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# Hydrothermally synthesized ZnO-RGO-PPy for water-borne epoxy nanocomposite coating with anticorrosive reinforcement

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\*: Corresponding authors <u>baoji miao@haut.edu.cn</u> (B. Miao), xianhu.liu@zzu.edu.cn (X. Liu) or nanomaterials2000@gmail.com (Z. Guo) Abstract: Waterborne epoxy (WEP) nanocomposite coating with hydrothermal synthesized zinc oxide (ZnO)-reduced graphene oxide (RGO)- polypyrrole (PPy) was prepared and an enhanced corrosion resistance was reported. Experiment results showed that WEP nanocomposite coating with Z8R2P (the mass ratio of ZnO-RGO-PPy of 8:2:1) exhibited the highest value of the impedance at the lowest frequency (such as  $|Z|_{0.01\text{Hz}}$ ), the lowest corrosion current density and the largest value of charge transfer resistance (R<sub>et</sub>). Even after 94 days of immersion, the  $|Z|_{0.01\text{Hz}}$  value of Z8R2P/WEP nanocomposite coating was  $4.45 \times 10^3 \,\Omega \cdot \text{cm}^2$ , pointing out that Z8R2P/WEP coating possessed the long superior anticorrosion performance. Moreover, salt spray experiments with a period of 50 days showed that Z8R2P/WEP coating had the best corrosion protection performance. The characterization and analysis of phase composition and corrosion morphology revealed that the synergistic protection mechanism of Z8R2P/WEP coating was attributed to barrier effects of RGO, chemical passivation of ZnO and accept the released electrons of PPy.

Keywords: Reduced Graphene Oxide; Polypyrrole; Corrosion; Epoxy; Nanocomposites.

#### 1. Introduction

Metals and their alloys have attracted much interests due to their wide applications [1-12] and the easy corrosion has caused serious problems [13-17]. Many methods have been reported to prevent the corrosion [18-20]. Epoxy resin has been widely used in corrosion protection of metal surface due to excellent strong mechanical properties [21-24], corrosion resistance, chemical resistance [25], and

durable adhesion with metal matrix [26-34]. Owing to environmental considerations, waterborne epoxy resin (WEP) has been replacing solvent-borne epoxy resin in anticorrosive coatings fields [35-37]. Surfactants and hydrophilic groups are usually used to prepare WEP emulsion. Residual surfactants and hydrophilic groups in the curing process will lead to the micro-pores and defects in the coating, decrease the water-resistance of the coating, as well as the corrosion resistance [38, 39]. Hence, exploring new strategies and technologies to improve the corrosion protection of WEP coating is urgent.

Alkali metal oxide is usually used in the WEP coating for corrosion resistance on the metal surface. For example, ZnO has good ultraviolet shield effect [40-42], forms dense zinc-iron compounds on the surface between the coating and metal matrix, reduces the penetration rate of corrosive media. For example, Rahman *et al.* added ZnO nanoparticles into epoxy-polyamide matrix. Results revealed that the addition of high loading of nanoparticles decreased the glass transition temperature of the composites and increased the coating resistance against hydrolytic degradation [39]. Moreover, Ramezanzadeh *et al.* reported the effects of nano and micron sized ZnO particles on the hydrolytic degradation and corrosion resistance of an epoxy coating. Results showed that the nano-composites exhibited a greater hydrolytic resistance compared to micro-composite [43].

Graphene and its derivatives have excellent barrier reinforcements for epoxy coatings due to its high specific surface area and excellent impermeability [44-48]. However, graphene and its derivatives exhibit a close-packed layered structure owing to thier intrinsic van der Waals' interaction and the synthesis procedure consisting of a vacuum filtration, then leading to poor dispersion in epoxy coating [49-54]. To preclude the aggregation of GO nanosheets and to achieve a homogeneous dispersion and enhanced compatibility with epoxy, decorating sheets with inorganic nanoparticles is a facile and efficient approach [50, 55-58]. Moreover, the loading of nanoparticles on the GO surfaces increased

