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# 1 Optimization and Design of a Diffuse Optical 2 Wireless Sensor Network

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13 **Abstract:** Wireless sensor networks (WSNs) are currently being deployed in everyday objects  
14 to collect and transmit information related to humidity, temperature, heartbeat, motion, etc. Such  
15 networks are part of the massive machine-type communication scenario (mMTC) within the  
16 fifth/sixth generation of wireless networks. In this paper, we consider the optimization and design  
17 of an optical WSN composed of multiple battery-powered sensor nodes based on light-emitting  
18 diode transmitters. Extending our previous work, we take into account both line-of-sight and  
19 diffuse light propagation, and show that in indoor scenarios, diffuse radiation can improve link  
20 availability under shadowing/blocking and extend battery life. In order to optimize the optical  
21 wireless link parameters, we use a machine-learning approach based on a genetic algorithm to  
22 ascertain the performance limits of the system. The presented results indicate that the proposed  
23 system is a viable wireless option for WSNs within the context of mMTC.

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## 25 1. Introduction

26 The internet-of-things (IoT) [1] constitutes one of the main drivers for the information and  
27 communication technology (ICT) industry. The fifth generation (5G) wireless networks have  
28 identified massive machine-type communications (mMTC) as a key enabler, encompassing  
29 use cases where multiple low-power sensor nodes (SNs) sporadically transmit information at  
30 relatively low data rates. Typical examples include smart-grids [2], smart cities [3], infrastructure  
31 monitoring [4], asset tracking [5], healthcare [6] and others. Wireless sensor networks (WSNs)  
32 composed of spatially distributed SNs within 5G/6G networks come with ever-increasing demands  
33 for higher energy efficiency and longer life spans [7].

34 WSNs offer unique features of network scalability, distributed control, etc. A range of radio  
35 frequency (RF) wireless technologies have been developed for industrial applications [8] but  
36 encounter problems such as tight wireless bandwidth resources, increased crosstalk (especially in  
37 multi-hop scenarios [9]), easy signal interception, fading, and relatively low power efficiency.  
38 Optical wireless communications (OWC) covering the infrared [10] and visible [11] part of  
39 the spectrum are being considered as part of future 5G/6G enabling technologies in certain  
40 applications, where RF-based systems are not the preferred option [12]. Typical applications  
41 include smart manufacturing [13], information proclaiming to the public [14], underwater IoT [15],  
42 intelligent transportation [16], agriculture [17] and smart health-care [18]. OWC-based WSN  
43 may offer higher data throughputs, inherent security, lower energy usage [13], [14]. However,  
44 due to the limitations of line-of-sight (LOS), energy-efficient network models and routing  
45 protocols must be used. In [19], an industrial monitoring system based on an optical camera

46 communication system with an artificial neural network-based group detection mechanism for  
 47 industry applications was proposed and implemented. In [20] and [21], channel modeling and  
 48 characterization of indoor visible light communication for medical body-area networks were  
 49 investigated. In [22], a triple-hop underwater WSN based on the hybrid RF and OWC links  
 50 with the relay between the SNs and the access point was investigated by means of Monte-Carlo  
 51 simulation. In [23], energy harvesting and energy efficient modulation schemes for visible light  
 52 communication (VLC) in industrial applications were investigated.

53 In [24], we studied an indoor OWC-based WSN using a VLC down-link and an infrared (IR)  
 54 up-link to connect master nodes (MN) and SNs. The system under consideration is shown in  
 55 Figure 1. Figure 1a shows a number of SNs that are periodically sending sensor readouts to one or  
 56 multiple MNs using IR OWC up-links. The MN uses a VLC down-link to send acknowledgments  
 57 and coordinate transmissions. Light signals transmitted from the SN can reach the MN through  
 58 the LOS path or via multiple reflections from various surfaces of the room (diffuse path). **Figure**  
 59 **1b shows the transceiver diagram.** At the transmitter (TX), the sensor information modulates  
 60 the intensity of the IR LED(s) via the driver circuit. At the receiver (RX), an optical bandpass  
 61 filter is used for limiting the ambient light noise prior to optical-to-electrical conversion using a  
 62 PIN photodiode and a trans-impedance amplifier (TIA). In addition to the actual sensors, the  
 63 node contains a micro-controller unit (MCU), which coordinates the node data transmission  
 64 cycle. The MN architecture is similar except for exchanging the transmitting/receiving to use a  
 65 LED-based VLC system for simultaneous communication and illumination. Considering the  
 66 LOS contribution only, one may obtain significant battery lifetimes.

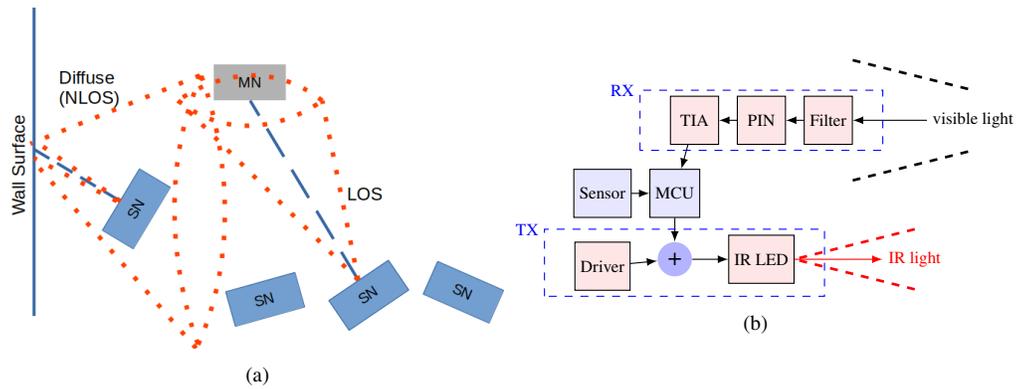


Fig. 1. (a) Hybrid VLC/IR network architecture and (b) SN subsystem.

67 The contribution of the present work lies in several areas. First of all, **we provide a more**  
 68 **practical analysis of the OWC-based WSN.** Compared to our previous work [24], where we only  
 69 **considered LOS, in this work, we now account for the contribution of diffuse light resulting from**  
 70 **beam reflections at various room surfaces.** For relatively high data-rate links, it is well known  
 71 that such reflections may result in inter-symbol interference (ISI) [25]. However, we initially use  
 72 a ray tracing scheme to show that the optical wireless channel can be considered approximately  
 73 flat for the data rates considered in typical IoT applications (i.e., of the order of kb/s). Therefore,  
 74 at the MN RX, diffuse radiation simply adds up to the LOS contribution, thus improving the  
 75 signal-to-noise ratio (SNR). This implies prolonged battery life, which is highly desirable in  
 76 WSNs.

