_{v_i}^T (Z^i \tilde{C}_i)^T \\
&\quad + d_{v_i}^T (Z^i \tilde{D}_{d_i})^T] W_i^T W_i [Z^i \tilde{C}_i e_{v_i}(t)
\end{aligned}$$

$$\begin{aligned}
&\quad + Z^i \tilde{D}_{d_i} d_{v_i}(t)] \\
&\quad - \eta_i^2 d_{v_i}^T d_{v_i} - e_{v_i}^T (Z^i \tilde{C}_i)^T W_i^T W_i \underline{X}_i \phi_i(t) \\
&\quad - d_{v_i}^T (Z^i \tilde{D}_{d_i})^T W_i^T W_i \underline{X}_i \phi_i(t) - \beta_i^2 \phi_i^T \phi_i \\
&\quad + \phi_i^T \underline{X}_i^T W_i^T W_i \underline{X}_i \phi_i - \phi_i^T \underline{X}_i^T W_i W_i^T Z^i \tilde{C}_i e_{v_i} \\
&\quad - \phi_i^T \underline{X}_i^T W_i^T W_i Z^i \tilde{D}_{d_i} d_{v_i} + \dot{V}(e_{v_i})) dt \\
&\quad - \int_0^\infty \dot{V}(e_{v_i}) dt \\
&< 0. \quad (42)
\end{aligned}$$

The above inequality can be expressed as

$$\begin{pmatrix} \Gamma_{i1} & \Gamma_{i2} + \Upsilon_i^{de} \\ \star & \Upsilon_i^{dd} \end{pmatrix} < 0,$$

where $\Gamma_{i1} = N_i^T Q_i + Q_i N_i + (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i + \varepsilon_i \theta_{M_i} I + \varepsilon_i^{-1} Q_i T_i T_i^T Q_i$, $\Gamma_{i2} = Q_i (T_i \tilde{B}_{d_i} - S_i Z^i \tilde{D}_{d_i} (S_i \underline{X}_i - T_i \tilde{X}_i))$, $\Upsilon_i^{de} = (Z^i \tilde{C}_i W_i^T W_i Z^i \tilde{D}_{d_i} - (Z^i \tilde{C}_i)^T W_i^T W_i \underline{X}_i)$ and $\Upsilon_i^{dd} = \begin{pmatrix} (Z^i \tilde{D}_{d_i})^T W_i^T W_i Z^i \tilde{D}_{d_i} - \eta_i^2 I & -\underline{X}_i^T W_i^T W_i Z^i \tilde{D}_{d_i} \\ \star & \underline{X}_i^T W_i^T W_i \underline{X}_i - \beta_i^2 I \end{pmatrix}$.

Similar to Theorem 1, the above is equivalent to

$$\mathcal{T}_{3i} + \mathcal{V}_{3i} \mathcal{S}_{3i} + \mathcal{S}_{3i}^T \mathcal{V}_{3i}^T < 0, \quad (43)$$

where

$$\begin{aligned}
\mathcal{T}_{3i} &= \begin{pmatrix} (Z^i \tilde{C}_i)^T W_i^T W_i Z^i \tilde{C}_i + \varepsilon_i \theta_{M_i} I & Z^i \tilde{C}_i W_i^T W_i Z^i \tilde{D}_{d_i} \\ * & (Z^i \tilde{D}_{d_i})^T W_i^T W_i Z^i \tilde{D}_{d_i} - \eta_i^2 I \\ * & * \\ * & * \end{pmatrix} \\
&\quad - \begin{pmatrix} (Z^i \tilde{C}_i)^T W_i^T W_i \underline{X}_i & 0 \\ -\underline{X}_i^T W_i^T W_i Z^i \tilde{D}_{d_i} & 0 \\ \underline{X}_i^T W_i^T W_i \underline{X}_i - \beta_i^2 I & 0 \\ * & -\varepsilon_i I \end{pmatrix}, \\
\mathcal{S}_{3i} &= \begin{pmatrix} N_i & T_i \tilde{B}_{d_i} - S_i Z^i \tilde{D}_{d_i} & S_i \underline{X}_i - T_i \tilde{X}_i & T_i \end{pmatrix}, \\
\mathcal{V}_{3i} &= \begin{pmatrix} Q_i \\ 0 \\ 0 \\ 0 \end{pmatrix}.
\end{aligned}$$

By selecting

$$\mathcal{K}_{3i}^T = (Y_i^T \ 0 \ 0 \ 0), \quad \mathcal{V}_{3i} = \sigma_{3i} Y_i,$$

for a scalar σ_{3i} and a nonsingular general matrix Y_i , one can obtain the following sufficient condition

$$\begin{pmatrix} \Lambda_i^1 & \Lambda_i^2 & \Lambda_i^3 & Y_i T_i & \Lambda_i^4 \\ * & \Lambda_i^5 & -\underline{X}_i^T W_i^T W_i Z^i \tilde{D}_{d_i} & 0 & \Lambda_i^6 \\ \star & * & \Lambda_i^7 & 0 & \Lambda_i^8 \\ * & * & * & -\varepsilon_i I & \sigma_{3i} T_i^T Y_i^T \\ * & * & * & * & -\sigma_{3i} (Y_i + Y_i^T) \end{pmatrix} < 0,$$

