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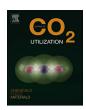


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Enhanced selectivity of carbonaceous products from electrochemical reduction of CO₂ in aqueous media



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ABSTRACT

This study highlights the importance of CO_2 supply method and impact of electrolyte alkalinity in aqueous electrochemical CO_2 reduction using Cu_xO catalyst. Two different CO_2 supply methods using a two-chamber (2C) cell with CO_2 purging into catholyte and a CO_2 gas diffusion electrode (GDE) cell were compared. Faradaic efficiency (FE) of carbonaceous products in GDE cell was more than 3-folds higher than the 2C cell due to improved CO_2 mass transfer. From the investigation of alkaline catholyte in GDE cell, the higher catholyte alkalinity led to higher current density and higher FE of carbonaceous products with a better selectivity of C_2 (ethanol and ethylene). The reason lies in the OH groups around catalyst surface which improve the reaction kinetics and moreover stabilize the catalyst surface oxygen during the reduction process. With the potential of -1.17 V (RHE) in 2.0 M KOH, C_2 FE of 40% and current density of -234 mA cm $^{-2}$ were achieved. The production rate of ethylene and ethanol was respectively 0.105 mg min $^{-1}$ and 0.035 mg min $^{-1}$ on 2 cm 2 electrode with CO_2 flow rate 15 ml min $^{-1}$, which are promising for further development and scale-up.

1. Introduction

The increasing demand for energy and challenges from environmental issues and climate change has led to numerous researches on sustainability and carbon recycling. CO2 concentration in the atmosphere has reached 427 ppm causing environmental concerns and climate change [1]. Increasing production of renewable energy results in demands on energy storage materials and devices. Effectively utilising and directly converting carbon dioxide (CO2) into fuels as energy storage media and other valuable chemicals could provide a solution. Among the approaches of CO2 conversion, electrochemical CO2 reduction reaction (eCO₂RR) attracted large interests as it only consumes water and electricity as the inputs to build hydrocarbons and oxygenates (i.e., alcohols and carboxylic acids) and to release pure O2 as a byproduct on the anodic side. However, hydrogen evolution reaction (HER) shares similar reaction potential (0.0 V vs. RHE) with eCO2RR and takes place simultaneously. Due to the big energy barrier of CO2 activation [2], H₂ is theoretically much easier to be produced than carbonaceous products under aqueous eCO₂RR conditions [3,4].

The rate-determining steps for eCO_2RR and HER in the competitive charge transfer are both one-electron reversible process as illustrated in Equation (1) and Equation (2 or 3) respectively [2–4].

HER: Acidic:
$$H^+ + e^- \leftrightarrow H(ads)$$
 (2)

Neutral/Alkaline:
$$H_2O + e^- \leftrightarrow OH^- + H(ads)$$
 (3)

The reaction rate of the one-electron reversible electrode process is generally defined as Equation (4) [5].

$$R = \frac{j}{nF} = \frac{j_0 \left[\frac{C_O(0,t)}{C_O^*} e^{-\alpha f \eta} - \frac{C_R(0,t)}{C_R^*} e^{(1-\alpha)f \eta} \right]}{nF}$$
(4)

Where: j: local current density (A m⁻²)

n: number of electron transfer, here it is 1

F: faradaic constant (96,485 C mol⁻¹)

 j_0 : exchange current density (A m⁻²)

 $C_O(0,t)/C_R(0,t)$: the surface concentration of oxidant/reduced product at time t

 C_O^*/C_R^* : the bulk concentration of oxidant/reduced product

 α : transfer coefficient (= 0~1)

f: a constant (=F/RT)

n: overpotential (V)

The initial rate of either eCO_2RR or HER accords with Equation (4) which is mainly co-determined by the exchange current density j_0 , the surface concentration of reactant, and overpotential. The j_0 is primarily

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 $eCO2RR: CO_2(aq) + e^- \leftrightarrow CO_2^-(ads)$ (1)

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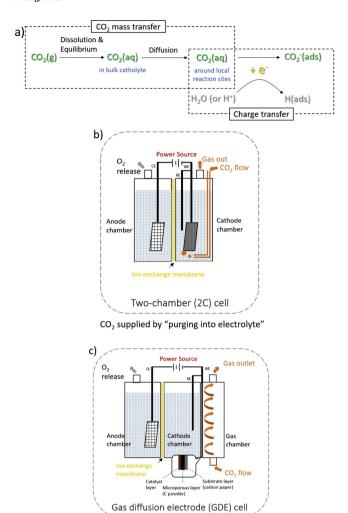


Fig. 1. a) Mass transfer and charge transfer in aqueous eCO₂RR system. Schematic diagrams of aqueous eCO₂RR system using b) 2C cell and c) GDE cell.