77 Second, we provide an efficient and low-complexity received power estimation scheme in order  
 78 to estimate the link budget, taking into account the diffuse light contribution. Our approach is, in  
 79 fact, a simplified version of the impulse response estimation model presented in [26]. Since the  
 80 diffuse channel can be considered as flat, there is no need to track arrival times of the diffuse

81 components, and hence the power estimation is considerably simplified requiring much less  
82 computational time and memory resources, compared to full-blown ray tracing simulations.

83 Third, we adopt a machine-learning approach based on a specially tailored genetic algorithm  
84 (GA) [27] to optimize link design in terms of the battery life time. Using established diffuse  
85 impulse response estimation models such as those based on ray-tracing would render such  
86 optimizations impractical. Our simplified link budget model discussed above, however, renders  
87 such optimizations feasible. Various parameters are included in the optimization pertinent to the  
88 SN/MN arrangement considering the indoor environment (wall configuration, surface reflectivity,  
89 etc). To the best of the authors knowledge, **such an application of a GA for optimizing the optical  
90 wireless link parameters in the context of IoT applications has not been reported in the literature.**

91 The fourth area of our contribution is the fact that, as evidenced by the obtained results, the  
92 achieved battery life times of the SNs are considerable, indicating the potential of optical wireless  
93 for WSNs. We pay special attention to scenarios where no LOS power is received (e.g. due to  
94 blocking) and show that optimizing the TX beam-width can lead to significant power savings.  
95 Our results can therefore pave the way for adopting optical wireless technologies in the context  
96 of WSNs and IoT.

97 It is worth mentioning that, in every system optimization problem, there are two basic  
98 ingredients: the system model and the optimization engine. The rest of the paper is organized in  
99 order to reflect these two points. Section 2 describes the model developed to describe the OWC  
100 link and the energy usage for the application scenario at hand. Initially, we use ray-tracing to  
101 show that in typical indoor scenarios, the diffuse channel is effectively flat and can therefore  
102 be simply described by a channel gain coefficient. We then outline how the received diffuse  
103 power can be efficiently calculated. For a target up-link bit error rate (BER), we can therefore  
104 estimate the required transmission power and the driving current at the LED of the SN. Given the  
105 transmission cycle of the SN, this information can also be used to estimate the battery life time.  
106 The model of Section 2 then feeds a GA to optimize the battery life of the SNs, which is outlined  
107 in Section 3. Next, Section 4 presents the results obtained and their impact on WSN-based  
108 applications. Section 5 concludes the paper, providing also a research outlook.

## 109 2. System Model

110 We consider two rooms of different dimensions as outlined in Table 1. Configuration A is a small  
111 room and is identical to the one considered in [26], whereas configuration B is a larger room  
112 indicative of office spaces, storage rooms, etc. The reflectivity values in Table 1 correspond to  
113 typical white paint on plasterboard or acoustic tiles for the sidewalls/ceiling and light gray tiles  
114 for the floor.

### 115 2.1. Optical wireless channel

116 The OWC channel is a linear, time invariant (LTI) system described by its impulse response  $h(t)$ .  
117 The LOS contribution is described by a Dirac delta function  $h_{\text{MN}}\delta(t - t_{\text{MN}})$  [26], where  $h_{\text{MN}}$  is  
118 the LOS channel gain,  $t_{\text{MN}} = R_{\text{MN}}/c$  the propagation delay between the SN and the MN,  $R_{\text{MN}}$   
119 their distance and  $c$  the speed of light. The total impulse response  $h(t)$  equals the sum of the  
120 LOS and the diffuse light component  $h_{\text{D}}(t)$ , i.e.:

$$h(t) = h_{\text{MN}}\delta(t - t_{\text{MN}}) + h_{\text{D}}(t) \quad (1)$$

121 We use an in-house Python implementation of the modified Monte Carlo ray-tracing method [28]  
122 to obtain  $h_{\text{D}}(t)$  and then use the fast Fourier transform (FFT) to determine the diffuse channel  
123 frequency response  $H_{\text{D}}(f) = \mathcal{F}\{h_{\text{D}}(t)\}$ , where  $\mathcal{F}\{\cdot\}$  denotes the Fourier transform. We  
124 assume purely diffusive ideal Lambertian reflectors.

125 Figure 2 shows  $H_{\text{D}}(f)$  obtained for the up-link for configurations A and B of Table 1  
126 and for MN positioned in the middle of the ceiling,  $\mathbf{r}_{\text{MN}} = [L/2, W/2, H]$  while the SN is

Table 1. Simulation parameters

Parameter	Config. A	Config. B
Length, $L$	5 m	10 m
Width, $W$	5 m	10 m
Height, $H$	3 m	4 m
Window height, $H_w$	1 m	2 m
Window width, $W_w$	1 m	2 m
Peak spectral irradiance, $p_n$	2 W/nm/m <sup>2</sup>	
Ambient light temperature, $T_K$	5800 K	
Wall reflectivity, $\rho_w$	0.8	
Ceiling reflectivity, $\rho_c$	0.8	
Floor reflectivity, $\rho_f$	0.3	
MN field-of-view, $FOV_{MN}$	$\pi/2$	
SN field-of-view, $FOV_{SN}$	$\pi/2$	
MN orientation, $\mathbf{n}_{MN}$	$\hat{\mathbf{z}}$	
SN orientation, $\mathbf{n}_{SN}$	$-\hat{\mathbf{z}}$	
MN transmission power, $P_{MN}$	6 W	
Maximum SN transmission power, $P_{SN}$	25 mW	
IR LED half intensity angle, $\Phi_{1/2}$	60°	
IR LED pattern order, $m$	1	
IR LED driver curve	TSFF5210 [24]	
Max SN driver current, $I_{max}$	100 mA	
Responsivity model	BPV10NF [24]	
VLC rejection filter model	VTB5051BH [24]	
IR rejection filter model	BPV10NF [24]	
Maximum data rate, $R_{max}$	10 kb/s	
Target error rate, $BER_0$	$10^{-3}$	
Spectral efficiency, $\eta_{eff}$	0.4 bit/s/Hz	
Up-link message length, $L_u$	200 bits	
Down-link message length, $L_d$	200 bits	
Feedback resistance, $R_F$	1 M $\Omega$	
Modulation type	OOK	
RMS voltage noise density, $V_{rms}$	15 nV/ $\sqrt{\text{Hz}}$	
RMS current noise density, $V_{rms}$	400 fA/ $\sqrt{\text{Hz}}$	
Voltage noise corner frequency, $f_{cv}$	1 kHz	
Current noise corner frequency, $f_{ci}$	1 kHz	
Sleep mode current, $I_{SL}$	400 nA	
Wake-up current, $I_{WU}$	1.3 mA	
Read out current, $I_{RO}$	1.3 mA	
Wake-up time, $t_{WU}$	20 ms	
Read-out time, $t_{RO}$	40 ms	
Cycle period, $t_{CY}$	1 min	
Battery capacity, $Q_{TOT}$	220 mAh	

