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# 1 Solution Blow Spinning of Piezoelectric Nanofiber Mat for 2 Detecting Mechanical and Acoustic Signals

3

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25 **Abstract**

26 Solution blow spinning (SBS) technique can produce nanofibers (NFs) mat in large scale  
27 production. In this work, the SBS was used to fabricate piezoelectric polyvinylidene  
28 fluoride (PVDF) nanofiber membranes that can be utilized for energy harvesting  
29 applications. The effect of operating air pressure from (2-5 bar) on the surface  
30 morphology of the NFs has been studied. The structural analysis for crystalline  
31 polymorph  $\beta$ -phase for PVDF powder, casted film, electrospinning and SBS NFs has  
32 also been presented with the aid of Fourier-transform infrared spectroscopy (FT-IR) and  
33 X-ray diffraction (XRD). Piezoelectric characteristics of PVDF NFs mats were tested by  
34 applying impact impulse with different weights from different heights between 1 cm  
35 and 10 cm. The sensitivity of the voltage response increased from 1.71 mV/g to 8.98  
36 mV/g respectively. Besides, the SBS generated PVDF mat is found to be sensitive to  
37 pressure forces in a range of few Newtons with the generated voltage according to  
38 detected sensitivity of 80 mV/N with analysis of the impact of a few Hertz mechanical  
39 vibrations. In addition, the produced SBS nanofibers are applied as an acoustic signal  
40 detector within different acoustic frequencies. The results prove that the  $\beta$ -phase PVDF  
41 nanofibrous membrane produced via the SBS technique has a great potential to be used  
42 as a piezoelectric sensor.

43 **Keywords:** solution blown, piezoelectric nanofiber, energy harvesting

44

## 45 1. Introduction

46 Nanofibers have been widely used as a promising material for various  
47 applications such as energy[1], textile[2], filtration [3]and biomedical engineering[4]. Up  
48 to date, several methods have been utilized for non-woven nanofiber fabrication which  
49 includes template synthesis[5], thermal-induced phase separation [6], self-assembly[7],  
50 melt spinning[8], centrifugal force spinning [9] and electrospinning [10].  
51 Electrospinning is considered to be the most common, versatile and cost-effective  
52 technique for nanofiber production [11]. **Despite these advantages, there are several**  
53 **limitations for needle electrospinning type, such as the required high electric voltage,**  
54 **low production rate, difficulty to obtain 3D structure and repeatability challenge**  
55 [12]. This demands either improvements, with potential large investment, to the existing  
56 electrospinning systems or the development of alternative techniques.

57 SBS became a promising technology for nanofiber synthesis due to its low cost,  
58 higher production rate (compared to electrospinning) and simplicity of the setup[13,  
59 14]. **SBS as a novel technique for nanofiber scaling-up production to make non-woven**  
60 **webs with fiber diameters like those produced by electrospinning.** Medeiros et al.[15]  
61 first developed SBS method in which they combined solution blowing and melt blowing  
62 techniques involving extruding molten polymer through a narrow orifice directly into a  
63 stream of a high-velocity hot air which elongates the molten polymer into fibres[16]. The  
64 setup for SBS consists of a nozzle with unique concentric design through which the

65 polymer solution is ejected by the action of either an inert gas (e. g. nitrogen, argon) or  
66 air that in turn allows quick solvents evaporation [17]. This process usually produces  
67 random non-woven mats comprising micro or nanofibers. Fibres using thermoplastic  
68 polymers such as polyethene oxide (PEO), polyurethane (PU) and polyvinylidene  
69 fluoride (PVDF) were successfully manufactured using SBS technique [13, 18-20] for  
70 potential applications in biomedical and electrical industries. Using SBS, not only fibres  
71 of pure polymers can be produced, but polymer-ceramic composites can also be made  
72 [21].

73 The filtration efficiency of the NF mat produced by SBS ranged from 83.10 % to  
74 93.45 %, and the pressure drop was between 15.37 and 30.35 Pa which is hugely lower  
75 than the reported data for electrospun and commercial membranes. Nylon 6 air  
76 filtration membrane was made through SBS technique with studying the membrane  
77 properties such as thickness and pore size on the filtration performance [16].  
78 Furthermore, PVDF/Ni composite NFs were produced from the SBS method with  
79 superior magnetic properties [19]. The magnetic analysis of the nanocomposite showed  
80 that it has the same behaviour as ferromagnetic materials. At the same time, the zero-  
81 field cooling (ZFC) and field cooling (FC) curves revealed the presence of super  
82 paramagnetic performance which makes it suitable for various applications such as  
83 electric motors and generators. Combined nanofiber fabrication methods via  
84 electrospinning and solution blowing were introduced to produce self-powered non-

85 woven nanogenerator that can be used in wearable electronic textiles[22, 23]. The design  
86 of nanogenerator system consisted of flexible and conductive PVA/PEDOT: PSS mat  
87 prepared by electrospinning and working as an electrode, while the second layer was  
88 the piezoelectric PVDF nanofiber which was prepared by SBS with the aid of high-  
89 pressure airflow. The piezoelectric properties showed high negative and positive output  
90 current of 70 nA and -65 nA at an impact frequency of 3 Hz with high durability and  
91 robustness, which proves the capability of a nanocomposite structure in wearable  
92 electronics and energy harvesting applications.

93 In this study, we have used a facile technique for producing PVDF nanofibers  
94 membrane for piezoelectric applications employing bespoke concentric SBS nozzle  
95 system. The preliminary tests aimed to obtain a highly efficient piezoelectric response  
96 from the SBS mat using different operating air pressures and studying their effect on the  
97 morphological structure of SBS nanofibers. A detailed comparison for the structural  
98 properties of PVDF powder, cast film, electrospinning and SBS has been  
99 investigated through the FTIR and XRD analysis. As an application, our SBS mat was  
100 analysed to detect mechanical vibrations of a few Hz frequency range. In addition, the  
101 developed nanofibers membranes were applied as an acoustic signals detector at  
102 different acoustic spectrum frequencies.

## 103 2. Materials and Methods

### 104 2.1 Materials

105 PVDF (Kynar, melt viscosity: 23.0-29.0) was supplied by ARKEMA (King of  
106 Prussia, PA, USA). N, N-Dimethyl Formamide (anhydrous, 98%) is purchased from  
107 LobaChemie (India). Chemicals have been used without further dilution or  
108 purifications.