where

$$\begin{aligned}
\Lambda_i^1 &= Y_i N_i + N_i^T Y_i^T + (Z^i \tilde{C}_i)^T W_i^T Z^i \tilde{C}_i + \varepsilon_i \theta_{M_i} I, \\
\Lambda_i^2 &= Y_i T_i \tilde{B}_{d_i} - Y_i S_i Z^i \tilde{D}_{d_i} + Z^i \tilde{C}_i W_i^T W_i Z^i \tilde{D}_{d_i}, \\
\Lambda_i^3 &= Y_i S_i \tilde{X}_i - Y_i T_i \tilde{X}_i - (Z^i \tilde{C}_i)^T W_i^T W_i \tilde{X}_i, \\
\Lambda_i^4 &= -Y_i + Q_i + \sigma_{3i} N_i^T Y_i^T, \\
\Lambda_i^5 &= (Z^i \tilde{D}_{d_i})^T W_i^T W_i Z^i \tilde{D}_{d_i} - \eta_i^2 I, \\
\Lambda_i^6 &= \sigma_{3i} \tilde{B}_{d_i}^T T_i^T Y_i^T - \sigma_{3i} Z^i \tilde{D}_{d_i}^T S_i^T Y_i^T, \\
\Lambda_i^7 &= \tilde{X}_i^T W_i^T W_i \tilde{X}_i - \beta_i^2 I, \\
\Lambda_i^8 &= \sigma_{3i} \tilde{X}_i^T S_i^T Y_i^T - \sigma_{3i} \tilde{X}_i^T T_i^T Y_i^T.
\end{aligned}$$

Replacing N_i and T_i with their respective values, and applying the linearising change of variables $U_i = Y_i H_i$, $R_i = Y_i S_i$, (39) is obtained. This guarantees residual performance index (19) and the asymptotic stability of error dynamics (9). \square

Remark 5 One could note that it is possible to relax constraint (21). Indeed, this equality constraint implies that the span of the rows of U_i is included in $\ker(V_{v_i})$. Hence, one could turn this into a minimisation of its maximum singular value which could be minimised, i.e. for a scalar $\vartheta_i > 0$

$$\min_{U_i} \vartheta_i$$

subject to

$$-\vartheta_i I + U_i V_{v_i} \vartheta_i^{-1} (U_i V_{v_i})^T < 0. \quad (44)$$

Applying the Schur complement to (44) yields the following LMI

$$\begin{pmatrix} \vartheta_i I & U_i V_{v_i} \\ * & \vartheta_i I \end{pmatrix} < 0. \quad (45)$$

Remark 6 Note that here, as opposed to what is typically done in literature, we do not impose that $T_i \tilde{B}_{d_i} - S_i Z^i \tilde{D}_{d_i} = S_i \tilde{X}_i = 0$. Indeed, maintaining this constraint while solving the proposed inequalities can be unfeasable for some systems. Contrary to other works using unknown input observer, our approach does not require invertibility conditions except on Y_i which is inherently required by the proposed LMIs. Thus, no rank condition is required for the existence of the unknown input observer to solve the LMIs.

Residual evaluation

In order to isolate the faulty element (the specific faulty agent and/or faulty link), the residuals are evaluated by comparing them with an offline computed threshold defined hereafter. For this purpose, let us select the

following root-mean-square evaluation functions [41], $\forall p \in \mathcal{N}_i \cup i$

$$\begin{aligned}
J_{i,p}^e(t) &= \|r_i^p(t)\|_{\text{rms}} \\
&= \left(\frac{1}{T_w} \int_t^{t+T_w} (r_i^p(\tau))^T r_i^p(\tau) d\tau \right)^{\frac{1}{2}}, \quad (46)
\end{aligned}$$

where T_w is a finite evaluation window with

$$r_{v_i}^T(t) = [(r_i^i(t))^T, (r_i^{i_1}(t))^T, \dots, (r_i^{i_{N_i}}(t))^T],$$

and $r_i^p(t) \in \mathbb{R}^{n_y}$, $\forall p \in \mathcal{N}_i \cup i$. Noise, disturbances, communication uncertainties (etc.) are treated as unstructured unknown inputs, and the RMS threshold is computed as

$$J_{i_{pth}}^e = \sup_{\text{attack/fault free}} \|r_i^p(t)\|_{\text{rms}}, \quad (47)$$

where one could set $J_{i_{th}}^e = \max\{J_{i_{th}}^e, \dots, J_{i_{N_i th}}^e\}$. For isolation purpose, let us define the secure detection flags π_i , such that if $J_{i,i}^e(t) \leq J_{i_{th}}^e$ then $\pi_i = 0$ and $\pi_i = 1$ when $J_{i,i}^e(t) > J_{i_{th}}^e$. An agent i is assumed to request the secure detection flag of its neighbours when a fault or an attack has been detected through the generated residual functions $J_{i,j}^e(t)$, $j \in \mathcal{N}_i$.

In order to summarise the proposed scheme, two algorithms are proposed hereafter. Optimisation Algorithm 1 is ran offline and proposes steps to compute the observer matrix gains using a finite-frequency mixed $\mathcal{H}_\infty/\mathcal{H}_-$ approach by simultaneously combining Theorems 1–3 and Remark 5. Define the multi-objective cost function

$$s_i = \frac{\lambda_{i1} \eta_i + \lambda_{i2} \beta_i + \lambda_{i3} \vartheta_i}{\lambda_{i4} \gamma_i + \lambda_{i5} \varrho_i}, \quad (48)$$

where $\lambda_{i1}, \lambda_{i2}, \lambda_{i3}, \lambda_{i4}, \lambda_{i5}$ are positive trade-off weighing constants.