CO2 supplied by "Diffusion from GDE"

related to the adsorption energy of the active species ($\mathrm{CO_2}^-(\mathrm{ads})$ and H (ads)) on the electrode material [6]. A suitable catalyst [7] can change the adsorption energy to those species, intending to control the selectivity between carbonaceous products and H₂. In the aqueous eCO₂RR system, the inherent competitive advantage for HER is mass transfer, in another word, the surface concentration of H₂O (or H⁺) is always sufficient. However, the mass transfer of heterogeneous $\mathrm{CO_2}$ gas is a more complicated process as illustrated in Fig. 1a.

Majority of publications [8,9] applied a traditional two-chamber (2C) cell where the reactant CO_2 gas was supplied by "purging into electrolyte", as shown in Fig. 1b. CO_2 mass transport is determined by CO_2 solubility. Different approaches have been carried out to increase CO_2 solubility in the electrolytes, such as altering the reaction environment with high pressure [10–12] and low temperature [13], and using alcoholic base [14,15] or ionic liquid [16] as the electrolyte. However, comparing with the ambient pressure, room temperature and aqueous electrolytes, those approaches carry their own set of cost and sustainability issues.

The use of a gas diffusion electrode (GDE) changes the CO₂ supply way from "purging into electrolyte" to "diffusion from GDE" as shown in Fig. 1c, which can directly feed CO₂ gas flow to the reaction interface which has been used by fuel cells for a long time [17]. An increasing number of GDE-based studies in aqueous eCO2RR were published in recent years, commonly achieving a remarkable current density (j) and reasonable faradaic efficiency (FE) towards C-products at ambient temperature and pressure, as summarised in Table 1. In the aqueous system with 2C cells, satisfying FE (> 50%) of carbonaceous products have also been reported but the current densities were averagely low $(< 10 \text{ mA cm}^{-2} \text{ at moderate potentials around } -1.0 \text{ V (vs. RHE) } [18])$ which is about 10-folds less than GDE cells. The application of GDE should be a reliable approach to transition this bench-scale research to industry. For the further optimisation, the real effect of GDE on eCO2RR and the factors for the high current density achieved in GDE-related studies still need to be explicit.

J. Albo et al. [25] compared the GDE performances with Cu₂O catalyst when CO2 supplied as gas and when CO2 supplied in saturated aqueous catholyte. The direct CO2 gas feeding showed ~ 3 mA cmhigher current density and ~ 9% FE increase in methanol production. However, the reactor dimensions, electrolytes, membrane, applied potential, supply rate of reactants, etc. all have impacts on eCO₂RR performances, an univariate comparison is needed to examine the effect of CO₂ supply method on eCO₂RR. In this work, a 2C cell and a GDE cell were designed in the same dimension and fabricated by 3D printing. Their eCO₂RR performances were compared using the same Cu_xO catalyst, KHCO3 catholyte with various concentrations at a wide range of potentials. The big difference of product distribution disclosed the crucial role of CO2 mass transfer in the selectivity of carbonaceous products. Compared to the 2C cell, GDE cell with efficient CO2 mass transfer showed more than 3-folds improvement of FE for carbonaceous products. eCO₂RR performances in GDE cell with KHCO₃ and KOH with various concentrations were also investigated.

2. Experimental

2.1. Cell fabrication and set up

The CO₂ supply methods of "purging into electrolyte" and "diffusion

Table 1
Summary of eCO₂RR performance with GDE working electrode from literature.