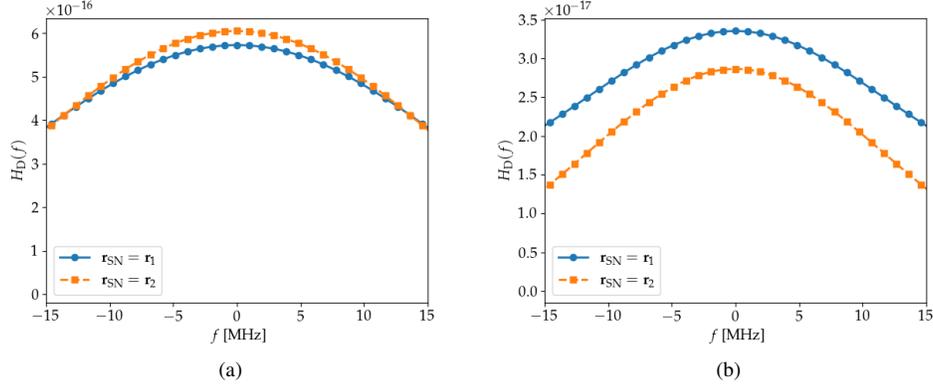


Fig. 2. Diffuse channel impulse response  $|H_D(f)|$  for: a) configuration A and b) configuration B.

127 positioned at two different locations along the floor diagonal:  $\mathbf{r}_{\text{SN}} = \mathbf{r}_1 = [L/2, W/2, 0]$  and  
 128  $\mathbf{r}_{\text{SN}} = \mathbf{r}_2 = [L/4, W/4, 0]$ . The SN and MN are directed according to Table 1. Figure 2a,  
 129 corresponding to configuration A, shows that for both SN positions,  $H_D(f)$  varies in the MHz-  
 130 range and can therefore be considered effectively flat in the sub-MHz frequency range. The half  
 131 width 1 dB bandwidth  $B_{1\text{dB}}$  values of  $|H_D(f)|^2$  are 8.2 and 7.3 MHz for  $\mathbf{r}_{\text{SN}} = \mathbf{r}_1$  and  $\mathbf{r}_{\text{SN}} = \mathbf{r}_2$   
 132 respectively. A similar behavior is obtained for configuration B, where  $B_{1\text{dB}}$  is now 7.2 and 5.3  
 133 MHz for  $\mathbf{r}_{\text{SN}} = \mathbf{r}_1$  and  $\mathbf{r}_{\text{SN}} = \mathbf{r}_2$ , respectively. These results indicate that the diffuse channel can  
 134 be considered flat for WSN applications and can therefore be described by a scalar channel gain  
 135 coefficient  $h'_{\text{MN}}$ . The total channel gain will simply be equal to the sum of the LOS and diffuse  
 136 channel gains:

$$h_{\text{MN}}^{\text{TOT}} = h_{\text{MN}} + h'_{\text{MN}} \quad (2)$$

137 where

$$h'_{\text{MN}} = \int_{-\infty}^{+\infty} h_D(t) dt \quad (3)$$

138 There are two basic aspects of the physical layer model that we present in this section: the link  
 139 budget model discussed in subsection 2.2 and the transceiver model discussed in subsection 2.3  
 140 which includes power consumption.

## 141 2.2. Diffuse power and link budget

142 Assuming a generalized Lambertian-type TX of order  $m$ , located at  $\mathbf{r} = \mathbf{r}_S$ , oriented along the  
 143 unitary vector  $\mathbf{n}_S$ , and a receiver placed at  $\mathbf{r} = \mathbf{r}_R$ , which is oriented along  $\mathbf{n}_R$  and has an effective  
 144 area  $A_R$  and field-of-view equal to FOV, the channel gain is determined by:

$$h(\mathbf{r}_R, \mathbf{n}_R, \mathbf{r}_S, \mathbf{n}_S) = \frac{m+1}{2\pi R^2} \cos^m \phi \cos \theta A_R U\left(\frac{\theta}{\text{FOV}}\right) \quad (4)$$

145 where

$$\cos \theta = \frac{\mathbf{n}_R \cdot (\mathbf{r}_S - \mathbf{r}_R)}{R} \quad (5a)$$

146

$$\cos \phi = \frac{\mathbf{n}_S \cdot (\mathbf{r}_R - \mathbf{r}_S)}{R} \quad (5b)$$

147

$$R = |\mathbf{r}_S - \mathbf{r}_R| \quad (5c)$$

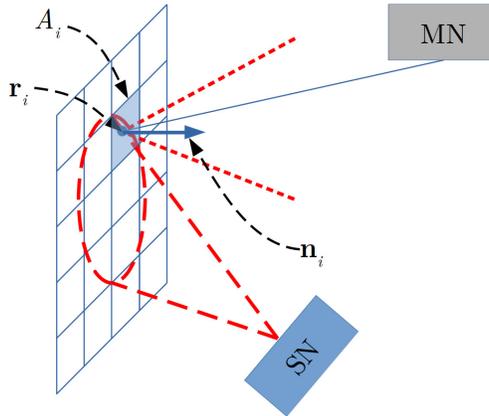


Fig. 3. Estimation of the diffuse light channel gain.