the layer spacing by separating nanosheets efficiently. For example, Pourhashem et al. used tetraethyl orthosilicate to decorate the surface of GO nanosheets by SiO2 nanospheres via a facile method. Then, embedding the well-distributed SiO<sub>2</sub>-GO nanohybrids into epoxy coating remarkably enhanced the corrosion resistance compared to GO nanosheets [59]. Yu et al. synthesized TiO2-GO sheet hybrids [60] and Al<sub>2</sub>O<sub>3</sub>-GO [61] with the help of 3-aminopropyltriethoxysilane, respectively. Embedding the nanosheets into epoxy resin improved the corrosion resistance. In addition, polypyrrole (PPy) has recently been used in the field of anticorrosion coatings due to excellent conductivity and flexibility [62]. Ding et al. [63] prepared PPy nanowires/graphene composites through an in-situ polymerization, and improved the corrosion resistance of WEP coatings. Results showed that a high barrier performance of graphene and passivation effect of PPy were conducive to corrosion protection. Qiu et al. [50] reported the synergistic effect of PPy-intercalated graphene for enhanced corrosion protection of WEP coatings. Zhu et al. [36] prepared the GO-PPy composites through an in-situ polymerization to significantly improve the corrosion resistance of WEP coatings in 3.5% NaCl solution. To the best of our knowledge, using ternary composites ZnO-RGO-PPy to improve the corrosion resistance of WEP coating has not yet been reported.

Herein, the synergistic effect of ZnO-RGO-PPy as a new nanofiller in WEP coating was investigated. ZnO-RGO composites were hydrothermally prepared by metal oxide and GO as precursors. Then Py monomer was added into the synthesized ZnO-RGO as precursors to synthesize ZnO-RGO-PPy composites. The corrosion resistance of ZnO-RGO-PPy/WEP coating were measured by electrochemical impedance spectroscopy (EIS) and salt spray test, and the protective mechanism was revealed by the phase composition and morphology.

# 2. Experimental

#### 2.1. Materials

Zn(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, KOH, NaCl and ethanol were purchased from Sinopharm Chemical Reagent Co., Ltd. All aqueous solutions were used with deionized water. Waterborne two-component epoxy/amine coating system and corresponding water-borne curing agent were supplied by the epoxy resin department of Baling Petrochemical Co., Ltd. GO were synthesized according to our previous report [5]. The dimension of the mild steel specimens was  $120 \times 50 \times 0.28 \text{ mm}^3$ , and these chemical compositions (wt%) were:  $\leq 0.22 \text{ C}$ ,  $\leq 0.045 \text{ P}$ ,  $\leq 0.70 \text{ Mn}$ ,  $\leq 0.34 \text{ Si}$ ,  $\leq 0.05 \text{ S}$  and balance Fe. Prior to coating the steel specimen, mild steel specimens were grinded with 100, 400, 800 grit SiC sandpapers to remove oxide layer, respectively. Then, these specimens were cleaned using ethanol solution.

#### 2.2. Synthesis of ZnO-RGO-PPy

ZnO-RGO-PPy were synthesized by two-step modification. ZnO-RGO was prepared by the hydrothermal synthesis according to our previous report [64]. Then, 0.1077 g ZnO-RGO was added to a breaker containing 100 mL deionized water. The dissolved solution was placed in the cell pulverizer for ultrasonic treatment to obtain a uniformly dispersed suspension system. Subsequently, 0.5 g of sodium dodecylbenzene sulfonate (C<sub>18</sub>H<sub>29</sub>NaSO<sub>3</sub>) was added to the suspension with continuous stirring in an ice bath. At the same time, 14.4 mmol Py monomer was added into a breaker of 20 mL ethanol solution. After Py was completely dispersed, the solution was translated into the above suspension system, and sonicated for 30 min to absorb Py monomer on the surface of ZnO\_RGO. Then, 30 mL of 0.48 M (NH<sub>4</sub>)<sub>2</sub>S<sub>2</sub>O<sub>8</sub> was added to the above suspension and stirred continuously for 24 h in an ice bath. The flocs after hydrothermal reaction were filtered and washed several times with the

mixture solution of deionized water and ethanol (1:1). Finally, the ultimate flocs were placed in a vacuum drying oven and the temperature was maintained at 60 °C for 24 h, the obtained black powder was ZnO-RGO-PPy. Since the mass ratio among ZnO, PPy and GO was 2:2:1, the obtained ZnO-RGO-PPy was recorded as Z2R2P. For comparison, the composites with the mass ratio of ZnO-RGO-PPy of 8:2:1 and 2:6:3 were prepared by the same method and recorded as Z8R2P and Z2R6P3.