Algorithm 1: Observer–Detector module parameter computation at agent i (offline)

1. Construct local model (7)
 2. Define $\Omega_{\mathcal{F}_i}$ and choose the multi-objective weights $\lambda_{i1}, \lambda_{i2}, \lambda_{i3}, \lambda_{i4}$ and λ_{i5} ,
 3. Set $\sigma_{1i}, \sigma_{2i}, \sigma_{3i}, W_i, K_i$ and ε_i ,
 4. Minimise s_i by simultaneously solving Theorems 1–3 and (45) in Remark 5,
 5. Compute the observer matrix gains $S_i, H_i, N_i, G_{1i}, G_{2i}$ and L_i from (22) and T_i from (10a),
 6. Compute thresholds (47).
-

Remark 7 It should be noted that Algorithm (48) ensures that the best solution with respect to cost function (48) is obtained. This renders the residual functions as sensible as possible to the fault and attack signals while guaranteeing the best possible attenuation performance of the disturbances and communication uncertainties with respect to the residual evaluation functions. It is also worth mentioning that the proposed method introduces additional design variables to the optimisation problem (e.g. matrix variables Y_i), and no products between Lyapunov matrices (P_i , Q_i or X_i) and the observer matrices N_i . It allows the use of different Lyapunov matrices for each Theorem, and solving Algorithm 1 with the common design variable Y_i which, unlike Lyapunov matrices, is only required to be nonsingular. This fact, along with the addition of variables σ_{1i} , σ_{2i} , σ_{3i} and matrix K_i , allows more degree of freedom and reduces the conservatism of the overall solution.

Algorithm 2 given in the following is ran online and summarises the detection and isolation logic where an agent i is said to be faulty if $f_{a_i}(t) \neq 0$ and/or $f_{s_i}(t) \neq 0$.

Algorithm 2: Decision logic for agent i (online)

1. Apply evaluation functions (46),
2. If $\exists j \in \mathcal{N}_i$ such that $J_{i,j}^e(t) > J_{i,j}^{eth}$, and $J_{i,i}^e(t) \leq J_{i,i}^{eth}$ then request π_j . If $\pi_j \neq 0$ then node j is faulty, else the link (i, j) incident to agent i is faulty,
3. If $J_{i,p}^e(t) > J_{i,p}^{eth}$, $\forall p \in \mathcal{N}_i \cup i$, then agent i is faulty. Request π_j , $j \in \mathcal{N}_i$, if $\pi_j \neq 0$ then agent j is also faulty, else the link $\{i, j\}$ incident to node i is faulty,
4. If $J_{i,p}^e(t) < J_{i,p}^{eth}$, $\forall p \in \mathcal{N}_i \cup i$, then no fault/attack has occurred.

4 Illustrative example

To show the effectiveness of the proposed algorithm, let us consider a heterogeneous MAS composed of one-link flexible joint manipulator robots. In the following, there are three followers labelled 1 to $N = 3$ and one virtual leader labelled 0. They are connected according to the directed graph topology represented in Fig. 1.

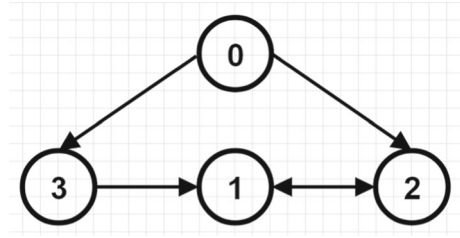


Fig. 1 Communication topology

The associated adjacency matrix is given as

$$\mathcal{A} = \begin{pmatrix} 0 & 0.5 & 0.5 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}.$$

Their dynamics is expressed as [42]

$$\begin{cases} \dot{\theta}_{m_i} = \omega_{m_i}, \\ \dot{\omega}_{m_i} = \frac{k_i}{J_{m_i}}(\theta_{l_i} - \theta_{M_i}) - \frac{B_i}{J_{m_i}}\omega_{m_i} + \frac{K_{\tau_i}}{J_{m_i}}u_i, \\ \dot{\theta}_{l_i} = \omega_{l_i}, \\ \dot{\omega}_{l_i} = -\frac{k_i}{J_{l_i}}(\theta_{l_i} - \theta_{M_i}) - \frac{m_i g h_i}{J_{l_i}}\sin(\theta_{l_i}), \end{cases}$$

where θ_{m_i} is the rotation angle of the motor, θ_{l_i} is the rotation angle of the link, ω_{m_i} and ω_{l_i} are their angular velocities. The following table summarises the parameters.

Parameter	Unit
Link inertia J_{l_i}	kg m ²
Motor inertia J_{m_i}	kg m ²
Viscous friction coefficient B_i	Nm V ⁻¹
Amplifier gain K_{τ_i}	Nm V ⁻¹
Torsional spring constant k_i	Nm rad ⁻¹
Link length h_i	m
Mass m_i	kg
Gravitational acceleration g	ms ⁻¹

By setting, for all $i = 1, 2, 3$, $x_i^T = (\theta_{m_i} \ \omega_{m_i} \ \theta_{l_i} \ \omega_{l_i})$ $= (x_{i1} \ x_{i2} \ x_{i3} \ x_{i4})$ and $x_0^T = (x_{01} \ x_{02} \ x_{03} \ x_{04})$ where x_0 is the virtual leader state, the state space representation can be given as

$$A_i = \begin{pmatrix} 0 & 1 & 0 & 0 \\ -\frac{k_i}{J_{m_i}} & -\frac{B_i}{J_{m_i}} & \frac{k_i}{J_{m_i}} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_i}{J_{l_i}} & 0 & -\frac{k_i}{J_{l_i}} & 0 \end{pmatrix}, \quad B_{u_i} = \begin{pmatrix} 0 \\ \frac{K_{\tau_i}}{J_{m_i}} \\ 0 \\ 0 \end{pmatrix},$$

$$B_{d_i} = \begin{pmatrix} 0 \\ 0.1 \\ 0 \\ 0.5 \end{pmatrix}, \quad \varphi_i(x_i(t)) = \begin{pmatrix} 0 \\ 0 \\ 0 \\ -\frac{m_i g b_i}{J_{l_i}} \sin(\theta_{l_i}) \end{pmatrix},$$