148 As part of our optimizations and in order to avoid adopting time-consuming ray-tracing  
 149 schemes as in Section 2.1, we use a faster simulation method, where all room surfaces are  
 150 represented by a collection of elementary sub-surfaces  $A_i$ , as shown in Figure 3. We first calculate  
 151 the incident power  $P_i^{(1)}$  on each  $A_i$  from the SN using (4), i.e., at the first light bounce. We  
 152 also calculate the intra-subsurface LOS gain  $h_{qp}$  assuming  $A_p$  and  $A_q$  are the TX and the RX,  
 153 respectively. For  $A_p$ , the transmit power is  $r_p P_p^{(0)}$ , where  $r_p$  is the reflectivity of  $A_p$ . Following  
 154 the second bounce, the power received by  $A_q$  is written as the sum of powers received by all  
 155 other elementary surfaces. More generally, the power received at the  $b^{\text{th}}$  bounce is given by:

$$P_q^{(b)} = \sum_{p=1}^{N_E} h_{qp} r_p P_p^{(b-1)} \quad (6)$$

156 In (6),  $N_E$  is the number of elementary surfaces within the room. If  $h_q^{\text{MN}}$  are the channel gains  
 157 assuming  $A_q$  is the TX and MN the RX, then the diffuse-light power  $P_D^{(b)}$  is the sum of the  
 158 received power from all  $A_q$  and therefore, the total diffuse power is given as:

$$P_D = \sum_{b=1}^{N_B} P_D^{(b)} = \sum_{b=1}^{N_B} \sum_{q=1}^{N_E} h_q^{\text{MN}} r_q P_q^{(b)} \quad (7)$$

159 where  $h_q^{\text{MN}}$  is the channel gain between  $A_q$  and the MN. Using (6) and (7) is analogous to the  
 160 impulse response estimation adopted in [26], except that the channel here is considered to have  
 161 flat response, and hence we simply add power contributions from consecutive bounces, speeding  
 162 up computations significantly.

163 Assuming the SN is positioned on various points along the diagonal  $\mathbf{r}_{\text{SN}} = [x, x, 0]$  and its  
 164 orientation is vertical, i.e.  $\mathbf{n}_{\text{SN}} = \hat{\mathbf{z}}$ , we have investigated the power distribution profiles  $P_D^{(b)}$  in  
 165 Figure 4a for configuration B. Interestingly enough, the power for  $b = 1$  is smaller than  $b = 2$ .  
 166 For  $b = 1$ , most of the IR power illuminates the ceiling elements and therefore lies outside the  
 167 field-of-view (FOV) of the MN. For  $b = 2$ , the MN captures optical power from sidewall elements  
 168 that are now illuminated by the ceiling. Figure 4b, depicts the power distribution profiles for the  
 169 LOS and diffuse paths, as well as the total power level for configuration B. Note that, near the  
 170 center of the diagonal ( $x \cong L/2$ ), the LOS path is much stronger than the diffuse path. This is  
 171 because for  $x \cong L/2$ , the alignment is optimal, since both  $\mathbf{r}_{\text{SN}}$  and  $\mathbf{r}_{\text{MN}}$  lie on the line between  
 172 the transceivers. Near the edges of the room, the diffuse component contributes greatly to the  
 173 total received power, since alignment is worse.

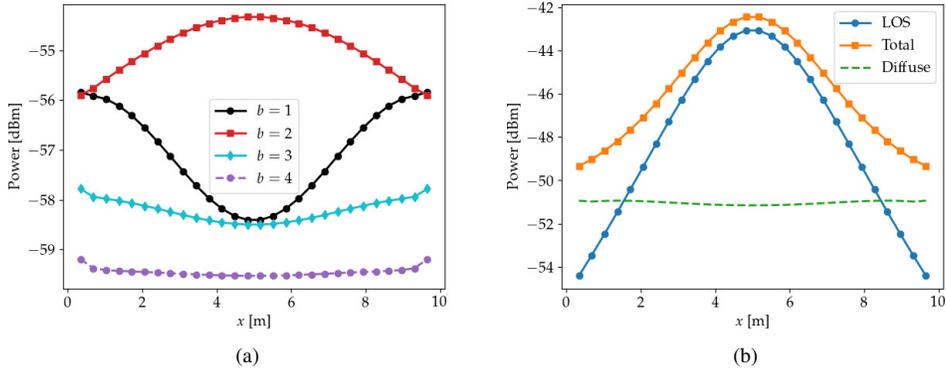


Fig. 4. a) Diffuse power contribution depending on bounce  $b$  and b) comparison of each propagation path contribution to the received power.

### 174 2.3. Transceiver model and energy efficiency

175 The transceiver model includes the transmission spectra of nodes, RX filter spectra, photodiode  
 176 responsivity, ambient light noise and TIA noise. Here we briefly describe the model features and  
 177 the interested reader is referred to [24] for an in-depth analysis.

178 The SN transceiver is modeled based on the characteristics of the TSFF5210 IR LED and the  
 179 VTB5051BH silicon photodiode with an IR rejection filter (Table 1). The IR LED transmission  
 180 spectra  $S_T(\lambda)$  is described by a Gaussian profile with a full width at half maximum (FWHM) of  
 181  $\Delta\lambda = 40$  nm, peaking around  $\lambda = 870$  nm. The optical power-current characteristic  $P_T = f(I_D)$   
 182 is obtained by polynomial fitting of the actual light-current curve of TSFF5210. We assume a  
 183 super-Gaussian profile for the IR rejection filter of order 3 with a 10 dB bandwidth of 230 nm  
 184 peaking at 435 nm while the responsivity  $\mathcal{R}(\lambda)$  of the detector is described by a polynomial with  
 185 respect to  $\lambda$  with coefficients extrapolated by curve-fitting from the BPV10NF responsivity.

186 The MN transceiver is modeled based on typical spectra of warm white phosphorescent  
 187 LEDs [29]. We describe the transmission spectra using a sum of two Gaussian profiles,  
 188 corresponding to the blue and the phosphor components peaking at 470 and 600 nm, respectively,  
 189 with FWHM equal to 20 and 100 nm, respectively. The daylight blocking filter is described by  
 190 a 3rd order super-Gaussian peaking at 870 nm with a 10 dB bandwidth of 300 nm. Given the  
 191 spectral properties of the transceiver, we determine the effective responsivity  $\mathcal{R}_{\text{eff}}$  describing  
 192 the matching between the transmission spectra, the receiver's rejection filter and responsivity.  
 193 Following the approach of [24], we obtain 0.49 and 0.32 A/W for  $\mathcal{R}_{\text{eff}}$  in the up-link and down-link,  
 194 respectively.