#### 2.3. Preparation of ZnO-RGO-PPy/WEP coatings

Fig. 1 represents the schematic diagram of the preparation process of ZnO-RGO-PPy/WEP composite coatings. Typically, 0.504 g of Z8R2P was added to 10 mL deionized water and ultrasonic treatment for 30 min to obtain a uniformly dispersed composite system. Then, 5.2 g of aqueous curing agent was added to the above suspension and stirred magnetically for 30 min. After that, 20 g WEP emulsion was added to the above mixed solution and continued stirring. Then the mixture solution was placed in a vacuum drying oven for 30 min for degassing treatment to eliminate bubbles in the mixture. To maintain the same thickness of the coatings, the wire rod of 80 μm was used to coat the pretreated mild steels and placed the coated steels at room temperature for 24 h. After that, all samples were cured in an electric blow-drying oven for 60, 90 and 120 °C for 2 h, respectively. Finally, the obtained coating was named as Z8R2P/WEP. For comparison, WEP, Z2R2P/WEP, and Z2R6P3/WEP coatings were prepared by the similar methods.

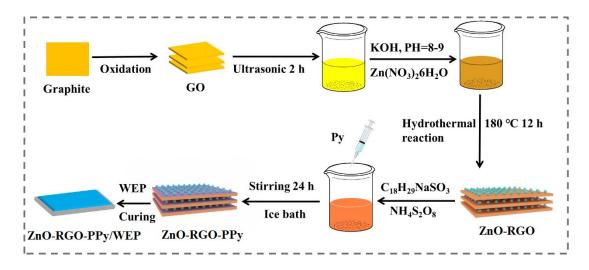


Fig. 1. Schematic diagram of the preparation process of ZnO-RGO-PPy/WEP composite coatings.

#### 2.4. Characterization

The morphologies of the GO, Z2R2P, Z8R2P, Z2R6P3 and these corresponding composite coatings were characterized by field emission scanning electron microscope (FESEM, an Inspect F50 scanning electron microscope). The structure characteristics of GO, Z2R2P, Z8R2P, Z2R6P3 and these corresponding composite coatings were characterized by X-ray diffraction patterns (XRD, Bruker D8 Advance) with Cu K $\alpha$  radiation at 40 mA and 40 kV by a scanning rate of 1° min<sup>-1</sup> 14. The Fourier transform infrared (FT-IR) spectra of GO, Z2R2P, Z8R2P and Z2R6P3 were recorded using the Prestige-21 with the range from 400 to 4000 cm<sup>-1</sup>. Raman spectra of GO, Z2R2P, Z8R2P and Z2R6P3 were obtained from a Nano-finder 30 confocal Raman Microscope (Lab RAM HR Evolution, French) with the range from 50 cm<sup>-1</sup> to 3000 cm<sup>-1</sup> via a He-Ne laser beam with a wavelength of 532 nm.

The corrosion resistance performances of the composite coatings were tested using an electrochemical impedance spectroscopy (EIS) by an electrochemical workstation (RST5200F, Zhengzhou Shiruisi Instrument Technology Co., Ltd.) with a conventional three-electrode configuration including the work electrode, platinum counter electrode and reference electrode

(Ag/AgCl), and the corrosive electrolyte was the 3.5 wt% NaCl solution. A geometrical area of 12 cm<sup>2</sup> was used to the electrolytic solution for the work electrode. A scan rate of 1 mV s<sup>-1</sup> was carried on the electrochemical workstation to obtain the polarization plots. All EIS measures were run in the frequencies range from 105 to 10-2 Hz with an amplitude of 5 mV. EIS spectra were fitted using a ZSimpWin software to obtain the equivalent circuit and the key electrochemical parameters. Salt spray test measurements of the composite coatings were conducted in a salt spray chamber according to GB 1771-2007 standards, and the concentration of NaCl solutions was 5 wt%.