Cathode	Anode Electrolyt	e	Cell voltage/cathode potential (V)	j (mA cm ⁻²)	FE for main products
Sn-GDE [19]	Pt/C coated membrane pressed GDE	0.1 M KHCO_3 (C) 1 M KOH (A)	Cell: -2.75 V	-26	65% Formate
Ag-GDE [20]	Pt/C-GDE	1 M KCl	Cell: -3 V	-90	92% CO
Ag-GDE [21]	Pt/C-GDE	1 M CsOH	Cathode: -1.62 V (vs. Ag/ AgCl)	-80	89.8% CO
Cu _x O-GDE [22]	IrO ₂ -GDE	1 M KOH	Cathode: -0.8 V (vs. RHE)	-400	> 50% C ₂
N-doped graphene quantum dots-GDE [23]	IrO_2 -GDE	1 М КОН	-1.0 V (vs. RHE)	-240	60% C ₂ 5% C ₃
Pb-GDE [24]	PtRu-GDE	$0.5 \text{ M } \text{ K}_2 \text{SO}_4 + 0.5 \text{ M}$ $\text{H}_2 \text{SO}_4 \text{ (C)}$ 1 M KOH (A)	– 2 V (vs. SHE)	-330	90% Formate

from GDE" were carried out by two different electrochemical cells respectively: a 2C cell and a GDE cell were designed with the same dimension of the cathodic and anodic chambers, and fabricated by 3D printer (Form 2, Formlabs) using the photoreactive resin (Form 2 Clear Resin, Formlabs). Cell parts were screwed together using metal bolts. The cathodic and anodic chambers were separated by a cation exchange membrane (CEM) (F-950, Fumapem). The cathode used in both cells was $\mathrm{Cu_xO}$ painted GDE with the geometric surface area $2\,\mathrm{cm}^2$ and the anode was Platinum plated Titanium mesh with a dimension of $4\,\mathrm{cm}^2$. The schematics of the two cells are as described in Fig. 1b and c. Figure S1 shows the 3D drawings of the two cells set-up, with the design information given below in the Supplementary Data.

2.2. Catalyst synthesis and working electrode preparation

 Cu_xO catalyst was synthesized using the hydrothermal method by reduction of Cu acetate (Sigma-Aldrich, 98%) in the solvent of water and ethanol (Sigma-Aldrich, > 99.8%) mixture reported previously [26]. The volume ratio of water and ethanol was controlled as 1:7, i.e., 10 ml water and 70 ml ethanol. The catalyst was dried at 60 °C in an oven (Oven-30S, SciQuip) in air for 8 h.

 $15\,mg$ catalyst (Cu_xO) was weighed and dispersed in $200\,\mu l$ isopropanol and $33\,\mu l$ Nafion suspension (Sigma-Aldrich, 5 wt.%) to prepare the catalyst ink. The ink was sonicated for 20 min before painting onto the surface of carbon paper with gas diffusion layer (GDL) (H2315 I2 C6, Freudenberg). Drying (45 °C, 1~3 min) was applied between each layer. Painting and drying were repeated until the desired Cu_xO catalyst loading of 4~5 mg cm $^{-2}$ was achieved.

2.3. eCO₂RR electrochemical analysis

All the electrochemical reactions and measurements were carried out at ambient temperature and pressure using a potentiostat (Metrohm Autolab PGSTAT128 N). The flow rate of CO₂ (BOC 99.99%) was controlled at 15 ml min⁻¹ by a flow meter (Cole-Parmer TMR1-010462). 5 M KOH solution was employed as the anolyte in all the tests. KHCO₃ (Alfa Aesar, 99%) and KOH (Emsure®, 85%) solution with different concentrations of 0.1, 0.5, 1.0, and 2.0 M (only in KOH) were used as the catholyte, and the comparison was carried out. Ag/AgCl (RE-5B, BASI, 3 M NaCl, 0.197 V vs. SHE) was used as the reference electrode, and a luggin capillary was applied to prevent it from being damaged in alkaline electrolyte. The applied potentials (vs. Ag/AgCl) in the three-electrode system were all converted to the reversible hydrogen electrode (RHE), thus the potentials stated in this study are referred to RHE unless otherwise stated.

In the 2C cell, CO_2 was purged into catholyte 1 h before electrochemical tests.

In the GDE cell, a peristaltic pump (120U/DM2, Watson Marlow) was used to supply fresh catholyte to maintain the local pH and to remove liquid product for reaction equilibrium. The flow rate was controlled at 0.25 ml min $^{-1}$ under the applied potential $-0.17\mathchar`-0.77\math V$ and at 0.5 ml min $^{-1}$ under the applied potential $-0.77\mathchar`-1.17\math V$.