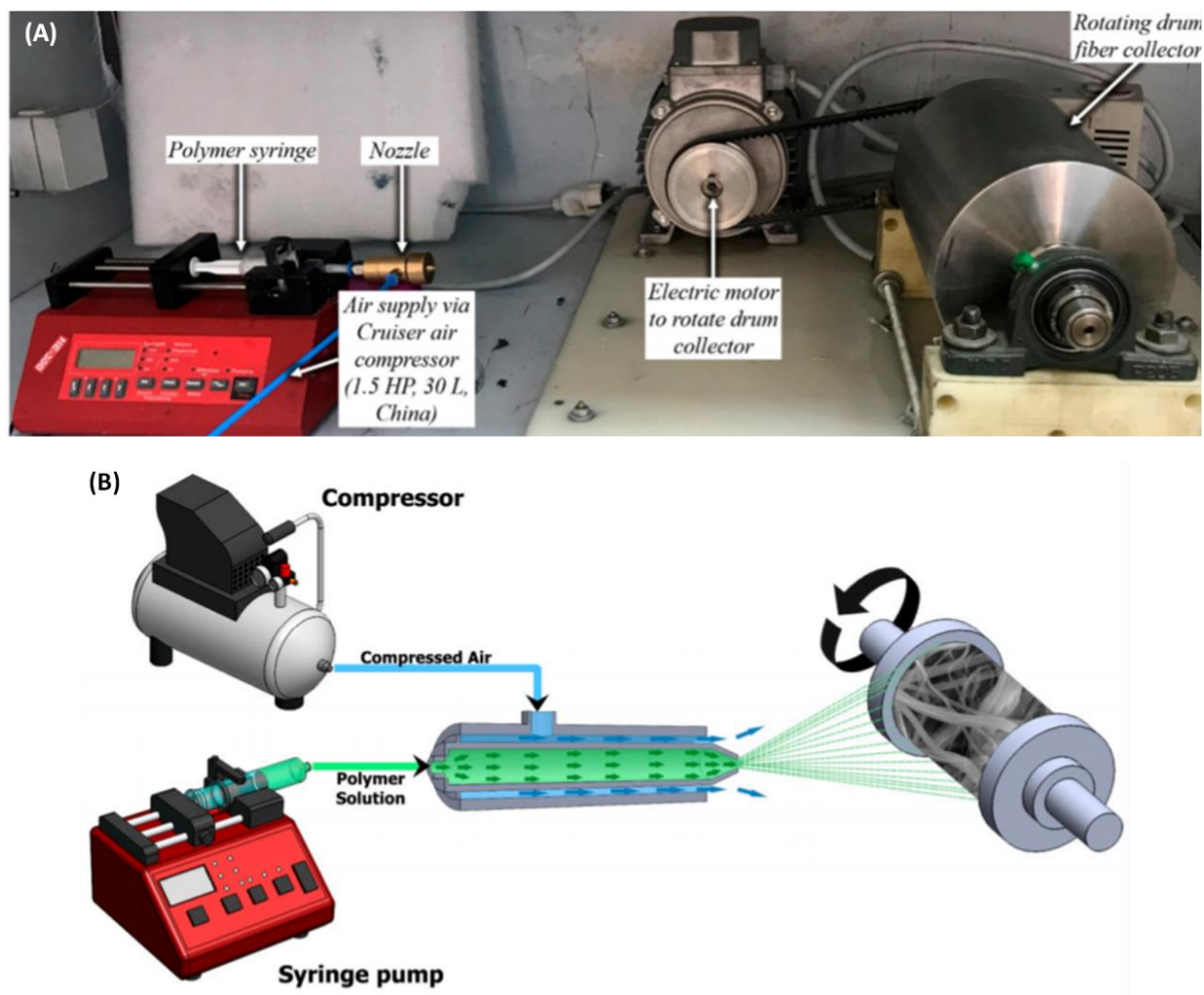
## 109 **2.2 Nanofibers membrane manufacturing**

110 A custom-made SBS concentric nozzle is provided by AREKA group, Turkey for  
111 nanofiber production. Air pressures of 2, 3, 4, and 5 bar using (Cruiser air compressor,  
112 30L, 1.5 HP, China) is used to study the effect of air pressure on the morphological  
113 structure of PVDF nanofibers. 15 wt. % of PVDF polymer solution is pumped with the  
114 aid of NE-300 infusion syringe pump on 10 ml/h flow-rate through a 21-gauge needle,  
115 which is located inside the concentric nozzle with internal diameter  $d_i = 2$  mm at a  
116 working distance of 30 cm between the nozzle and drum collector (Figure. 1)[24].

117 Electrospun PVDF nanofiber and casted film were manufactured to compare the  
118 difference in the crystalline phases between the PVDF structures (Powder, Electrospun  
119 NF, Solution blown NF, and casted membrane). The electrospinning process was  
120 performed using NE1000 syringe pump (New Era Pump Systems, Suffolk County, NY,  
121 USA) to control the flow rate at  $1 \text{ ml h}^{-1}$  at 25 kV through a high-voltage power supply  
122 CZE1000R (Spellman, Hauppauge, NY, USA). A grounded rotating drum collector at  
123 1000 rpm is placed 10 cm away from the needle tip to collect the PVDF nanofibers. The

124 casted membrane was produced using the vapour induced phase separation (VIPS)  
125 technique.

126



127

128 Figure 1: (A) Image of solution blow spinning set up and, (B) Schematic description of the process

## 129 2.3 Material Characterization

### 130 2.3.1 Fibre morphology

131 The morphological structure of SBSPVDF NFs has been observed by the  
132 Scanning Electron Microscope (JEOL, JSM-6010LV-SEM). One sample for each pressure



133 was cut and stacked onto carbon tabs before sputtering with platinum. The average  
134 fibrediameter wasmeasuredusing Image-J softwareatthree different image scales (5  $\mu\text{m}$ ,  
135 10  $\mu\text{m}$  and 50  $\mu\text{m}$ ).

### 136 2.3.2 Physical properties

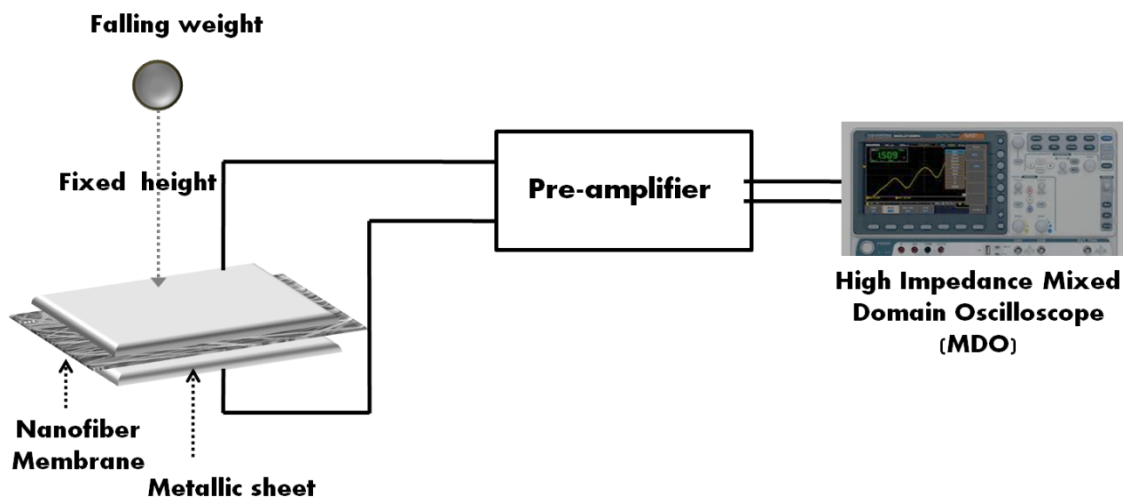
137 The crystalline phase of PVDF powder, cast film, electrospinning and SBS NFs  
138 was determined using X-Ray Diffractometer (XRD) (Shimadzu Xlab 6100 instrument  
139 using Cu as a target), scanning range of 5-80° and scanning speed of 1deg/min for  
140 precise detection of the peaks.