$$\begin{aligned} B_{f_i} &= B_{u_i}, \quad D_{f_1} = \begin{pmatrix} 1 \\ 1 \end{pmatrix}, \quad D_{f_2} = D_{f_3} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}, \\ D_{d_1} &= \begin{pmatrix} 0.05 \\ 0.1 \end{pmatrix}, \quad D_{d_2} = \begin{pmatrix} 0.1 \\ 0.2 \end{pmatrix}, \quad D_{d_3} = \begin{pmatrix} 0.5 \\ 0.7 \end{pmatrix}, \\ C_1 &= \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{pmatrix}, \quad C_2 = \begin{pmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}, \\ C_3 &= \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{pmatrix}, \end{aligned}$$

$$D_{z_{13}} = \mathbf{1}, \quad D_{u_{13}} = \mathbf{1}, \quad D_{z_{31}} = \mathbf{1}, \quad D_{u_{31}} = \mathbf{1}, \quad D_{z_{12}} = I, \\ D_{u_{12}} = \mathbf{1}, \quad D_{z_{21}} = I, \quad D_{u_{21}} = \mathbf{1}.$$

In the following simulations, the parameter uncertainties are considered as $\Delta a_{ij}(t) = 0.1 \sin(a_{ij}t)$ and the perturbations $d_i(t)$ as Gaussian white noise with values in $[-0.2, 0.2]$. For the followers, the parameters are chosen as $m_1 = m_2 = m_3 = 0.21 \text{ kg}$, $k_1 = 0.18 \text{ Nm} \cdot \text{rad}^{-1}$, $k_2 = 0.1 \text{ Nm} \cdot \text{rad}^{-1}$, $k_3 = 0.22 \text{ Nm} \cdot \text{rad}^{-1}$, $B_1 = 4.6 \times 10^{-2} \text{ NmV}^{-1}$, $B_2 = 3.6 \times 10^{-2} \text{ NmV}^{-1}$, $B_3 = 5.6 \times 10^{-2} \text{ NmV}^{-1}$, $J_{m_1} = J_{m_2} = J_{m_3} = 3.7 \times 10^{-3} \text{ kgm}^2$, $J_{l_1} = J_{l_2} = J_{l_3} = 9.3 \times 10^{-3} \text{ kgm}^2$, $K_{\tau_1} = 0.08 \text{ NmV}^{-1}$, $K_{\tau_2} = 0.085 \text{ NmV}^{-1}$, $K_{\tau_3} = 0.09 \text{ NmV}^{-1}$, $g = 9, 8 \text{ m/s}^2$, $h = 0.3 \text{ m}$. The leader parameters are given as $m_0 = 0.21 \text{ kg}$, $k_0 = 0.18 \text{ Nm} \cdot \text{rad}^{-1}$, $B_0 = 4.6 \times 10^{-2} \text{ NmV}^{-1}$, $J_{m_0} = 3.7 \times 10^{-3} \text{ kgm}^2$, $J_{l_0} = 9.3 \times 10^{-3} \text{ kgm}^2$, $K_{\tau_0} = 0.08 \text{ NmV}^{-1}$.

It is thus easy to verify that $\theta_{M_1} = \theta_{M_2} = \theta_{M_3} = 3.3$. The initial conditions are given as $x_0(0) = (0, 0, 0, 0)$, $x_1(0) = (0.1, 0, 0.2, 0)$, $x_2(0) = (0.5, 0, 0.1, 0)$, $x_3(0) = (0.3, 0, 0.4, 0)$. In this example, a tweaked version of the leader–follower control algorithm proposed in [47] is used based on the estimated state:

$$u_i = -M_i \left[\sum_{j=1}^3 a_{ij} (\hat{x}_i - \hat{x}_i^j) + g_{0i} (\hat{x}_i - x_0) \right],$$

where $\hat{x}_{v_i}^T = (\hat{x}_i^1 \hat{x}_i^{i_1} \dots \hat{x}_i^{i_{N_i}})$, $e_{v_i}^T = (e_i^1 e_i^{i_1} \dots e_i^{i_{N_i}})$ $= (e_{i_1}^1 \dots e_{i_4}^1 e_{i_{11}}^{i_1} \dots e_{i_{14}}^{i_{N_i}})$, $\hat{x}_i^p \in \mathbb{R}^4$, $e_i^p = x_p - \hat{x}_i^p \in \mathbb{R}^4$, $\forall p \in \mathcal{N}_i \cup i$, M_i is a control gain matrix and g_{0i} defines the communication link between agent i and leader 0 ($g_{0i} = 1$ when 0 communicates with i and $g_{0i} = 0$ otherwise). The control gains are given as

$$\begin{cases} M_1 = [1.6207 \ 0.2210 \ -0.5444 \ 3.2570], \\ M_2 = [1.6924 \ 0.2308 \ -0.5685 \ 3.4011], \\ M_3 = [1.7642 \ 0.2405 \ -0.5925 \ 3.5452]. \end{cases}$$

The multi-objective weights are chosen as $\lambda_{i1} = \lambda_{i2} = \lambda_{i3} = \lambda_{i4} = \lambda_{i5} = 1$, $\forall i$. The vector \mathcal{F}_i is assumed to belong to the finite-frequency domain $[0, 0.1)$. It is worth noting that inequalities (20), (30), (39) and (45) can be solved using an appropriate solver (YALMIP, etc. [48]).