195 The RX noise is mainly due to the ambient light-induced shot noise and the TIA thermal noise,  
 196 where the former is usually dominant and can be characterized by its spectral irradiance, which  
 197 in our model follows a black-body radiation model with an absolute temperature of 5800 K.  
 198 Given the position and orientation of the emitting surfaces (e.g. windows), (4) can be modified  
 199 to estimate the ambient light power incident at the RX. We assume a 1 and 4 m<sup>2</sup> window for  
 200 configurations A and B, respectively, (Table 1) with a peak spectral irradiance of 2 W/nm/m<sup>2</sup>.  
 201 We note that,  $\mathcal{R}_{\text{eff}}$  for ambient light is 0.09 A/W for the MN and 0.13 A/W for the SN [24].  
 202 Assuming on/off keying (OOK) modulation, then for a given SNR the transmit power  $P_T$  and  
 203 thus the LED drive current  $I_D$  can be determined. The energy usage at the SN can be calculated  
 204 considering the currents drawn by the transceiver and the MCU during various phases. Table  
 205 1 quotes typical values for each cycle [24]. Based on these, we can calculate the charge  $Q_{\text{CY}}$   
 206 drawn from the battery at each cycle and determine the node battery lifetime  $t_{\text{BL}}$  given the battery

207 capacity  $Q_{\text{TOT}}$  (assumed 220 mAh, typical of a coin-cell battery).

### 208 3. Link Optimization

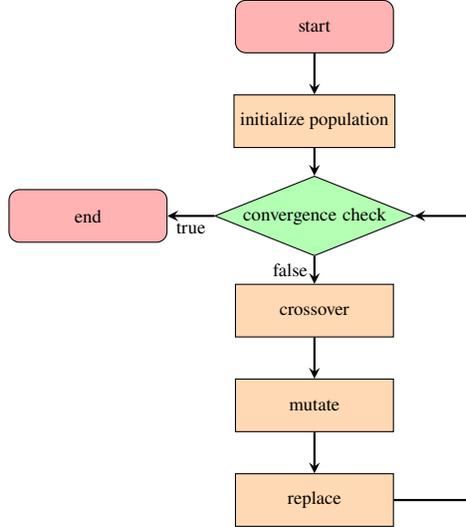


Fig. 5. The flowchart of the genetic algorithm used in this work.

209 In Figure 5, we show the flowchart of the GA used to optimize the system parameters such as  
 210 the SN orientation and data rate. Initially, we randomly choose a population consisting of  $N_{\text{INIT}}$   
 211 realizations of the system (chromosomes). The algorithm then proceeds to select candidates by  
 212 generating offsprings using a *crossover* operation, which transfers part of the parent genes to the  
 213 offsprings. The genes of the offsprings are also *mutated*, i.e. randomly changed in an attempt to  
 214 increase diversity. If a chromosome is produced that is stronger than the weakest chromosome  
 215 in the existing pool, then the former chromosome is replaced by the latter. We then carry out  
 216 a convergence check to see whether the algorithm’s termination criteria are met and if not, we  
 217 repeat the previous steps.

218 In each iteration, the strongest 50 % of the chromosomes constitute the mating pool. We  
 219 choose two parents through tournament selection and we calculate the offspring using uniform  
 220 crossover, which consists of tossing an unbiased coin and randomly selecting the value of each  
 221 offspring gene from either the first or the second parent. The mutation is achieved by adding a  
 222 random correction factor  $\Delta v_k$  to each of the offspring genes  $v_k$ . The corrections are determined  
 223 by  $\Delta v_k = \alpha \beta_k v_k$ , where  $0 \leq \alpha \leq 1$  is the *mutation factor*, and  $\beta_k$  are randomly chosen from a  
 224 uniform distribution inside  $[-1, 1]$ . The chromosome values considered for the optimization  
 225 are the inclination and azimuth angles  $\theta$  and  $\phi$ , respectively, as well as the data rate  $R_b$ . The  
 226 angles determine the orientation of the SN,  $\mathbf{n}_{\text{SN}} = [\cos \phi \sin \theta, \sin \phi \sin \theta, \cos \theta]$ , while  $R_b$   
 227 is related to the required bandwidth  $B$  and the transmission time  $t_{\text{TX}}$ . Note that, the strength of  
 228 each chromosome is determined by a fitness function. In our case, we let  $t_{\text{BL}}$  determine the  
 229 fitness of each system in order to optimize the energy efficiency at the SN. It is important to  
 230 ensure that the maximum driving current should not exceed a specified value  $I_{\text{max}}$  due to the  
 231 LED specifications, see Table 1. If this condition is not met, we set the fitness value equal to zero  
 232 to avoid a non-viable solution.

233 The overall model including the GA which is available under an open-source license [30], is  
 234 implemented in Python using standard libraries such as `numpy`, `scipy` and `matplotlib`.  
 235 In order to speed-up the code execution, we choose to rely on vectorization, avoiding loops as

236 much as possible. For example, it is much more efficient to determine all intra-channel gains  $h_{qp}$   
 237 simultaneously using a vector/matrix approach. In addition we only need to calculate  $h_{qp}$  once,  
 238 since they only depend on the positioning and orientation of the sub-surfaces  $A_q$ . This speeds up  
 239 the fitness evaluations considerably. In our simulations we also took advantage of Python's  
 240 multiprocessing package to distribute computations in multiple processor cores. **The full**  
 241 **link and energy consumption models and the optimization engine of our proposed approach,**  
 242 **implemented in Python, are freely made available under an open-source license [30].**

#### 243 4. Results and Discussions

244 In the proposed optimization scheme, we seek to determine the optimal values of  $[\phi, \theta, R_b]$   
 245 for every position in the floor diagonal  $\mathbf{r}_{SN} = [x, x, 0]$ . We examine three cases: in the first  
 246 and second variations, we only account for either the LOS or diffuse light power, respectively,  
 247 when calculating  $t_{BL}$ . In the third variation, we sum up both contributions. The population  
 248 has  $N_{INIT} = 50$  chromosomes and we use a mutation factor  $\alpha = 0.1$ . The algorithm terminates  
 249 when either a maximum number of crossovers occurs (in our case 20000) or the population's  
 250 fitness values  $f_i$  do not differ significantly from each other. The population fitness smoothness  
 251 is determined as  $S = (f_{max} - f_{min})/f_{max}$  where  $f_{max}$  and  $f_{min}$  are the maximum and minimum  
 252 values of  $f_i$ , respectively. We terminate the algorithm if  $S < 0.05\%$ .