#### 3. Results and discussion

#### 3.1. Structure and morphologies of Z2R2P, Z8R2P and Z2R6P3

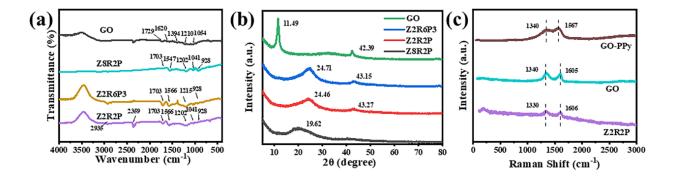


Fig. 2. FT-IR, XRD and Raman spectrums of GO, Z2R2P, Z8R2P and Z2R6P3.

FT-IR is used to confirm and track the formation of chemical bonds during the modification process. Fig. 2(a) shows the FT-IR spectra of GO, Z2R2P, Z8R2P and Z2R6P3. The peaks at 1620 and 1729 cm<sup>-1</sup> in the spectrum of GO were assigned to the stretching vibration of C=O bond and the stretching vibration of C=C bond, respectively. Other peaks at 1394, 1210 and 1054 cm<sup>-1</sup> were assigned to the deformation vibration of C-O-H bond and the stretching vibration of C-H and C-O bonds.

Therefore, these results indicate that graphite surface is endowed with oxygen functional groups in the process of oxide to GO. After the hydrothermal reaction between GO and Zn (NO<sub>3</sub>)<sub>2</sub>, the containing oxygen functional groups on the surface of GO gradually disappeared, New absorption peak appeared, for example, C=C (1729 cm<sup>-1</sup>), C-O-H (1394 cm<sup>-1</sup>) and C-O (1054 cm<sup>-1</sup>), etc. The peaks at 1547, 1202 and 1041 cm<sup>-1</sup> in the spectrum of Z8R2P were assigned to the vibration of pyrrole ring and the tensile vibration of antisymmetric C-N and C-H bonds [65, 66], respectively. In addition, the peaks at 900, and 928 cm<sup>-1</sup> were related to the doped PPy [67] and ZnO [68], respectively. Altering the mass ratio of ZnO, GO and PPy, the peak locations in the spectra of Z2R2P and Z8R2P changed slightly compared to that of Z2R6P3, indicating that Z2R2P, Z8R2P and Z2R6P3 were successfully synthesized.

Fig. 2(b) shows the XRD patterns of GO, Z2R2P, Z8R2P and Z2R6P3. The characteristic peak of GO appeared at  $2\theta = 11.6^{\circ}$ , corresponding to the crystal plane (001). Owing to the doping of ZnO and PPy, the original characteristic peak that belonged to GO disappeared, and the new characteristic peaks appeared at  $2\theta = 20^{\circ}$ ,  $23^{\circ}$  and  $24^{\circ}$  for Z2R2P, Z8R2P and Z2R6P3, respectively. The above results were consistent with the characteristic peak of ZnO\_RGO\_PPy [69], revealing that GO had formed this disordered accumulation in the synthesis of ternary composites. Raman spectra were used to analyze the structure of composites, especially for carbon materials. The Raman spectra of GO, GO-PPy and ZnO\_RGO\_PPy are shown in Fig. 2(c). According to the calculation of energy band, the values of *ID/IG* belonged to GO, PPy, and Z8R2P were 1.84, 1.39 and 2.57, respectively. Therefore, this indicated that the disorder degree of GO was improved greatly owing to the doping of ZnO and PPy.

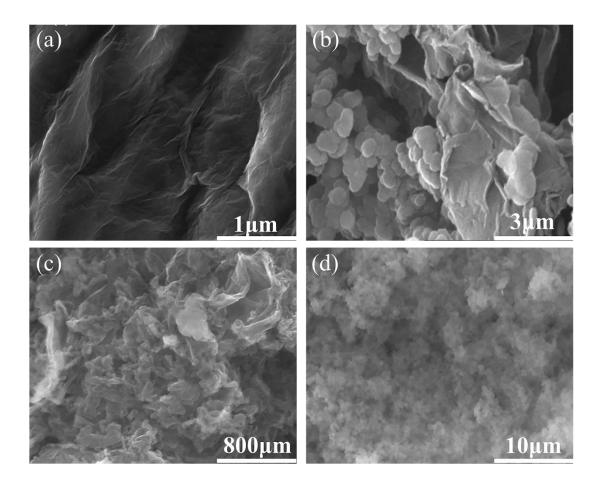


Fig. 3. The FESEM morphologies of GO<sub>2</sub> Z2R2P<sub>2</sub> Z8R2P and Z2R6P3.