$\forall i \in \{1, 2, 3\}$, Algorithm 1 is applied for $\sigma_{1i} = 1$, $\sigma_{2i} = 0.2$, $\sigma_{3i} = 0.1$, $K_i = -2B_{u_i}$, $\varepsilon_i = 0.04$ and $W_i = I$, yielding $\eta_1 = 0.2$, $\beta_1 = 0.2$, $\vartheta_1 = 0.01$, $\gamma_1 = 0.1$, $\varrho_1 = 0.81$, $\eta_2 = 0.15$, $\beta_2 = 0.15$, $\vartheta_2 = 0.02$, $\gamma_2 = 0.1$, $\varrho_2 = 0.85$, $\eta_3 = 0.04$, $\beta_3 = 0.4$, $\vartheta_3 = 0.01$, $\gamma_3 = 0.7$, $\varrho_3 = 0.77$.

Remark 8 It should be highlighted that the computation of the matrix gains is done offline and once. Based on Theorems 1–3, for each agent, the observer matrix gains are computed according to Algorithm 1. Therefore, a set of LMIs has to be solved offline and once. One can note that the dimension and number of LMIs linearly increase as the state and number of agents increase. Here, $4N$ LMIs (N is the number of agents) should be solved. For an agent i , their dimensions are: $(3n_x^i + n_{f_s}^i + \underline{n}_{f_z}^i) \times (3n_x^i + n_{f_s}^i + \underline{n}_{f_z}^i)$ for Theorem 1, $(3n_x^i + n_{f_a}^i + N_i n_{f_u}) \times (3n_x^i + n_{f_a}^i + N_i n_{f_u})$ for Theorem 2, $(3n_x^i + n_d^i + \underline{n}_z^i + \underline{n}_u^i) \times (3n_x^i + n_d^i + \underline{n}_z^i + \underline{n}_u^i)$ for Theorem 3 and $n_x^i \times n_x^i$ for Remark 5. These dimensions are given in Table 2 for the illustrative example. Additionally, for each agent, the size of the FDI modules (i.e. Eq. (8)) is only dependent on the number of neighbouring agents regardless of the agents' control inputs, which makes the proposed scheme highly scalable.

Remark 9 It is interesting to note that for implementation of the method proposed in this work, each agent

Table 2 LMI dimensions for each agent, where LMIST1: LMI Size in Theorem 1, LMIST2: LMI Size in Theorem 2, LMIST3: LMI Size in Theorem 3, LMIST1: LMI Size in Remark 5

Agent	LMIST1	LMIST2	LMIST3	LMISR5
1	40 × 40	39 × 39	46 × 46	12 × 12
2	27 × 27	26 × 26	30 × 30	8 × 8
3	13 × 13	13 × 13	14 × 14	4 × 4

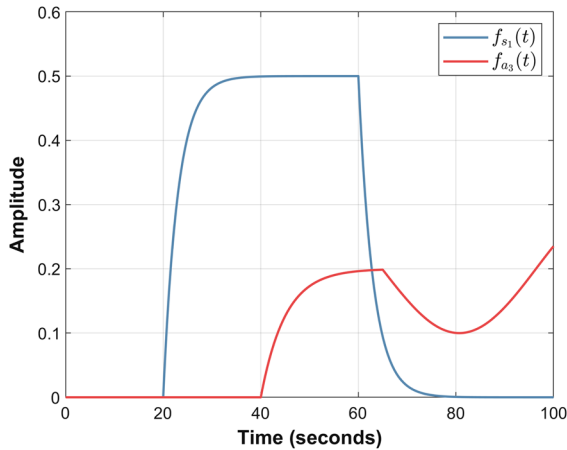


Fig. 2 Faults signal in scenario 1

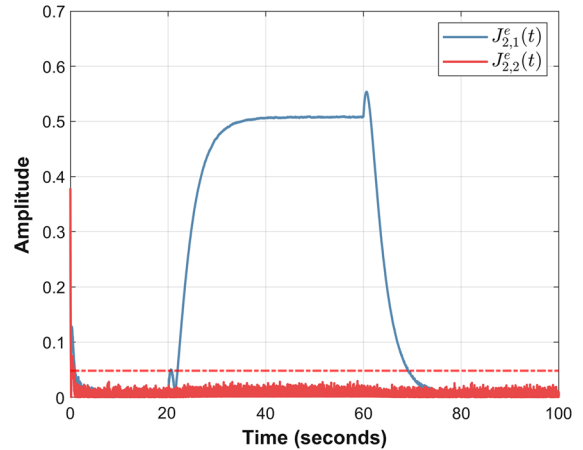


Fig. 4 Residual evaluation functions at agent 2 in scenario 1

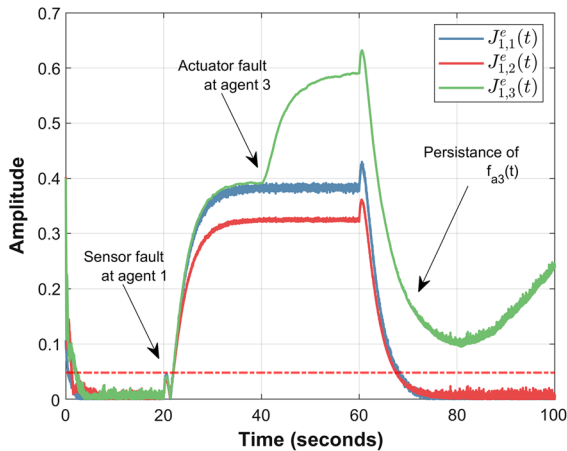


Fig. 3 Residual evaluation functions at agent 1 in scenario 1. The dashed red lines represent the threshold