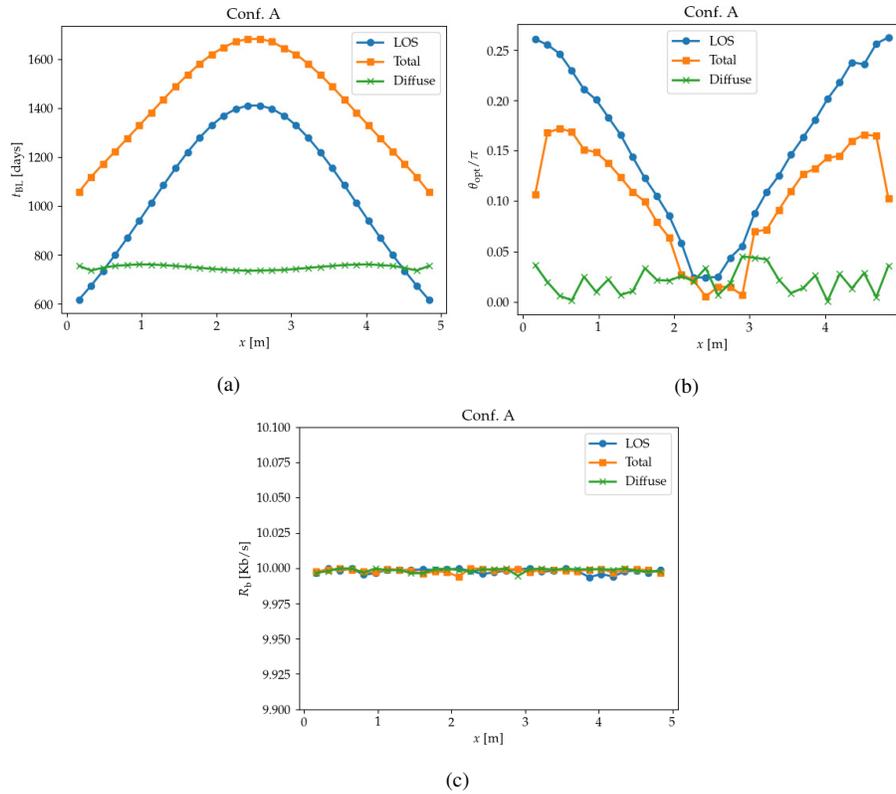


Fig. 6. Optimization results for room configuration A: a) battery lifetime, b) optimal elevation angle and c) optimal data rate

253 Figure 6a depicts the fitness function (i.e.  $t_{BL}$ ) across the diagonal of the room  $[x, x, 0]$   
 254 obtained by the GA for configuration A, assuming LOS, diffuse and a combination of both. It is

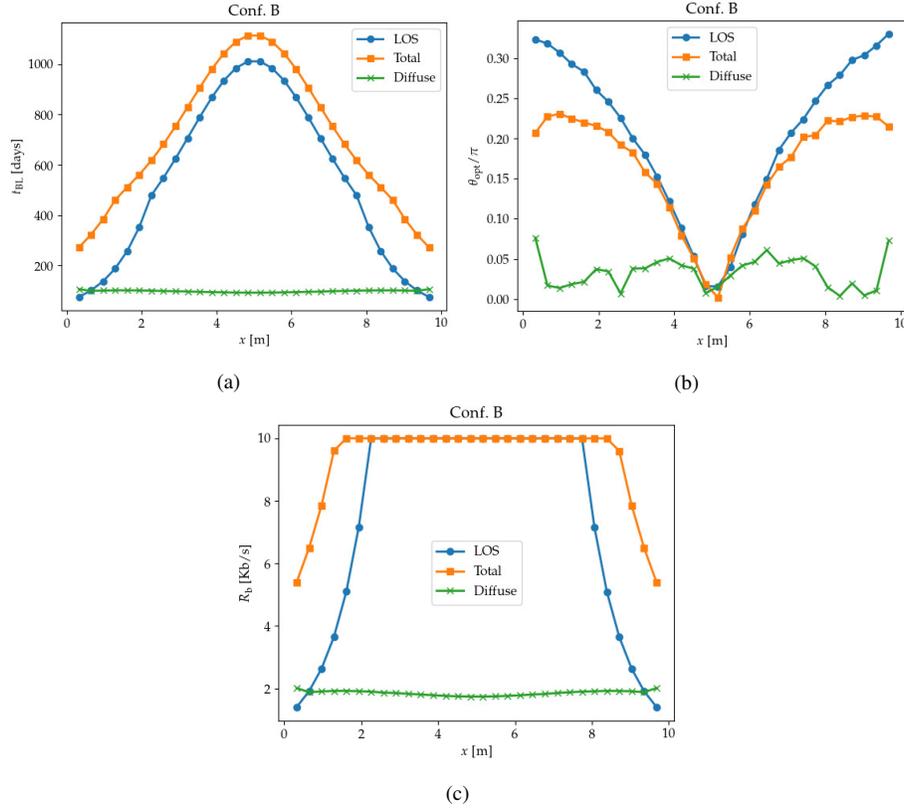


Fig. 7. Optimization results for room configuration B: a) battery lifetime, b) optimal elevation angle and c) optimal data rate