Electrochemical characterisations were made by cyclic voltammetry (CV) and electrochemical impedance spectroscopy (EIS). CV was carried out three cycles between 1.4 to $-1.0\,\mathrm{V}$ with the scan rate 50 mV s $^{-1}$ to initially explore the cathode electrochemical behaviour. The FRA32 M module on the Autolab potentiostat was operated for EIS measurement, which was recorded with an ac-amplitude of 10 mV over the frequency range from 10k Hz to 0.1 Hz either at open circuit voltage (OCV) or at $-0.77\,\mathrm{V}$ cathodic potential. The impedance spectra were analysed and fitted using NOVA 2.0 software.

eCO₂RR was carried out by chronoamperometry (CA) recording the current at a particular applied potential for 30 min. The current density (j) was calculated based on the geometric surface area $2\,\mathrm{cm}^2$ of the working electrode.

2.4. Product analysis

A gas chromatography (Shimazu Tracera GC-2010) equipped with Barrier Discharge Ionization (BID) detector was used to analyse gas products and alcoholic liquid products. The ShinCarbon ST micropacked column 80/100 (Restek) was used to quantitatively analyse permanent gases and light hydrocarbons, while the Zebron ZB-WAXplus capillary column (Phenomenex) was used for alcoholic liquids. An ion chromatography (Eco IC, Metrohm) equipped with the "METROHM 6.1005.200" column was used for quantifying volatile fatty acids (VFA) including formic acid. The faradaic efficiency (FE) for each product was calculated based on Faraday's law (5)³, where z is the number of electrons transferred for per mole of reactant (e.g., z = 2 for reduction of CO₂ to CO), n is mass of the product from the electrode in moles, F is Faraday's constant (96,500 C mol $^{-1}$), Q represents the total charge passed.

$$FE = \frac{z \, n \, F}{Q} \tag{5}$$

2.5. Material characterisation of Cu_xO catalyst

X-ray diffraction (XRD) spectrum which showing the crystal structure of the catalyst were obtained by a Philips X-ray diffractometer PW 1730 diffractometer equipped with a Cu X-ray tube (Cu–K α ; $\lambda=0.154$ nm) operated at 40 kV and 40 mA. To determine the elemental compositions and valence states of the electrode surface (~10 nm depth), X-ray photoelectron spectroscopy (XPS) was performed on a Kratos Axis Nova XPS spectrometer using a K-Alpha line X-Ray source (225 W) over an area of approximately 300×700 µm. Microstructural characterisation of the catalyst was performed by scanning electron microscopy (SEM, Hitachi SU-70) coupled with an energy dispersive X-ray detector (EDX, Bruker Quantax 400).

3. Results and discussion

3.1. Effect of CO₂ supply method

The two CO2 supply methods of "purging into electrolyte" and "diffusion from GDE" implemented by 2C cell and GDE cell respectively, were compared through eCO2RR using the same CuxO-painted GDE as the cathode and same KHCO3 catholyte. The catalyst morphology before and after 3 h eCO₂RR in 1.0 M KHCO₃ was analysed by SEM and EDX as shown in Figure S2. The fresh catalyst consisted of spherical particles (100 ~ 1000 nm) which became finer after reaction. The EDX analysis (Figure S2) indicated that Cu_xO catalyst was reduced during eCO₂RR since the atomic ratio of copper to oxygen (Cu/O) was increased from 2.81 (before reaction) to 8.13 (after reaction). Since the substance composition and morphology of Cu_xO catalyst changed over the eCO₂RR duration, fresh Cu_xO catalyst was used in each eCO₂RR, with CV measurements in N2 and CO2 atmosphere respectively at the beginning. CV results which preliminarily evaluated the reaction behaviour are shown in Figure S3. After CV, eCO₂RRs were carried out by CA at specific fixed potentials (30 min for each potential), the raw data of CAs are given in Figure S4. The normalized FEs for carbonaceous products and H₂, and the average current density of eCO₂RRs in the 2C and GDE cell were calculated and are shown in Table S1. FE sum of all the carbonaceous products and current density (j) taken from Table S1 are presented in Fig. 2.