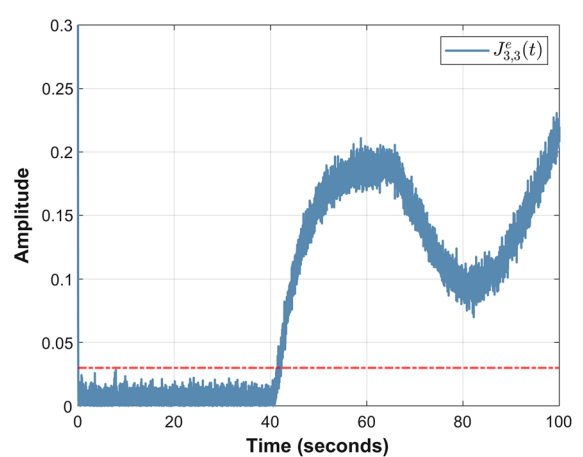


Fig. 5 Residual evaluation functions at agent 3 in scenario 1

sends its corrupted output and its corrupted control input (dimension $n_u + n_y$). This can increase the communication cost in contrast with [27] for instance, where the FDI modules only require estimated outputs to be broadcasted (dimension n_y). However, as opposed to [27], the proposed method does not require the agents to be equipped with relative information sensors. Indeed, requiring that the agents are equipped with both relative information sensors and wireless communication modules, can limit the cost-effectiveness of the method proposed therein.

Let us consider hereafter two scenarios. In the first one, two faults occur in the network: a sensor fault

$f_{s1}(t)$ at agent 1 and an actuator fault $f_{a3}(t)$ at agent 3, as represented in Fig. 2. Figures 3, 4 and 5 show the generated residual evaluation functions by agents 1, 2 and 3, respectively. The worst case analysis of the evaluation functions corresponding to the non-faulty operation of the network under disturbances and uncertainties leads to the following thresholds $J_{1th}^e = 0.048$, $J_{2th}^e = 0.03$ and $J_{3th}^e = 0.027$ under the evaluation window $T_w = 10s$. It is usually not easy to accurately compute the value of the supremum of the RMS function in (47) to simultaneously prevent false alarms and avoid missed detections. As such, a series of Monte Carlo simulations have been conducted where the supremum of the RMS function in (47) is calculated

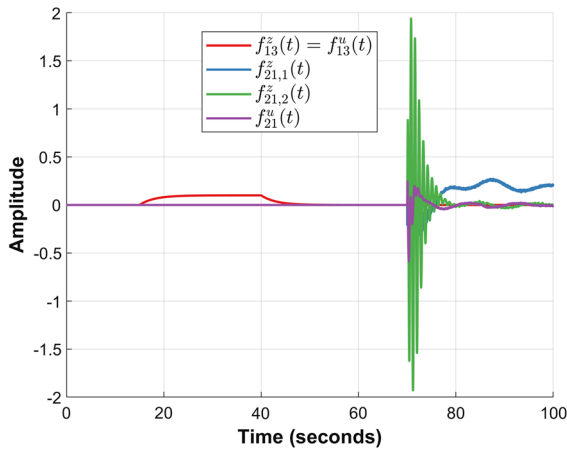


Fig. 6 Simulated attack signals in scenario 2, where $f_{21}^z(t) = [f_{21,1}^z(t), f_{21,2}^z(t)]^T$

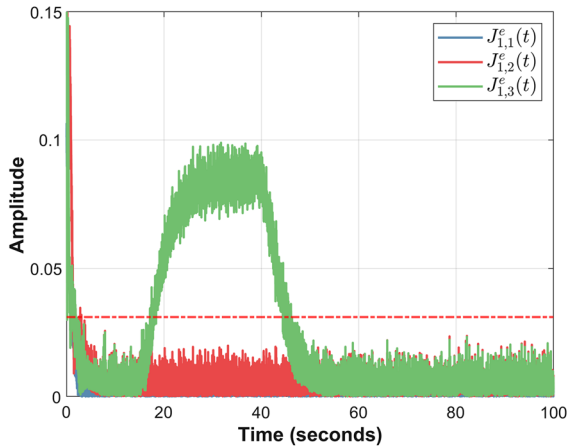


Fig. 7 Residual evaluation functions at agent 1 in scenario 2

under the healthy operation of the MAS, with different noises, disturbances and uncertainties. The corresponding maximum value has been taken as an appropriate threshold. The sampling period is set as $T_s = 10^{-1}$ s. One could see from Figs. 3, 4 and 5 that the faults could be clearly distinguished. Additionally, according to Algorithm 2, one can see from Fig. 3 that all generated functions $J_{1,1}^e(t)$, $J_{1,2}^e(t)$ and $J_{1,3}^e(t)$ increase at around $t = 20$ s and exceed the defined threshold due to the sensor fault $f_{s1}(t)$ occurring at agent 1. This confirms that a fault has occurred at agent 1. Figure 4 further confirms this, since only $J_{2,1}^e(t)$ increases due to this fault. At $t = 40$ s, the actuator fault $f_{a3}(t)$ occurs