FESEM is used to characterize the morphology and microstructure of the prepared composites. Fig. 3 shows the FESEM morphologies of GO, Z2R2P, Z8R2P and Z2R6P3. According to Fig. 3(a), GO displays a typical wrinkle structure. It was worth noting that the three proportions of ZnO\_RGO\_PPy had still wrinkle structure, which indicated that the lamellar structure of GO was not damaged during the modification process. The relatively rougher surfaces of these three composites (Z2R2P, Z8R2P and Z2R6P3) as depicted in Fig. 3(b-d) indicated that PPy had polymerized and formed a thin film on the nanosheets. Moreover, the granular ZnO on the surface of Z8R2P appeared more obviously compared to the other two ZnO\_RGO\_PPy, which was attributed to the high content of ZnO for Z8R2P composites. 3.2. Mechanical properties of the composite coatings

The impact resistance properties of WEP, Z2R2P/WEP, Z8R2P and Z2R6P3/WEP coatings were tested according to GB/T 1732-2020. The impact height of the drop hammer in this experiment was set at 50 cm. No obvious cracks, spalling and other defects were found in all coatings according to the observation with the aid of a magnifying glass. This indicated that all composite coatings had excellent impact resistance property and met the requirements of the practical application. The adhesion property of WEP, Z2R2P/WEP, Z8R2P and Z2R6P3/WEP coatings was tested according to GB/T 1720-2020. The adhesion of all composite coatings showed as grade 1, indicating excellent interfacial adhesion property between coating and substrate.

The flexibility of WEP, Z2R2P/WEP, Z8R2P and Z2R6P3/WEP coatings was tested according to GB/T 1731-2020. These composite coatings were checked carefully with a quadruple magnifying glass after the test was complete. No damages such as reticulation, crack and peeling were found according to the observation result, indicating excellent flexibility property of the composite coatings.

#### 3.3. Corrosion resistance property of the composite coatings

EIS measurements are used to evaluate the corrosion protection property of the composite coatings during immersion in 3.5 wt% NaCl solution. Fig. 4 shows the Nyquist plots of the WEP, Z2R2P/WEP, Z8R2P/WEP and Z2R6P3/WEP coatings after being immersed in 3.5 wt% NaCl for 24 h, 120 h, 240 h and 94 d. In the Nyquist plots, all plots presented the similar shape, which were semicircle but with different diameters. The flattened capacitive semicircle was an indicative of frequency dispersion owing to the defects in the WEP coatings [69-71]. The capacitive semicircle of

the Nyquist plots had been gradually decreased for all the prepared coatings by prolonging the immersion time, indicating that the corrosion resistance of the coatings has been gradually deteriorated. At the early period of immersion (24 h), the sequence of the capacitive characteristic diameter for the composite coating was Z8R2P/WEP > Z2R2P/WEP > WEP > Z2R6P3/WEP, indicating that the Z8R2P/WEP coating had the best corrosion protection. When the immersion time was up to 120 h, the sequence of the capacitive characteristic diameters for the composite coatings had not changed compared to that at 24 h immersion time. With prolonging the immersion time to 240 h, the above sequence had no change, and Z8R2P/WEP still exhibited the largest capacitive characteristic compared to other coatings. After 94 days of immersion, the diameter of flattened capacitive semicircle in Z8R2P/WEP coating still exhibited the largest while that of other coatings had an obvious decrease. This indicated that Z8R2P/WEP coating had the best corrosion protection performance through the whole immersion period of 94 d.

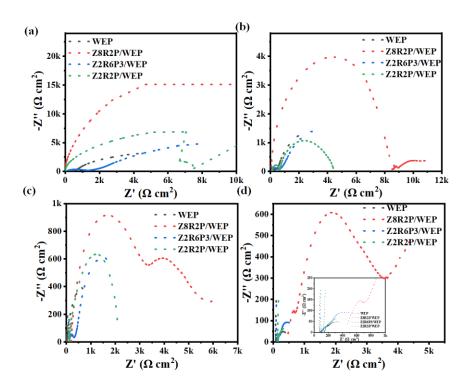


Fig. 4. The Nyquist plots of the WEP, Z8R2P/WEP, Z2R6P3/WEP and Z2R2P/WEP coatings after immersed in 3.5 wt% NaCl for (a) 24 h, (b) 120 h, (c) 240 h and (d) 94 d.