It can be observed from the comparison between Fig. 2a and b that: Within the potential range from -0.17 to -1.17 V, the GDE cell produced carbonaceous products with higher FE than the 2C cell. Although the current densities of the two cells were similar at the same catholyte and potential, the current in the 2C cell was mostly associated with HER. Only a small amount of formate and CO were produced when potentials were more negative than -0.37 V in the 2C cell, whereas CO

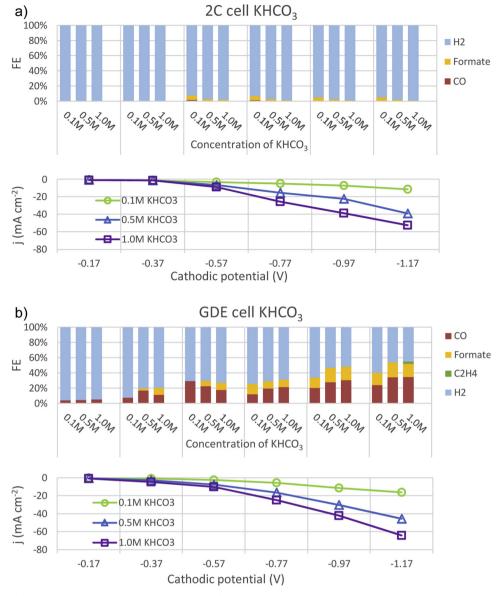


Fig. 2. eCO_2RRs catalysed by Cu_xO at a wide range of applied potentials in a) 2C cell with different concentrations of KHCO₃ and b) GDE cell with different concentrations of KHCO₃.

was observed from $-0.17\,V$ in all KHCO $_3$ electrolytes from GDE cell. The FE of carbonaceous products in GDE cell increased with more negative potential, 5% at $-0.17\,V$ to 54% at $-1.17\,V$.

The relationship between total FE of carbonaceous products and $\rm KHCO_3$ catholyte concentration in 2C cell and GDE cell were opposite. In the 2C cell, FE of carbonaceous products decreased with an increase in $\rm KHCO_3$ concentration (a similar result was reported by Hori [27]). However, the GDE cell showed the carbonaceous FE increased with the increasing $\rm KHCO_3$ concentration.

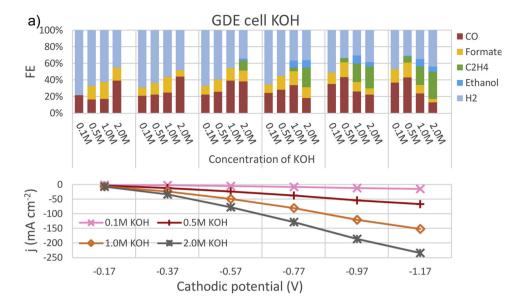
This can be caused by different reaction species from different CO_2 supply method. In the 2C cell, it has been widely accepted that the real reactant in the eCO₂RR system is the dissolved CO_2 (generally written as CO_2 (aq) or $H_2CO_3^*$), rather than ionic HCO_3^- and CO_3 [2–27,1–29]. Although $H_2CO_3^*$ concentration increased from higher CO_2 solubility in higher concentration of KHCO₃, the CO_2 reduction was determined by the ratio of $H_2CO_3^*$ /Total carbonate, which is higher in lower concentrations of KHCO₃ according to Heng et al.29] leading to higher selectivity in 0.1 M KHCO₃ than in 1.0 M KHCO₃.

In aqueous medium, the process of CO₂ mass transfer is composed of two major steps: Step 1. CO₂ gas dissolution and equilibrium to produce

the reactant $CO_2(aq)$, Step 2. $CO_2(aq)$ diffusion from bulk catholyte to local reaction sites. The rate of each step and the corresponding influence factors are summarized in Table S2. A brief review related to CO_2 mass transfer process given below Table S2 indicates that KHCO₃ with higher concentration can balance slightly more $CO_2(aq)$ in the bulk electrolyte [29] in Step 1, but constrains $CO_2(aq)$ diffusion [30] in Step 2. Moreover, under reduction potential, the K⁺ of catholyte would be adsorbed around the double layer that further hinders $CO_2(aq)$ diffusion [31], in favour of hydrogen evolution.