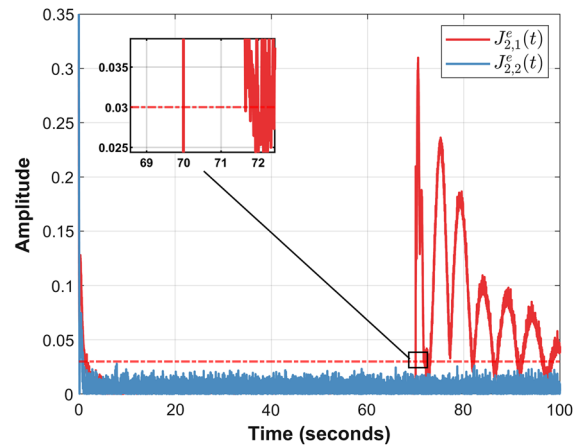


Fig. 8 Residual evaluation functions at agent 2 in scenario 2

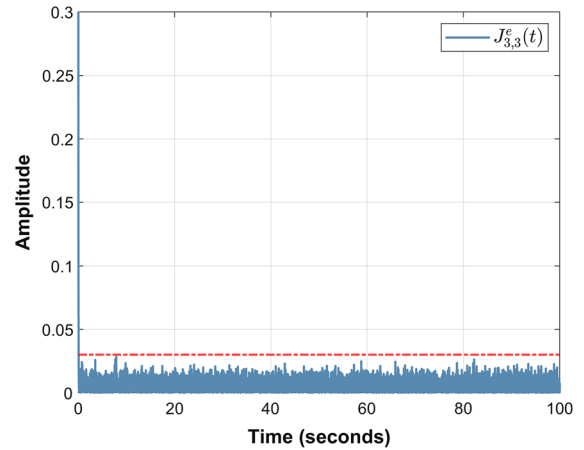


Fig. 9 Residual evaluation functions at agent 3 in scenario 2

at agent 3, where one can see in Fig. 3 that agent 1 detects it (its residual evaluation function for agent 3, i.e. $J_{1,3}^e(t)$, is greater than J_{1th}^e even though both $J_{1,1}^e(t)$ and $J_{1,2}^e(t)$ are lower than J_{1th}^e). Hence, according to Algorithm 2, agent 1 can distinguish that the fault $f_{s1}(t)$ has disappeared and that agent 3 is now faulty. This is confirmed for agent 3 in Fig. 5.

Remark 10 It is worth mentioning that the sensor fault matrices D_{f2} and D_{f3} are not full column rank. Hence, the methods proposed in [27,28] for instance cannot be applied. Moreover, the effectiveness of the proposed method has been shown for heterogeneous MASs under directed topologies. Besides, compared with the decentralised observer proposed in [49] for example, in which faults occurring at agent i can only be detected

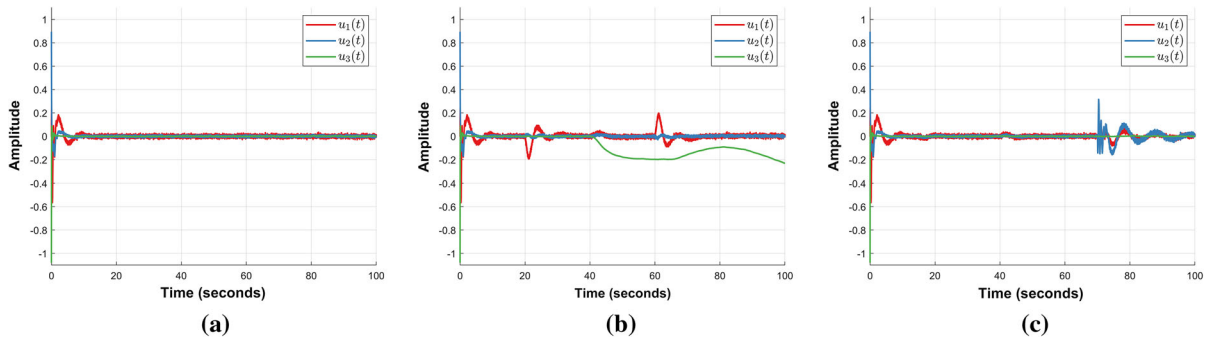


Fig. 10 Control efforts in: **a** the faultless case, **b** scenario 1, **c** scenario 2