141 Fourier transform infrared spectrometer (FT-IR) (Vertex 70 FT-IR, Bruker,  
142 Billerica, MA, USA) was operated in ATR mode. Samples were scanned 120 times at a  
143 resolution of 5  $\text{cm}^{-1}$  over a range of 4000–400  $\text{cm}^{-1}$ .

### 144 2.4 Piezoelectric measurements

145 Piezoelectric properties of the nanofiber mats were measured using two bespoke  
146 lab setups.The first one is calledimpulse loading, where the peak-to-peak voltage is  
147 detected when letting small masses to freely fall onto the developed nanofibers mats.  
148 The nanofibers mat of 2 cm x 2 cm wasplaced between two aluminiumelectrodesand  
149 exposed toimpulse loading from heights of 1 cm and 10 cm (Figure 2)[25].The generated  
150 voltage wasmeasuredusingtwo shielded wires, pasted on the electrodes, and connected  
151 to high impedance mixed domain oscilloscope (Tektronix MDO3012, Beaverton, OR,  
152 USA). In the othermeasurementsetup, piezoelectric testing was performed using a tool

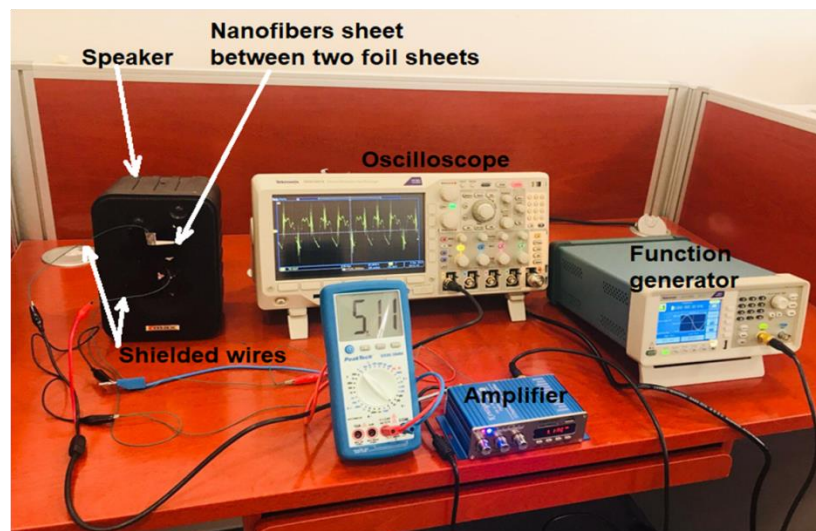
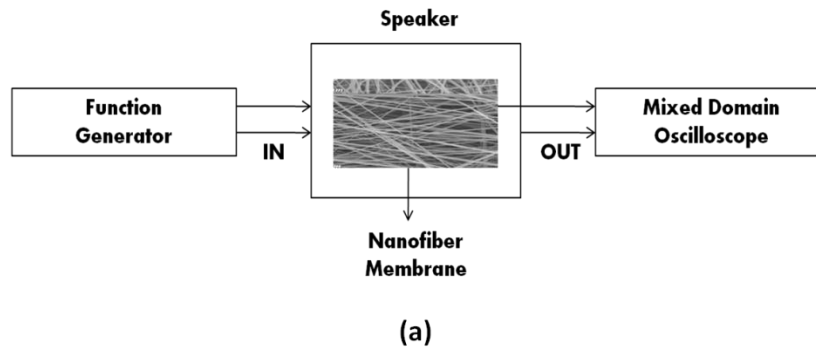
153 designed to control the applied force on PVDF nanofibers through a motorized spring.  
154 Changing the length of the spring could control the applied force on the piezo  
155 nanofibers. The nanofibers mat is inserted between two electrodes and connected  
156 through shielded wires to the previously mentioned oscilloscope. Then, the peak-to-  
157 peak voltage is measured with respect to the change in the applied force within sensitive  
158 range of few Newtons.



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Figure 2. Schematic description of the impulse loading setup

In a modified version of the previously mentioned piezoelectric setup, a source of acoustic signals (Figure 3)[26], which is a Tektronix function generator of Model AFG1062 with frequency range of 60 MHz and sampling rate of 300 MS/s, is connected through an acoustic amplifier to a speaker. Then, the oscilloscope shows the retraced acoustic signals detected by the nanofibers mat.



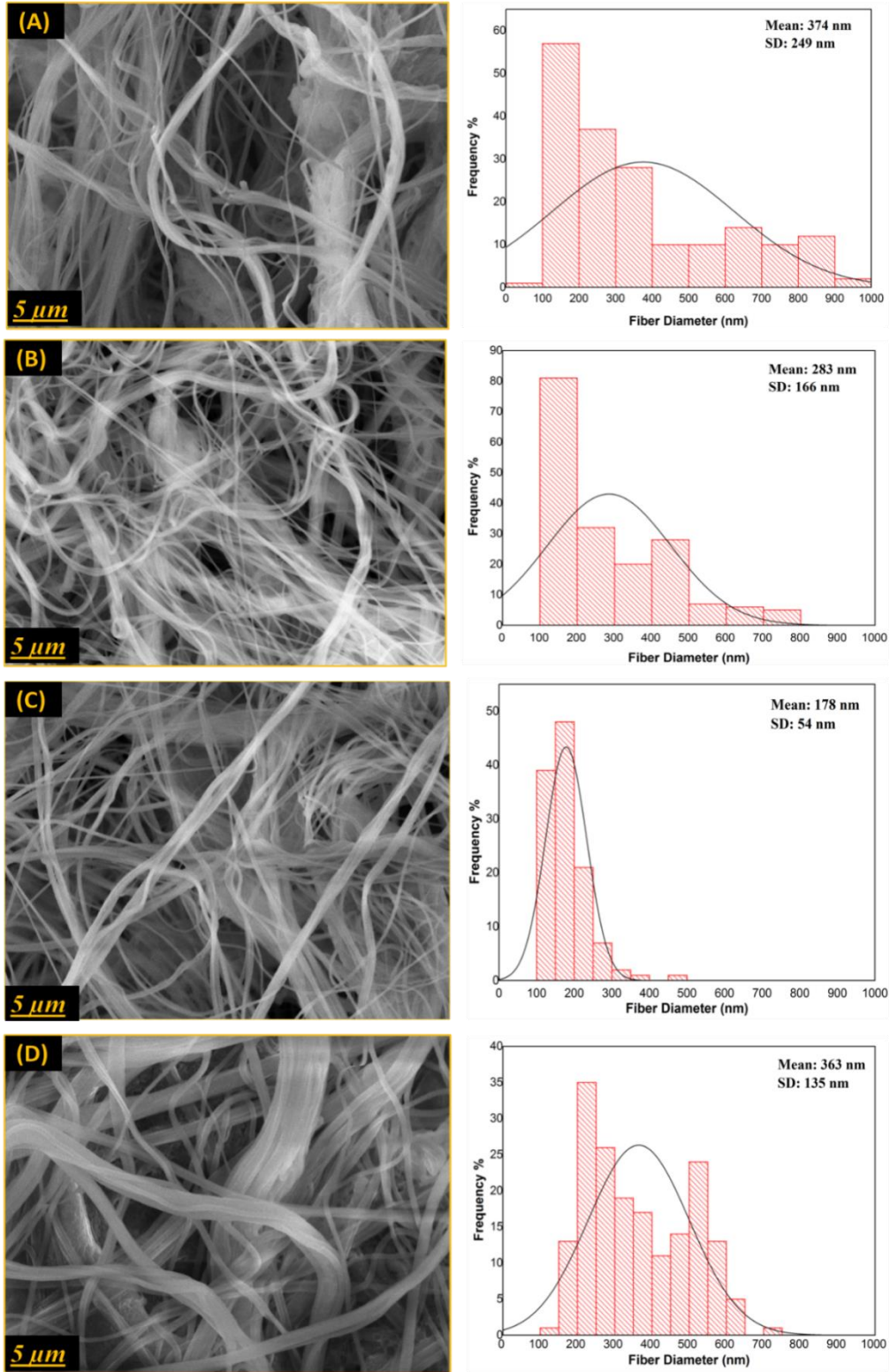
166  
 167 Figure 3. Schematic diagram of the acoustic energy harvesting setup (a), and a picture of the experimental  
 168 setup