In the GDE cell, the reactant was more likely activated CO_2 species, CO_2^* , which the adsorption mechanism as shown in Equation (6) where gaseous CO_2 or CO_2^* can be directly reacting at the catalyst interface. The gas adsorption mechanism in GDE was also reported in oxygen reduction reaction (ORR) related studies [32]. With this mass transfer mechanism in GDE cell, sufficient CO_2 reactant could be provided around reaction sites, which develops the competitiveness of eCO_2RR against HER, reflected in a significantly enhanced carbonaceous selectivity than 2C cell.

$$CO_2(g) \xrightarrow{e^-} CO_2^-(ads)$$
 (6)



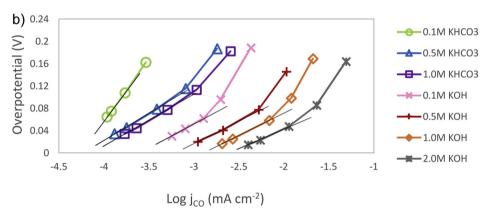


Fig. 3. a) eCO_2RRs catalysed by Cu_xO at a wide range of applied potentials in GDE cell with different concentrations of KOH. b) Tafel plots of the partial current density of CO_2 reduced to CO_2 reduced to CO_3 redu

In GDE cell, FE of carbonaceous products and current density both increased with the $KHCO_3$ concentration which was probably related to the alkalinity of catholyte. KOH with different concentrations were applied to further study the effect of alkaline catholyte in GDE cell, shown below (Fig. 3a).

3.2. Effect of alkaline catholyte in GDE cell

Fig. 3a shows the eCO $_2$ RR results in GDE cell by applying different concentrations of KOH as the catholyte, Cu $_x$ O was the catalyst. Tafel plots of CO production from eCO $_2$ RR are displayed in Fig. 3b to assess the mechanistic pathway of eCO $_2$ RR in GDE cell with different catholyte since CO was the common product for all the situations and the easiest to be generated at low overpotential. The Tafel slopes show the relationship of IR-corrected overpotential, to eliminate the effect from resistance of the solution, and the log of the partial current density using the actual electrode surface area 108.6 cm 2 , which was determined by measuring the double layer capacitance in 0.1 M HClO $_4$ [33] (Figure S5 and Table S3).

Table 2 shows the Tafel parameters of different catholytes in GDE cell obtained from Fig. 3b. With the increasing catholyte pH, the Tafel slope decreased, and the exchange current density $j_0(eCO_2RR)$ for CO production increased, indicating faster kinetics and higher activity of eCO_2RR with more alkaline catholyte. Apart from 0.1 M KHCO₃ with lowest [OH $^-$], the difference between other Tafel slope values were

Table 2Tafel parameters obtained from the Tafel plots (Fig. 3b), b represents the Tafel slope for the lower overpotential region.

	KHCO ₃			КОН			
	0.1 M	0.5 M	1.0 M	0.1 M	0.5 M	1.0 M	2.0 M
pH b /mV dec ⁻¹ j ₀ /mA cm ⁻²	5.41	9.04 95 5.76 ×10 ⁻⁵	9.67 92 7.30 ×10 ⁻⁵	13.02 90 2.61 ×10 ⁻⁴	13.56 86 5.77 ×10 ⁻⁴	13.96 81 1.30 ×10 ⁻³	14.30 74 2.60 ×10 ⁻³

small, decreased from 95 mV dec $^{-1}$ in 0.5 M KHCO $_3$ to 74 mV dec $^{-1}$ in 2.0 M KOH. This suggests the same mechanism for CO $_2$ reduction to CO despite different [OH $^-$] in the catholyte.

Comparing eCO $_2$ RR in GDE cell with KHCO $_3$ catholyte (Fig. 2b) and KOH catholyte (Fig. 3a), the selectivity of the carbonaceous products is greater with KOH solution than with KHCO $_3$ solutions shown by higher FE in KOH at the same potentials. Also in both KOH and KHCO $_3$ electrolytes, the carbonaceous FE was enhanced with increasing electrolyte concentrations. 1.0 and 2.0 M KOH at -0.17 V had similar FE of carbonaceous products to KHCO $_3$ at -1.17 V. This 1 V shift suggests lower energy required in catholyte with higher alkalinity.