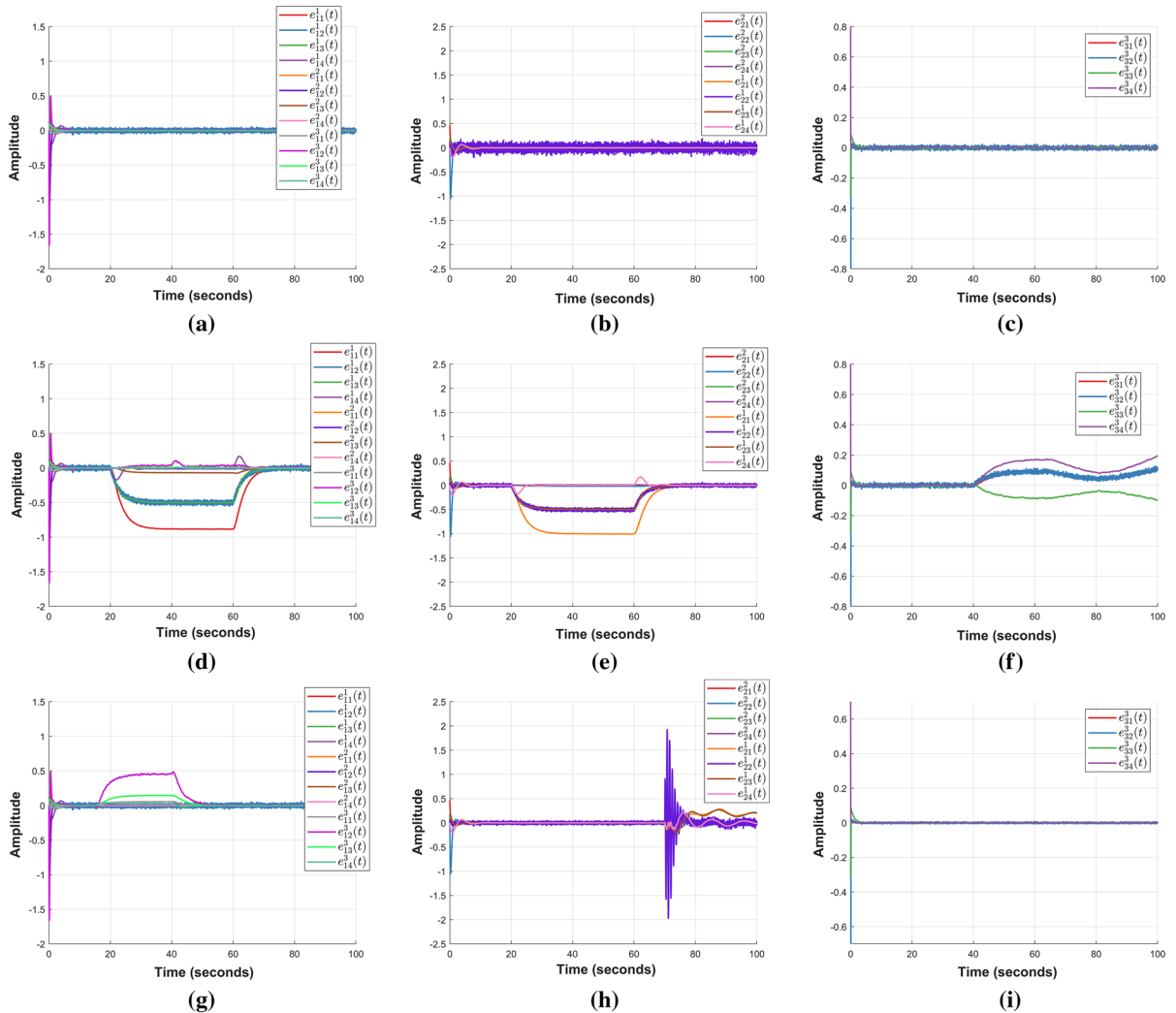


Fig. 11 Estimation errors: **a** at agent 1 in the faultless and attackless case, **b** at agent 2 in the faultless and attackless case, **c** at agent 3 in the faultless and attackless case, **d** at agent 1 in sce-

nario 1, **e** at agent 2 in scenario 1, **f** at agent 3 in scenario 1, **g** at agent 1 in scenario 2, **h** at agent 2 in scenario 2 and **i** at agent 3 in scenario 2

by the agent itself, our distributed observer can detect both the agent's faults and its neighbours' faults. At last, it can be noticed that the matching condition, i.e. $\text{rank}(C_i B_{f_i}) = n_{f_i}$, required in many existing works (e.g. [50]), is not needed in our methodology. Indeed, this condition is not satisfied for agents 2 and 3.

In the second scenario, two types of faults are considered: a data injection attack incident to agent 1 targeting the link going from agent 3 to 1, i.e. $f_{13}^z(t) = f_{13}^u(t)$ occurring at $15s \leq t \leq 40s$, and a replay attack incident to agent 2 at the link going from agent 1 to 2 at $t = 70s$, i.e. $f_{21}^z(t)$ and $f_{21}^u(t)$ with a delay of $T_{12} = 70s$. $f_{13}^z(t)$, $f_{13}^u(t)$, $f_{21}^z(t)$ and $f_{21}^u(t)$ are represented in Fig. 6. Figures 7, 8 and 9 show the generated evaluation functions by agents 1, 2 and 3, respectively, in the second scenario. The worst case analysis of the evaluation functions corresponding to the attack-less operation of the network under disturbances and uncertainties leads to the following thresholds $J_{1rh}^e = 0.016$, $J_{2rh}^e = 0.017$, $J_{3rh}^e = 0.02$. It is clear from the evaluation functions that the attacks can be distinguished when surpassing the computed thresholds. Indeed, from Fig. 7, one can see that the data injection attack in the link from 3 to 1 has been detected according to Algorithm 2. It is confirmed that this fault is an edge fault upon requesting agent 3's detection flag, as $J_{3,3}^e$ stays below the defined threshold throughout the duration of the attack. From Fig. 8, the replay attack in the link from agent 1 to 2 has been detected by $J_{2,1}^e(t)$ at $t = 70s$ which is confirmed by the fact that $J_{1,1}^e$ does not react to the attack.

The control efforts corresponding to the faultless case and scenarios 1 and 2 are depicted in Fig. 10. Figure 11 shows the estimation errors generated by the FDI modules for agents 1, 2 and 3, respectively. It can clearly be seen that the estimation errors converge to zero in the absence of any fault or attack.

From these simulations, it can be seen that the proposed FDI scheme is able to detect and isolate attacks, actuator faults and sensor faults in the presence of disturbances, noise and communication uncertainties.

5 Conclusion

In this paper, the problem of FDI in Lipschitz nonlinear MASs with disturbances, subject to actuator, sensor and communication faults has been addressed. A multi-objective finite-frequency $\mathcal{H}_-/\mathcal{H}_\infty$ design along with

nonlinear UIOs has been proposed. Sufficient conditions have been derived in terms of a set of LMIs. The combination of UIOs, removal of strict rank conditions and finite-frequency method has been shown to provide extra degrees of freedom in the FDI filter design. Additionally, the multi-objective method guarantees that the evaluation functions are robust with respect to all admissible disturbances and uncertainties and sensitive to all types of faults. A numerical example has been studied in order to showcase the effectiveness of the proposed scheme. As future works, instead of considering Lipschitz nonlinear systems, one could investigate other classes of nonlinear uncertain systems including chained-form dynamics. Based on the proposed FDI scheme, it would also be possible to design some fault accommodation strategies.

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Data availability The authors declare that the manuscript has no associated data.

Declarations

Conflict of interest The authors declare that they have no conflict of interest.

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