255 interesting to note that the LOS component  $t_{BL}$  is symmetrical around 2.5 m with a peak value of  
 256 1400 days dropping at a rate of 400 day/m compared to the diffuse, which is almost flat at 750  
 257 days, for  $0 \leq x \leq 5$  m. This is due to the fact that as the MN/SN distance is increased, the power  
 258 budget worsens. Considering both LOS and diffuse components, energy efficiency is improved  
 259 particularly near the edges of the diagonal. Figures 6b and 6c show the optimal elevation angle  
 260  $\theta$  and the data rate  $R_b$ . For LOS, the optimal  $\theta$  increases when we move away from the center  
 261 ( $x = 2.5$  cm) to better align with the MN, whereas the diffuse scenario favors  $\theta \approx 0$ , in which  
 262 case the SN is almost pointing directly upwards,  $\mathbf{n}_{SN} \approx \hat{\mathbf{z}}$ . The obtained data rate is given by  
 263  $R_b \approx 10$  kb/s =  $R_{max}$ , which is the maximum allowable value given by system constraints. The  
 264 fact that higher  $R_b$  are favored can be explained through the RX electrical SNR in the case of  
 265 OOK, given as:

$$\text{SNR} = \frac{R_{\text{eff}}^2 P_R^2}{2\sigma^2} \quad (8)$$

266 where  $P_R$  is the received optical signal power (proportional to the transmit power  $P_T$ ) and  $\sigma^2$   
 267 is the RX noise power. Neglecting the TIA noise, we have  $\sigma^2 = 2qI_{\text{amb}}B$ , where  $I_{\text{amb}}$  is the  
 268 DC current due to ambient light,  $q$  is the electron charge,  $B = R_b/\eta_{\text{eff}}$ , the signal bandwidth  
 269 and  $\eta_{\text{eff}}$  is the spectral efficiency. Thus, with reference to (8),  $P_T \propto \sqrt{R_b}$ . Assuming linear  
 270 light-current characteristic at the SN LED, we can also deduce that  $I_D \propto \sqrt{R_b}$ . Since the duration  
 271 of the transmission phase  $t_{TX}$  is proportional to the bit duration  $1/R_b$ , we readily see that the  
 272 charge drawn from the node battery is  $Q_{TX} \propto 1/\sqrt{R_b}$ . This implies that provided that  $I_D \leq I_{\text{max}}$ ,

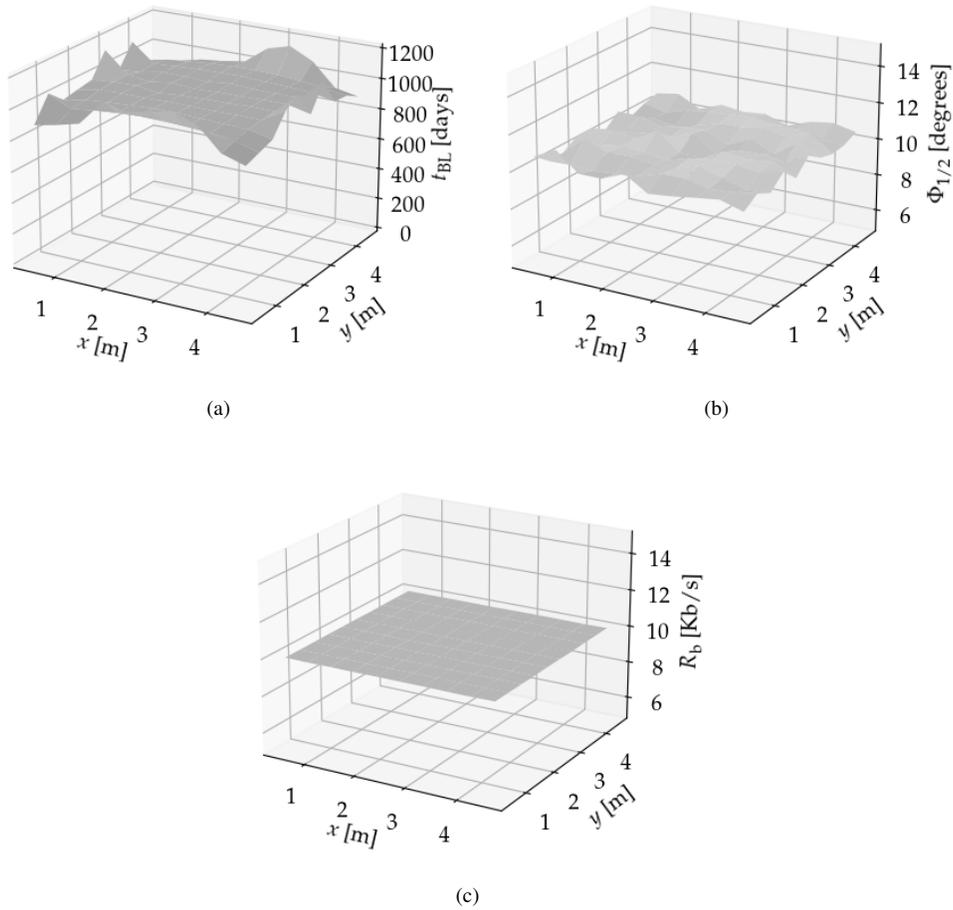


Fig. 8. Optimization results for diffuse light propagation configuration A: a)  $t_{BL}$ , b)  $\Phi_{1/2}$  and c)  $R_b$ .

273 increasing  $R_b$  leads to improved energy efficiency.

274 Figure 7 shows the optimized results for configuration B. As shown in Figure 7a, the diffuse  
 275 path offers the lowest battery lifetime with an average of  $\approx 96$  days. However it can still increase  
 276 the overall battery lifetime considerably, especially at the edges of the diagonal. The optimal  
 277 elevation angles exhibit a similar variation as those in Figure 6b, implying that if the diffuse  
 278 component alone is considered, the optimal SN orientation is still  $\mathbf{n}_{SN} \approx \hat{\mathbf{z}}$ . As expected, the  
 279 optimal SN elevation angles increase with the distance from the floor center, in order to improve  
 280 SN/MN alignment. Figure 7c depicts the optimal data rate, which is not always  $\approx 10$  kb/s since  
 281 the required driving current must not exceed  $I_{max}$ . Considering only the diffuse component, the  
 282 optimal  $R_b \approx 2$  kb/s. For the LOS component,  $R_b$  is much higher except for the points near the  
 283 edge of the diagonal. Assuming both contributions from LOS and diffuse paths, we obtain an  
 284 optimal data rate  $\geq 5$  kb/s for all SN positions considered (orange curve in Figure 7c).