 C_2 products (ethylene and ethanol) were notably produced in KOH catholyte with the concentration higher than 0.5 M. At -1.17 V, the C_2

FE reached almost 40% in 2.0 M KOH. Within the potential range in this study, C_2 selectivity was increased with more negative potentials and higher KOH concentration. Although the highest FE for C_2 was obtained in 2.0 M KOH, the differences between 1.0 and 2.0 M were insignificant indicating the applied potential related to the energy level of the reaction interface at higher pH more critical.

The current density (j) increased with increasing the overpotential and catholyte concentration. Under the same potential, the current density of KOH was much higher than KHCO $_3$ with the same concentration. EIS measurement with the CO $_2$ atmosphere was used to survey the effect of KOH concentration on resistances. The results displayed in Figure S7 and Table S4 indicate that KOH with higher concentration has smaller resistances of solution and charge transfer. The charge transfer resistance decreased with [OH $^-$], corresponding to the increasing exchange current density j_0 shown in Table 2. $-234\,\text{mA}$ cm $^{-2}$ current density was achieved at $-1.17\,\text{V}$ in 2.0 M KOH, with 40% FE of C $_2$. The production rate of ethylene and ethanol was respectively 0.105 mg min $^{-1}$ and 0.035 mg min $^{-1}$ on 2 cm 2 electrode with CO $_2$ flow rate 15 ml min $^{-1}$, implying the industrialisation potential for C $_2$ production.

The high alkalinity catholyte showing improved eCO₂RR kinetics and C₂ selectivity could be due to the adsorbed OH on catalyst surface. Zhang et al. [34] compared eCO₂RRs on three different local oxygen-induced surfaces: 1. fully oxidized Cu₂O surface, 2. partially oxidized Cu(110) – (2 × 1)O surface, 3. presence of OH spectators. The existence of OH groups as spectators on Cu° surface could flip the selectivity between CH₄ and CH₃OH, playing the similar role with the oxidized Cu surface. It has been widely accepted that oxide-derived electrocatalysts applied in eCO₂RR can reduce the energy barrier of CO₂ activation through enhancing the adsorption strength³⁵ and stability of the active species CO* on reaction sites [3,36,37]. The CO* dimerization is the rate determining step of C₂ products formation [38–42], which occurs at high local pH(\geq 12) [43], and easier to take place on an oxygen-induced Cu surface than bare metallic Cu [44,45].

The use of oxide-derived Cu as the catalyst for $\rm CO_2$ reduction has been recognized for the purpose of $\rm C_2$ production in some studies [22,37,44,46,47]. However, $\it J$. Albo et al. [48–50] used $\rm Cu_2O$ with 0.5 M KHCO $_3$ catholyte in a two-chamber cell and found methanol to be the major product, which was not detected in this work. Analyzing the methanol absence in this study compared to their work is hard as different type of Cu oxide catalyst applied. Also, the results above indicate, even with the same $\rm Cu_xO$ catalyst, the distribution of carbonaceous products varied by $\rm CO_2$ supply method, catholyte, and applied potential. XRD and XPS were applied to investigate the status of $\rm Cu_xO$ catalyst and reaction interfaces, as shown in Fig. 4.

Cu_xO applied as the catalyst in this study is a mixture of Cu₂O (main), CuO and Cu as observed in its XRD pattern (Fig. 4a). The reduction of Cu_xO to Cu° has much less negative potential than eCO_2RR as found in the CV results in Figure S3. Thus, under the reaction potential of eCO₂RR, the Cu_xO catalyst should be reduced to Cu° rapidly. The XRD patterns of the two "after reaction" samples indicate the main component in the bulk catalyst after reaction either in 1.0 M KHCO3 or 1.0 M KOH was metallic Cu. However, even though the bulk Cu_xO catalyst reduced to Cu°, the catalytic activity maintained over 4 h with stable C2 FE between 30-40%, as shown in Figure S6, suggesting the catalytic activity of Cu based catalyst may still be from Cu and OH or oxygen groups from oxide-derived catalyst could further reduce the activation energy and be favourable to carbonaceous products formation. XPS which was used to characterise the catalyst surface further proved this. Fig. 4b displays the XPS spectra on Cu_xO-GDE before eCO2RR and after 3 h eCO2RR in GDE cell with 1.0 M KOH and 1.0 M KHCO3. The reduction of the catalyst after reaction is also observed since the satellite peaks of Cu $2p_{3/2}$ and Cu $2p_{2/1}$ on the fresh catalyst are both largely attenuated after reaction [51]. These peaks are stronger mitigated in the "after reaction (KHCO3)" catalyst than those of "after reaction (KOH)", indicating the catalyst surface after reaction remains