Fig.5 shows the Bode modulus plots of the WEP, Z2R2P/WEP, Z8R2P/WEP and Z2R6P3/WEP coatings after immersed in 3.5 wt% NaCl for 24 h, 120 h, 240 h and 94 d. The impedance at the lowest frequency  $(Z_{0.01Hz})$  reflects the barrier ability of the coatings [72-74]. At the early stage of immersion (24 h), the Z<sub>0.01Hz</sub> values of WEP and Z2R6P3/WEP coatings were 9.91  $\times$  10<sup>3</sup> and 9.20  $\times$  10<sup>3</sup>  $\Omega$  cm<sup>2</sup>, respectively. Surprisingly, the Z<sub>0.01Hz</sub> values of Z8R2P/WEP and Z2R2P/WEP coatings were up to 1.17  $\times$  10<sup>5</sup> and 9.21  $\times$  10<sup>4</sup>  $\Omega$  cm<sup>2</sup>, which was increased by two orders of magnitude. This revealed that the coating could impede the current flow from anodic to cathodic. However, the  $Z_{0.01Hz}$  values of WEP, Z2R6P3/WEP and Z2R2P/WEP coatings sharply dropped to less than  $5 \times 10^3 \,\Omega \text{ cm}^2$  after 120 h of immersion. This indicated the rapid deterioration of barrier for these composite coatings and WEP coating since the aggressive species penetrated through the coating matrix to the mild steel surface. As expected, the  $Z_{0.01Hz}$  value of Z8R2P/WEP coating was maintained at 10<sup>4</sup>  $\Omega$  cm<sup>2</sup> after 120 h of immersion, which was significantly higher compared to other coatings. Moreover, with prolonging the immersion time to 94 d, the  $|Z|_{0.01\text{Hz}}$  value of Z8R2P/WEP coating was  $4.45 \times 10^3 \,\Omega \cdot \text{cm}^2$ , which had no obvious decrease than that after 240 h of immersion. While the  $|Z|_{0.01\text{Hz}}$  values of other coatings were less than  $0.5 \times 10^3 \,\Omega \cdot \text{cm}^2$ , which were far lower than that of Z8R2P/WEP coating. This indicated that Z8R2P/WEP coating formed tortuous diffusion pathways for aggressive species. Regardless of the immersion times, Z8R2P/WEP coating showed the largest  $Z_{0.01Hz}$  values while the neat WEP coating had the lowest  $Z_{0.01Hz}$  values, there was a difference of more than 6 times of magnitude between them. This indicates that Z8R2P/WEP had the best anticorrosion property and the neat WEP coating

had the worst anticorrosion property. This phenomenon was in an agreement with the Nyquist diagrams during the whole immersion periods.

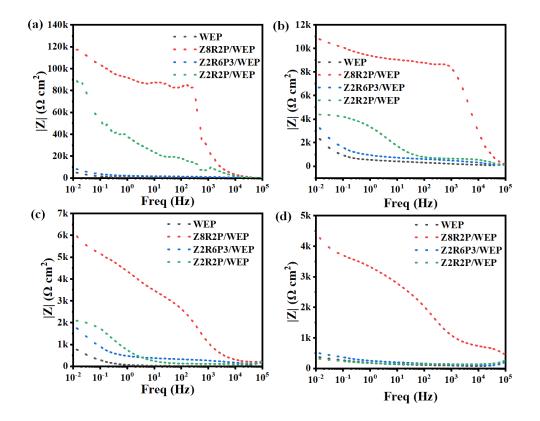


Fig. 5. The Bode modulus plots of the WEP、Z2R2P/WEP、Z8R2P/WEP and Z2R6P3/WEP coatings after immersed in 3.5 wt% NaCl for (a) 24 h, (b) 120 h, (c) 240 h and (d) 94 d.