285 For the LOS path, an obvious way to improve the link budget is to choose a smaller beam-width  
 286  $\Phi_{1/2}$  thereby reducing beam spreading at the expense of tighter alignment control and limited  
 287 mobility. It is interesting to investigate the optimal beam pattern for the diffuse path as well

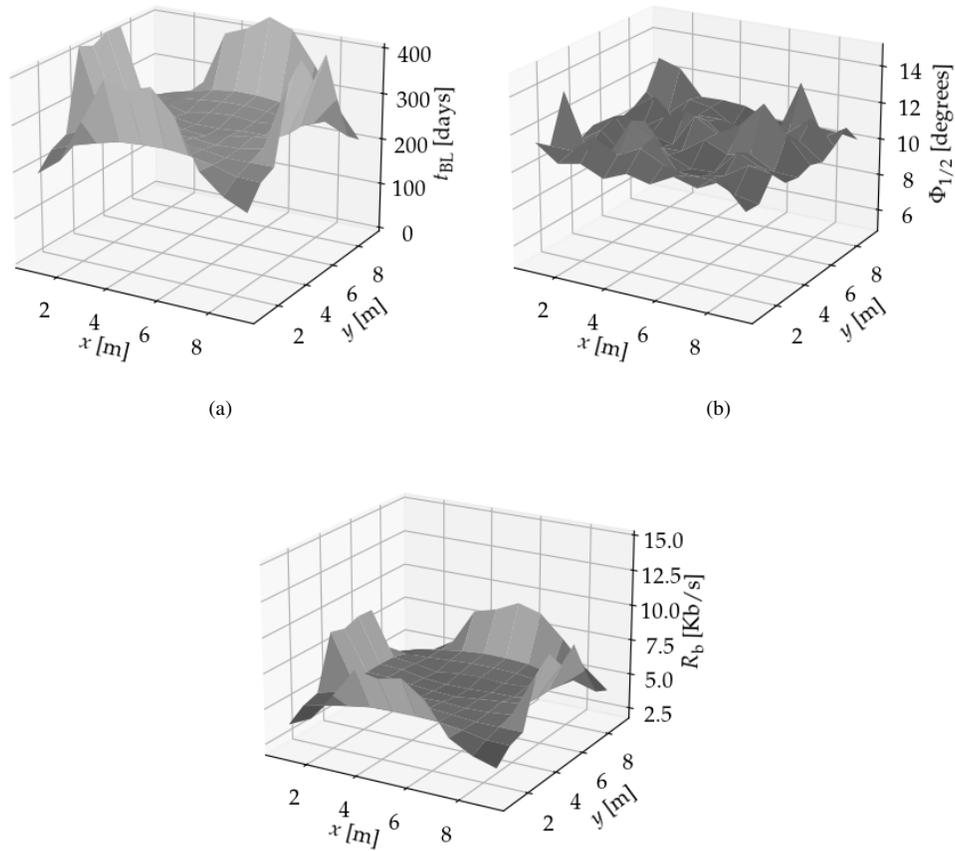


Fig. 9. Optimization results for diffuse light propagation configuration B: a)  $t_{BL}$ , b)  $\Phi_{1/2}$  and c)  $R_b$ .

288 considering many possible positions for the SN. Figures 8 and 9, show the results for the two room  
 289 configurations assuming that the beam-width  $\Phi_{1/2}$  is also included in the optimization inside a  
 290 range of  $[10^\circ, 20^\circ]$ . Figures 8a, 8b, and 8c depict the values of  $t_{BL}$ ,  $\Phi_{1/2}$  and  $R_b$  respectively  
 291 obtained for configuration A, assuming a  $10 \times 10$  grid on the floor of the room. A minimum  
 292 value of  $t_{BL}$  obtained was 890 days at the room corners. The optimal value for  $\Phi_{1/2}$  was near  
 293  $10^\circ$ . This does not change even if we widen the allowed range for  $\Phi_{1/2}$  in the GA and indicates a  
 294 non-directed scenario where a tight beam impinges on the nearby room sidewall and light reaches  
 295 the MN by a diffuse path. For all SN positions considered, the optimal  $R_b$  obtained is  $\cong 10$  kb/s.  
 296 The results for configuration B are shown in Figure 9. In this case, the minimum value of  $t_{BL}$  is  
 297 186 days and is maximized near the sidewalls reaching up to 450 days. Again, the algorithm  
 298 favors beam-widths near  $10^\circ$  while the optimal data rate ranges from 3.6 to 9.4 kb/s.

## 299 5. Conclusions and future directions

300 In this work, we took a deeper look at the potential of optical technologies for WSNs and IoT  
 301 applications, which are relevant for mMTC applications within 5G and beyond networks. We

302 presented a realistic model for describing a hybrid VLC/IR WSN, which included diffuse-light  
303 propagation. We showed that for typical data rates pertinent to most indoor mMTC applications,  
304 the diffuse channel can be effectively considered flat and simply be described by a channel gain.  
305 This allowed us to implement an efficient link budget model that can be used to significantly speed  
306 up computations in system optimizations. To maximize battery life, we used a machine learning  
307 approach based on a GA to optimize MN/SN configurations and showed that substantially  
308 increased SN battery lifetimes are obtained, even for coin-cell battery capacities. We also  
309 investigated scenarios where only the diffuse light contribution was considered and the SN TX  
310 beam-widths were included in the optimization. For data rates envisioned in such applications,  
311 diffuse light propagation can improve the up-link power budget as well as energy efficiency.  
312 This is true for both small and larger room configurations such as those examined in this work.  
313 The optimizations show that when the LOS path is blocked, the diffuse path actually favors  
314 non-directed configurations with narrower beam-widths, where the IR light is aimed at the room's  
315 sidewalls, reaching the MN via single and multiple bounces. Both the proposed model and  
316 the optimization engine are available freely on the web under an open-source license for other  
317 researchers to use and **can form a basis, where GA optimizations can be carried out possibly**  
318 **applying different channel modeling approaches for indoor [31] or even underwater systems [32].**  
319

320 The results obtained in this paper point towards some interesting research directions to  
321 implement VLC/IR WSNs. A key question is whether the SN configuration can be changed  
322 in an adaptive manner. One could envision controlling the IR LED radiation pattern using  
323 micro-electromechanical systems [33] while the direction of transmission could be also controlled  
324 using low-cost servo-motors mounted at the SN. It would also be interesting to develop algorithms  
325 for the real-time optimization of the up-link performance that can converge quickly, to limit  
326 power dissipation during the optimization stage. Another interesting scenario would be to  
327 investigate multi-hop scenarios where SNs, which are far from the MN or their LOS paths might  
328 experience shadowing and blocking, communicate with the MN via other SNs. It is our intention  
329 to investigate some of these research directions as part of our future research.

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