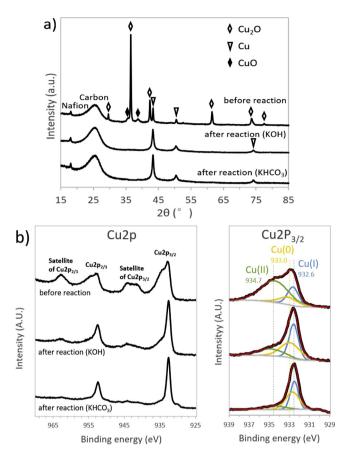


Fig. 4. a) XRD patterns and b) XPS spectra of Cu2P and the peak-differentiating of Cu2P $_{3/2}$ for the Cu $_x$ O-GDE before eCO $_2$ RR and after 3 h eCO $_2$ RR in 1.0 M KOH and 1.0 M KHCO $_3$.

higher oxidation degree in KOH than in KHCO $_3$. The Cu2P $_{3/2}$ photo-electric peak was fitted to quantitatively analysis Cu species [52,53]. The fresh catalyst surface contains 14.65% Cu(0), 21.99% Cu(I), and 63.36% Cu(II). After eCO $_2$ RR, the catalyst surface of "after reaction (KOH)" contains 37.82% Cu(0), 39.92% Cu(I) and 22.26% Cu(II), showing higher oxidation degree than that of "after reaction (KHCO $_3$)" containing 44.31% Cu(0), 41.15% Cu(I) and 14.54% Cu(II). Although the bulk Cu $_x$ O catalyst was substantially reduced to metallic Cu after eCO $_2$ RR, oxidized Cu partially remained on the catalyst surface.

In summary, the OH groups adsorbed on the catalyst surface may partially prevent the oxidised Cu surface from being reduced to metal and reduce the energy barrier of CO_2 activation through enhancing the adsorption strength [35] and stability of the active species CO^* on reaction sites [3,36,37]. Also, the high concentration of OH^- on Cu catalyst surface showed reduced CO-CO coupling energy barrier [47], resulting in enhanced selectivity of C_2 products.

4. Conclusions

In this study, the effects of CO_2 supply method and alkalinity on the selectivity of carbonaceous products, and C_2 products were investigated in aqueous electrolyte using Cu_xO catalyst. The results suggested that GDE cell with CO_2 supplied through gas diffusion has higher selectivity for carbonaceous products and suppression of HER compared to two-chamber cell with CO_2 purging into electrolyte. Faradaic Efficiency of carbonaceous products increased from < 10% in 2C cell to 55% in GDE cell at $-1.17\,V$ in $1.0\,M$ KHCO3. This was primarily due to different reactants for CO_2 electrochemical reduction in GDE and in reaction solution, being CO_2^* and hydrated $H_2CO_3^*$, respectively. The alkalinity of catholyte also had a significant influence on the selectivity of

carbonaceous products leading to higher FE from KOH than KHCO $_3$. Higher FE of C $_2$ products, ethanol and ethylene, were observed from KOH with higher concentration (\geq 0.5 M) and at higher overpotentials (-0.97 and -1.17 V), suggesting C-C coupling process occurring with high concentration of OH at catalyst interface with high energy input. XRD and XPS proved the effect of OH groups on the catalysts surface could be favourable to carbonaceous products formation. At -1.17 V with 2 M KOH, C $_2$ FE achieved at 40% with current density -234 mA cm $^{-2}$, producing 0.105 mg min $^{-1}$ ethylene and 0.035 mg min $^{-1}$ ethanol on 2 cm 2 electrode with CO $_2$ flow rate 15 ml min $^{-1}$. This is promising for further development and scale-up.

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Appendix A. Supplementary data

Supplementary material related to this article can be found, in the online version, at doi:https://doi.org/10.1016/j.jcou.2019.02.007.

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