In the Bode phase plots (Fig. 6), the low frequency constant reveals the corrosion response of the mild steel, the high frequency constant reveals the capacitance and defects of the coatings. Thus, a coating with two-time constants in Bode phase spectrum indicates that the aggressive species has contacted the surface of the mild steel during immersion periods. At the beginning of immersion (24 h), the time constant of the neat WEP appeared at the low frequency while the time constant of composite coating appeared at the high frequency. Due to the corrosion response at the low frequency, the corrosion reaction of WEP coating had begun at the initial stage. While Z2R2P/WEP and

Z8R2P/WEP coatings appeared at high frequency region, its phase angle was close to 90 °. This indicated that the Z2R2P/WEP and Z8R2P/WEP coatings prevented the corrosive media from diffusing through the coating and entering the mild steel surface.

In addition, compared with neat WEP and the Z2R6P3/WEP coatings, Z2R2P/WEP and Z8R2P/WEP coatings had the higher  $\varphi_{105Hz}$  value, indicating that these composite coatings had a better barrier ability. The time constant of Z2R2P/WEP coating moved to the low frequency direction, which indicated that the corrosion occurred after 120 h of immersion. With the immersion prolonged to 240 h, the time constant of Z2R2P /WEP coating further moved to the low frequency direction while the time constant of Z8R2P/WEP coating still appeared at the high frequency and the capacitive response of the coatings existed. While WEP coating showed the second time constant, indicating that the corrosive mediums had passed through the coating and entered the interface between metal and coating at this stage. Moreover, after 94 d of immersion, higher phase angle at high frequency range for Z8R2P/WEP coating was obtained compared to other coatings. These results indicated that Z8R2P/WEP coating had the best corrosion resistance property after the long-time immersion. The abnormal phenomenon in the Bode diagram is a corrosion system with multiple time constants. The time constant in the high frequency region corresponds to the capacitive response of the coating, and the time constant in the middle and low frequency region corresponds to the corrosion response of the substrate. As shown in Fig. 6 in the manuscript, the time constants for different immersion time of Z8R2P/WEP coating appear in the high frequency region, and the capacitive response of the coating shows that the coating has good barrier properties.

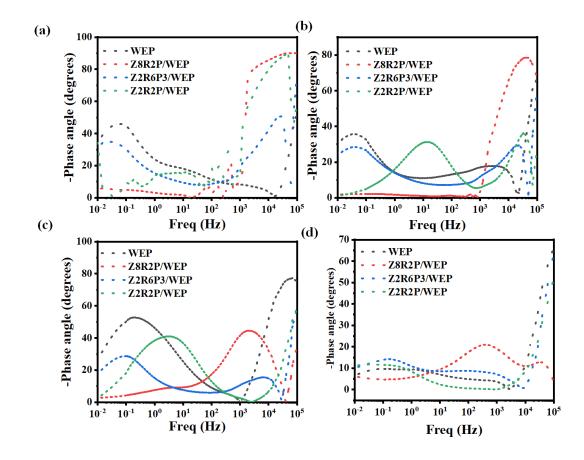


Fig. 6. The Bode phases plots of the WEP、Z2R2P/WEP、Z8R2P/WEP and Z2R6P3/WEP coatings after immersed in 3.5 wt% NaCl for (a)24 h, (b)120 h, (c)240 h and (d) 94 d.

Tafel plots and corresponding polarization parameters of WEP, Z2R2P/WEP, Z2R6P3/WEP and Z8R2P/WEP coatings are shown in Fig. 7 and Table S1. Generally, the lower *i*<sub>corr</sub> the material, the lower trend of corrosion and oxidation. At the early stage of immersion, the *i*<sub>corr</sub> values of WEP and Z2R6P3/WEP were  $9.426 \times 10^{-8}$  and  $4.817 \times 10^{-8}$  A/cm<sup>2</sup> while that of Z8R2P/WEP was up to  $7.750 \times 10^{-9}$  A/cm<sup>2</sup>, which was one order of magnitude lower than WEP coating. With the immersion being prolonged to 120 h, the *i*<sub>corr</sub> values of WEP<sub>5</sub> Z2R2P/WEP and Z2R6P3/WEP coatings were increased by an order of magnitude after 120 h of immersion. While Z8R2P/WEP coating had no obvious change at this immersion stage, with the time being prolonged to 240 h, the *i*<sub>corr</sub> value of Z8R2P/WEP coating was  $1.583 \times 10^{-7}$  A/cm<sup>2</sup>, which was not significantly improved compared with the initial immersion