169 **3.Results and Discussion**

170 **3.1 Morphological Characterization**

171 Figure 4 shows SEM images and diameter distributions of PVDF NFs produced at  
 172 different air pressures (2, 3, 4 and 5 bars). Clogging and obstruction of the tip nozzle at 2  
 173 and 3 bars were occurred due to the formation and subsequent accumulation of polymer  
 174 droplets which solidified very quickly, thus producing nanofibers with some

175 distributed beads. To overcome the polymer solidification and increase the solvent  
176 evaporation rate, higher operating air pressures of 4 and 5 bars were applied. As shown  
177 in Figure 4(D), stacked bundles were formed with the highest pressure used in this  
178 study (5 bar). The produced nanofibers at 4 bars showed the highest quality in terms of  
179 homogenous network and smaller fibre diameter distribution in the range of 178 nm  
180 without any observed beads or polymer stains. Therefore, these nanofibers produced at  
181 4 bars were chosen for piezoelectric measurements.



182

183

184

Figure4: SEM images for solution-blownnanofiber produced at different air pressure values (A) 2

bar, (B) 3 bar, (C) 4 bar and (D) 5 bar.

## 185 3.2 Structural Characterization

### 186 3.2.1 X-ray Diffraction ( XRD)

187 Figure 5 shows the XRD pattern for rawPVDF powder, casted film, electrospun  
188 and solution blown NFs. PVDF powder showed two distinct broad peaks at  $2\Theta = 18.16^\circ$   
189 and  $26.24^\circ$  and a sharp rise at  $2\Theta = 19.76^\circ$ . These peaks are attributed to the reflection of  
190 021, 020, 110, and 200 monoclinic  $\alpha$ -phase crystalplanes[22, 27, 28]. The casted film  
191 showed similar distribution with two intensive peaks at  $18.06^\circ$  and  $19.6^\circ$  which is  
192 attributed to the  $\alpha$  PVDF phase[28, 29]. The  $\alpha$  phaseof PVDF powder and casted film  
193 has low potential energy and non-polar trans gauge conformation (TG TG) structure due  
194 to the anti-parallel arrangement of the chains[27]. However, when PVDF was processed  
195 using SBS, the PVDF pattern showed a weak shoulder at  $\sim 2\Theta = 18.06^\circ$ depicting the  
196 disappearance of  $\alpha$  crystalline phase. The peak around  $2\Theta = 19.76^\circ$ was shifted to  
197  $20.64^\circ$ which is the diffraction peak on planes 110 and 200,indicating enhanced  $\beta$   
198 crystalline phase owing to the transformation from  $\alpha$  to the  $\beta$  PVDF [22]. The  
199 transformation was the result of the alignment of the  $\beta$  phase, all-trans (TTTT) zigzag  
200 chain conformation as a consequence of the dipole moment direction which is parallel  
201 to the force resulted from the applied air pressurethat stretched PVDF. The dipolesare  
202 perpendicular to the polymer chain causing an increase in the dipole moment, which  
203 results in high polarization.

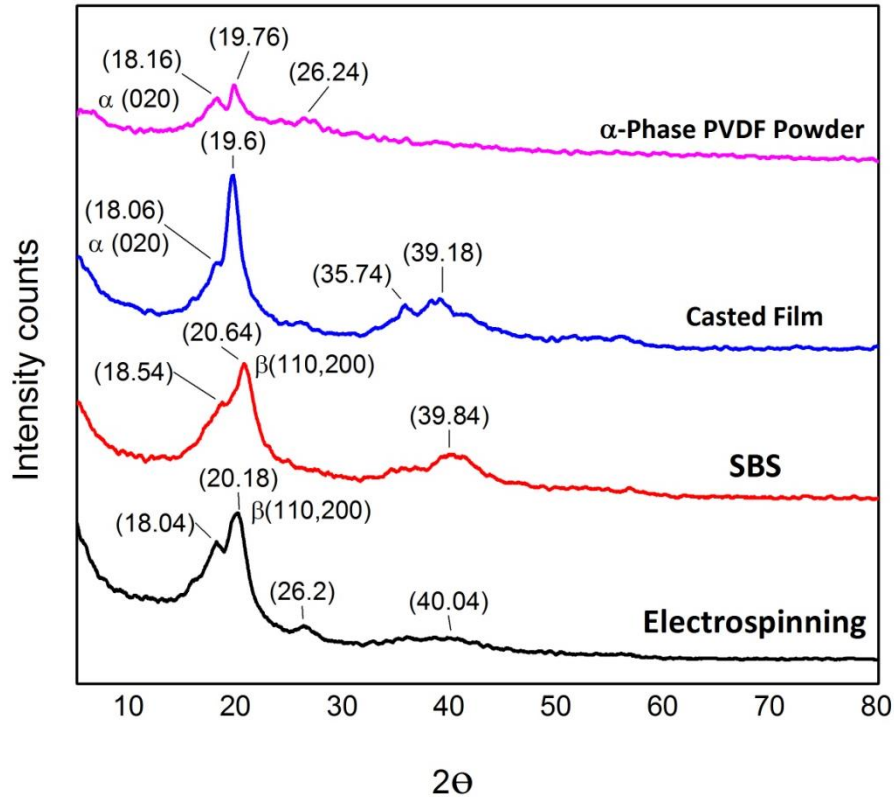


Figure 5: XRD pattern of PVDF powder, cast film, SBS and electrospinning

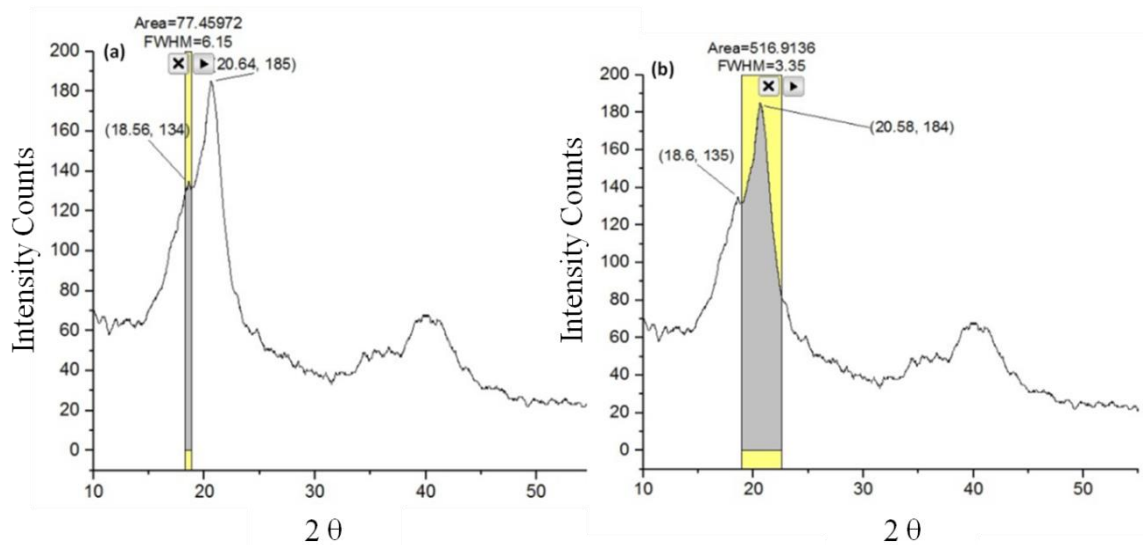
The crystallinity( $\beta$ ) of PVDF NFs produced by SBS technique can be calculated by the peak deconvolution method from the following equation [30].

$$\beta(\%) = \left( \frac{A(\beta)}{A(\alpha)+A(\beta)} \right) \times 100 \% \quad (1)$$

Where  $A_{\beta}, A_{\alpha}$  are the area under the curves of the  $\beta$  and  $\alpha$ , respectively. Origin software was used to calculate the area by the peak integration method as shown in Figure 6a&b. It was found that  $A_{\alpha} = 77.4$  while  $A_{\beta} = 516.9$ , giving the crystallinity of  $\beta$  phase to be  $\sim 87\%$ . Table 1 shows the  $\beta$  phase content for the different PVDF crystalline structures.

215 Table 1: The  $\beta$  phase content for the different PVDF crystalline structures

Sample	Raw powder	Casted film	SBS NFs	Electrospun NFs
$\beta$ -phase content %	No $\beta$ Phase	No $\beta$ Phase	87%	74%



216

217 Figure 6: Calculations of areas under (a) alpha, and (b) beta curves of SBS NFs.

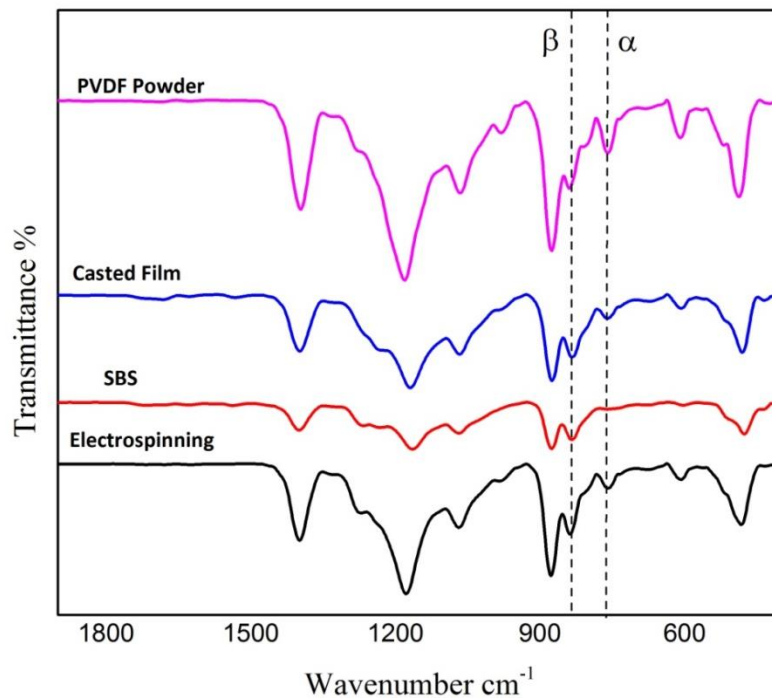
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### 219 3.2.2 FTIR

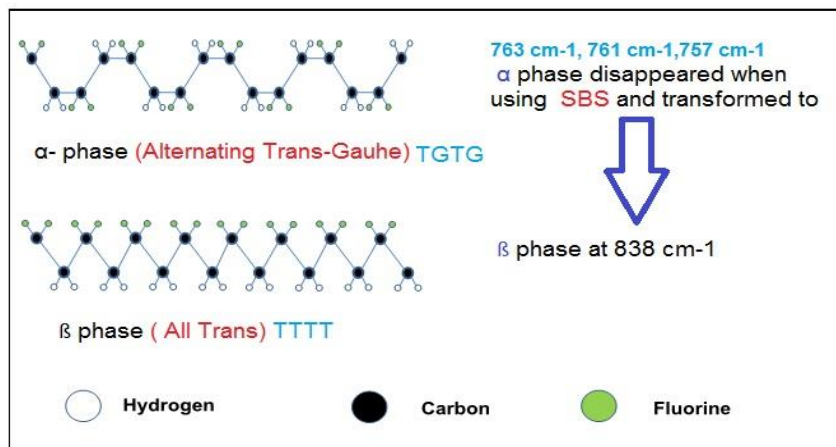
220 Figure 7 displays FTIR spectra for the PVDF NFs manufactured through different  
 221 techniques. A sharp peak was noticed at  $763\text{ cm}^{-1}$  for PVDF powder which is indicative  
 222 of the  $\alpha$  phase [31]. The peaks intensity of the  $\alpha$  phase, which appeared at  $757\text{ cm}^{-1}$  and  
 223  $761\text{ cm}^{-1}$  for electrospinning and cast PVDF NFs. In contrast, the  $\alpha$  phase completely  
 224 disappeared when using SBS for producing PVDF NFs as corroborated by XRD  
 225 results shown in figure 5. The spectra for PVDF powder show a very weak peak at  $\sim 838$



226  $\text{cm}^{-1}$  which could be ascribed to the  $\beta$  phase[32]. This peak appeared sharply with higher  
 227 intensity in PVDF processed through electrospinning, SBS and casting technique. These  
 228 results are in agreement with the XRD results, as discussed earlier. Figure 8 shows the  
 229 difference in monomers arrangement between  $\alpha$ -PVDF (TGTG) and  $\beta$ -PVDF (TTTT).



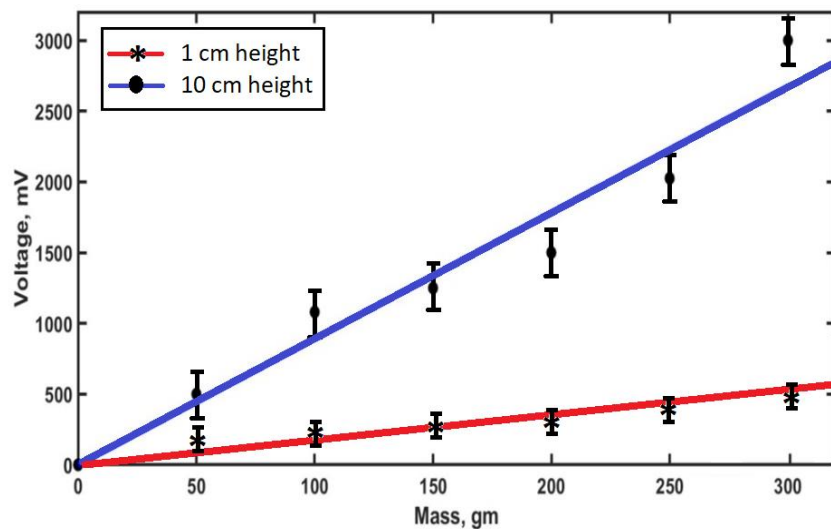
230  
 231 Figure 7: FTIR of PVDF powder, cast film, Solution blown and electrospun nanofibers



232  
 233 Figure 8: The arrangement of monomers in alpha and beta phases of PVDF

### 234 3.4 Piezoelectric Measurements

235 Figure 9 shows the piezoelectric response of the SBS NFs mats under impulse loading  
236 impact from two different heights of 1 cm and 10 cm. The generated electric potential  
237 response increases with increasing weight. The generated electrical potential within a  
238 higher height impulse loading case is higher in both voltage value and sensitivity. The  
239 slope between mean peak-to-peak voltage and applied falling masses, which presents  
240 the sensitivity response, is found to be 8.98 mV/g in case of 10 cm height of falling  
241 masses impulse loading compared to 1.71 mV/g in case of 1 cm height. That indicates  
242 the piezoelectric response of our developed nanofibers mats according to impulse  
243 forces, with increased sensitivity of voltage conversion in case of incremental impulse  
244 force associated to higher falling objects.



245

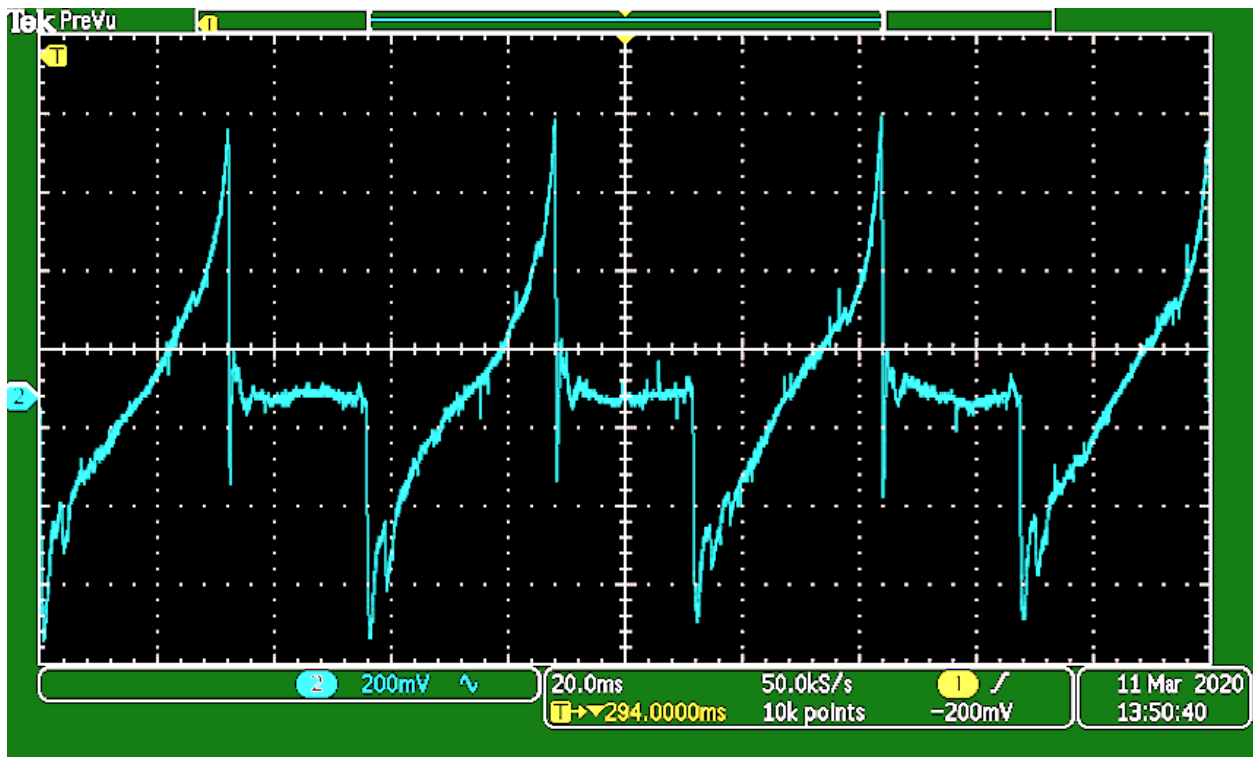
246 Figure 9: Piezoelectric responses (voltage) of solution blown nanofibers mat at both 1 cm and 10

247

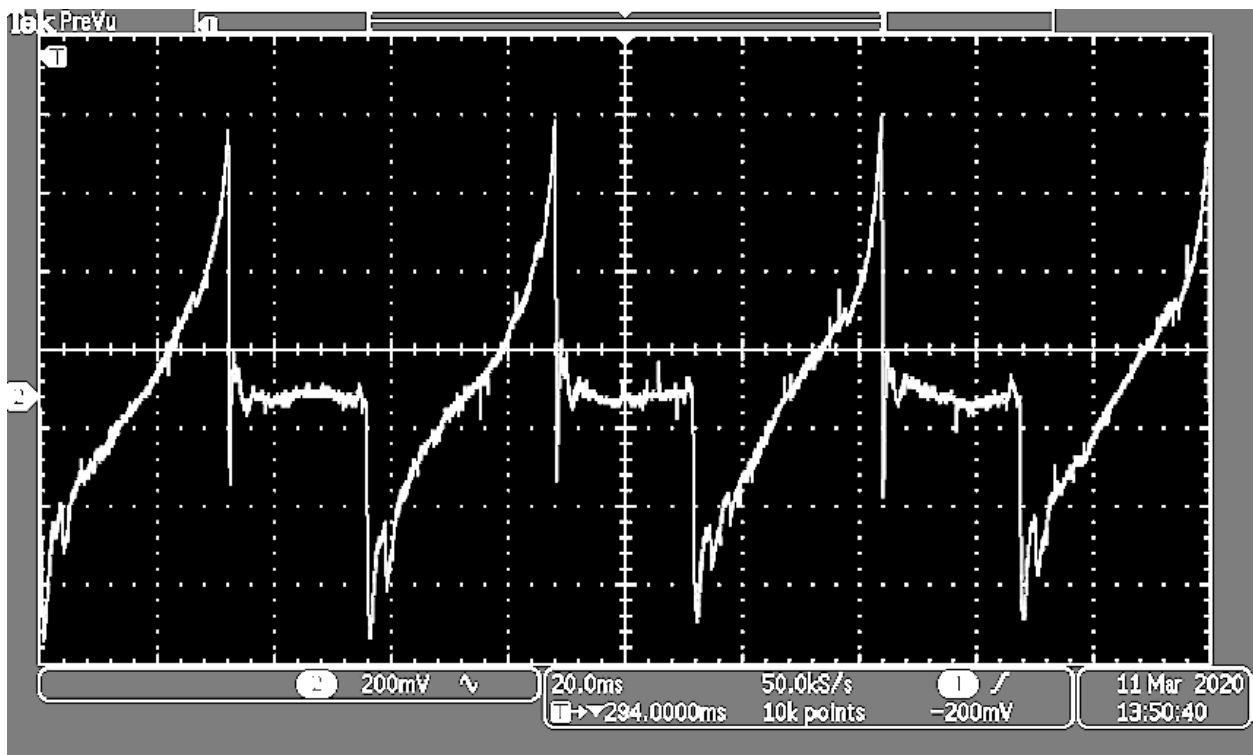
cm impulse loading with different masses.

248 In another piezoelectric analysis, different applied forces were exposed to the  
249 developed PVDF nanofibers mat. Figure 10 shows the generated electric voltage under  
250 applied cyclic forces on the SBS nanofibers mat. Figure 11 shows the output peak-to-  
251 peak voltage at different applied forces. It can be noticed that the developed nanofibers  
252 can be sensitive to a few Newton loads with piezoelectric response sensitivity of 80  
253 mV/Nat cyclic stress of 1 Hz frequency, due to the formed aligned electric dipoles  
254 associated to  $\beta$ -sheets inside SBS nanofibers. Further experiments of the impact of  
255 cyclic frequency of the applied forces have been verified. Figure 12 shows the relation  
256 between generated voltage and the used cyclic forces at different frequencies. At lower  
257 frequency of around 1 Hz, the relationship is relatively linear compared to high-  
258 frequency mechanical vibrations above 8 Hz. Beyond 8 Hz, there is some linearity of the  
259 relationship between voltage and force in particular within the region of applied forces,  
260 as shown in Figure 13. Overall, the piezoelectric sensitivity, which represents the  
261 relation between the applied mechanical forces and the generated electric potential, of  
262 the SBS piezoelectric mats is around 350-500 mV/N over the used frequencies with a  
263 change in the linearity response or slope according to the applied frequency.

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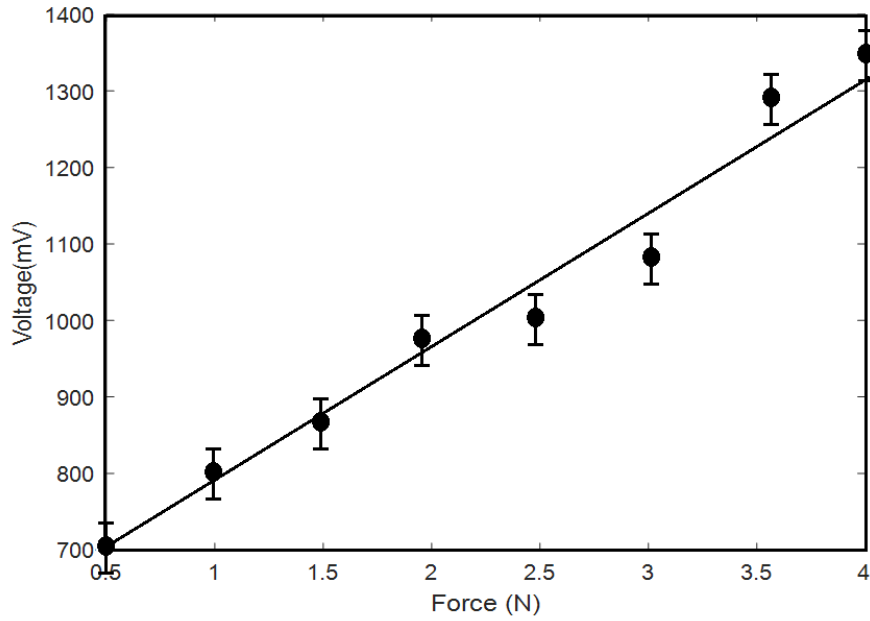


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Figure 10: Electric response of SBS nanofibers mat at a cyclic applied force (y-axis represents the generated voltage and x-axis is the time).



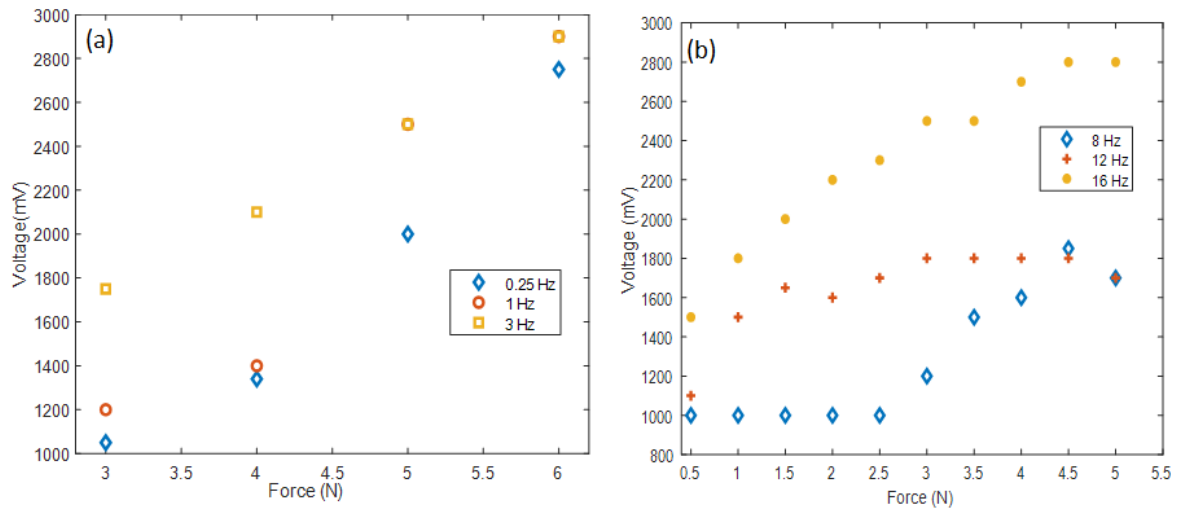
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270

Figure 11. The relation between mean peak-to-peak generated voltage according to different applied

271

forces at 1 Hz.

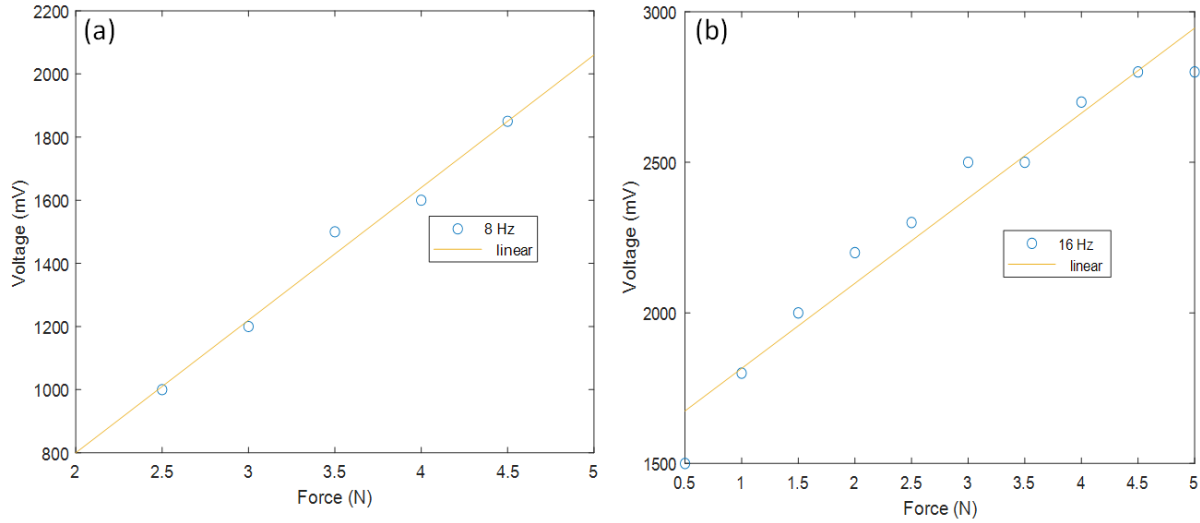


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Figure 12. The relation between mean peak-to-peak generated voltage according to different mechanical

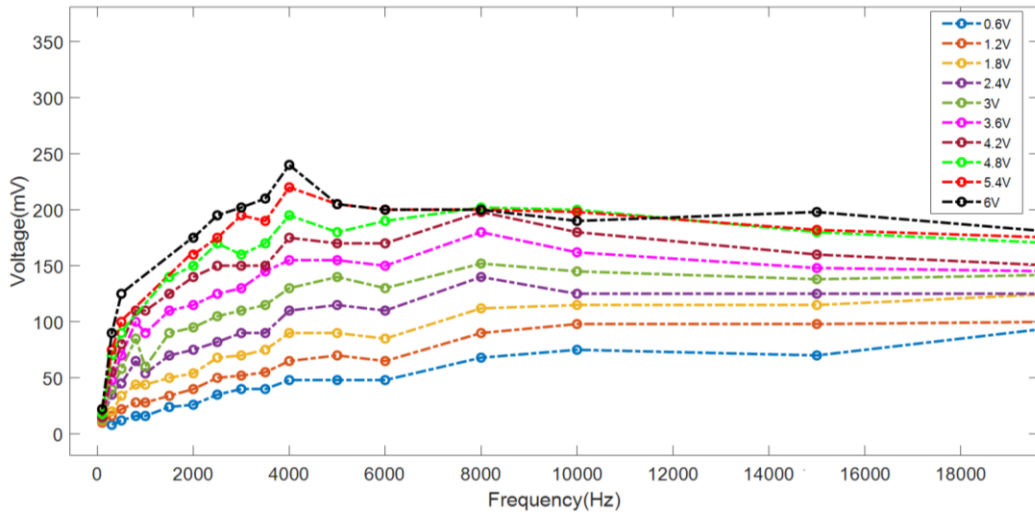
273

forces at different frequencies.



274 Figure 13. Linear fitting of the relation between generated voltage and cyclic force at (a) 8 Hz and (b) 16  
 275 Hz

276 The developed SBS nanofibers mat was also exposed to a wide range of audio  
 277 signal frequencies from 100 Hz to 20 kHz, with a wide range of amplitudes up to 6 V.  
 278 As shown in Figure 14, the output voltage generated from the NFs mat is found to be  
 279 increasing almost linearly for low applied voltage with an increase in frequency upto 2  
 280 kHz. At higher frequencies beyond 5 kHz, there is saturation behaviour in the response  
 281 of the piezoelectric nanofibers against applied acoustic signals at any of the used  
 282 amplitudes. Overall, the level of voltage detected is increasing with increased voltage  
 283 amplitude of the applied acoustic signal. As an example, the detected voltage is plotted  
 284 against the input acoustic amplitude at an acoustic frequency of 2 kHz in Figure 15. It is  
 285 found that there is a linear relationship between both output/input voltages with a  
 286 correlation factor of 30 mV/V.

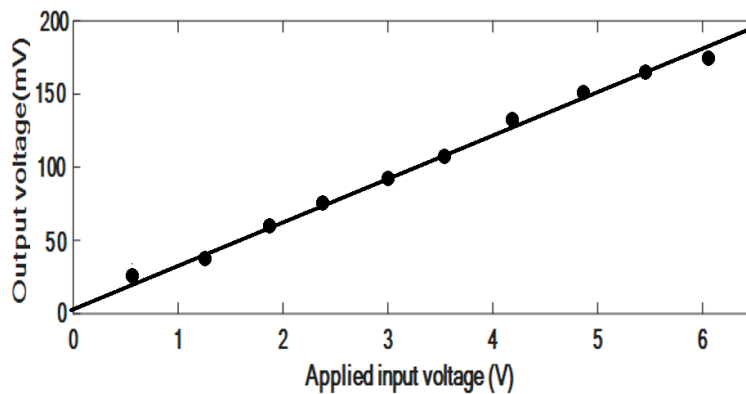


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288

Figure 14. Measured voltage versus frequency at different input applied voltage amplitudes.

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291

Figure 15. The relation between outputs generated voltage against the amplitude of input acoustic signal

292

at the acoustic frequency of 2 kHz.

293

## 294 Conclusions

295

Piezoelectric PVDF nanofiber mats were successfully fabricated by a bespoke SBS setup

296

employing a custom-made concentric nozzle. The produced nanofibrous mat showed

297

homogenous diameter distribution in the range of 200nm. At the same time, the

298 formation of  $\beta$ -phase PVDF through SBS and confirmed by XRD and FT-IR analysis led  
299 to a noticeable increase in the generated electric potential and sensitivity under different  
300 impulse loading up to 8.98 mV/g in case of 10 cm height. Furthermore, the generated  
301 SBS nanofiber mats were sensitive to the applied force of only a few Newtons and  
302 generated electric signals with a sensitivity of up to 500 mV/N at different applied cyclic  
303 vibrational frequencies. As an application to our developed mats, the fabricated SBS  
304 nanofiber mats have been used to detect the audio acoustic signals with linear  
305 behaviour up to 2 kHz acoustic frequency. All of these results demonstrated that  
306 solution blow spinning of PVDF non-woven mats will have several potential  
307 applications and can be used in the large-scale production of energy harvesting devices.

308

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### 316 **Conflicts of Interest**

317 The authors declare no conflict of interest



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