period. This indicated that Z8R2P could effectively impede the current flow from anodic to cathodic, thus showed the best corrosion protection property. In addition, the corrosion rate (d) of WEP, Z2R2P/WEP and Z2R6P3/WEP coatings were  $1.12 \times 10^{-3}$ ,  $1.99 \times 10^{-4}$  and  $5.43 \times 10^{-3}$  mm/year, respectively. However, the corrosion rate of Z8R2P/WEP coating was  $9.12 \times 10^{-5}$  mm/year, which was two order of magnitude lower compared with WEP and Z2R6P3/WEP coatings, and one order of magnitude lower than Z2R2P/WEP coating, respectively. Moreover, after 94 d of immersion, Z8R2P/WEP coating exhibited smaller current density and greater potential compared to other coatings as shown in Fig. 7(d). This indicated that Z8R2P/WEP coating had the long-term anticorrosion property, which was attributed to the fact that more Zn<sup>2+</sup> could lead to a more dense passive film on the surface of the substrate.

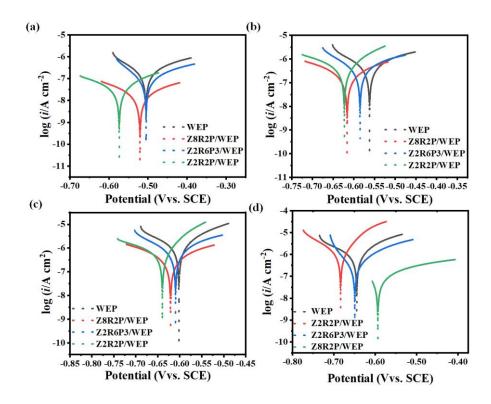


Fig. 7. The Tafel plots of the WEP, Z2R2P/WEP, Z8R2P/WEP and Z2R6P3/WEP coatings after

immersed in 3.5 wt% NaCl for (a) 24 h, (b) 120 h, (c) 240 h and (d) 94 d.

ZSimpWin was used to simulate equivalent circuit based on the EIS data of all coatings during the immersion period. In the fitting process, the appropriate equivalent model was selected based on the small Chi-Square value, which was consistent with the immersion period. The fitted equivalent circuit models and corresponding electrochemical parameters are shown in Fig. S1 and Table S2. The corresponding electrochemical parameter mainly include R<sub>s</sub>, R<sub>e</sub>, R<sub>ct</sub>, Cc and C<sub>dl</sub>, which represent the solution resistance between calomel reference electrode and working electrode, composite coating capacitance and the double electric layer. Combined with the data analysis of electrochemical impedance, the model as shown in Fig. S1(a) is suitable for all coating during 120 h of immersion, and the model as shown in Fig. S2(b) is suitable for all coatings after 240 h of immersion. All the Chi-Square values for the fitting results were little, which showed that the fitting results of the equivalent circuit were reliable.

At the early stage of immersion (24 h), the R<sub>ct</sub> values of WEP and Z2R6P3/WEP coatings were  $3.93 \times 10^3$  and  $6.02 \times 10^3 \ \Omega \cdot \text{cm}^2$  while that of Z8R2P/WEP coating was  $9.02 \times 10^3 \ \Omega \cdot \text{cm}^2$ , which was increased by 23 times of magnitudes than WEP coating, and 11.6 times of magnitudes than Z2R6P3/WEP coating. This depicted that Z8R2P/WEP coating had the best physical barrier capability after 24 h of immersion. After 240 h of immersion, the R<sub>ct</sub> values of WEP, Z2R2P/WEP, Z2R6P3/WEP and Z8R2P/WEP coatings had a significant decrease while that of Z8R2P/WEP coating still was 9.10  $\times 10^3 \ \Omega \cdot \text{cm}^2$ , which was improved by 5.4 times of magnitudes than WEP coating. With increasing the immersion time to 240 h, the aggressive corrosive media have entered the interface between the metal substrate and the coating. Then the equivalent circuit model as shown in Fig. S1(b) was suitable for all the composite coatings at this immersion stage. The R<sub>s</sub>, R<sub>c</sub>, and R<sub>ct</sub> values of Z8R2P/WEP coating were

 $0.25 \times 10^3$ ,  $2.49 \times 10^3$  and  $2.16 \times 10^3 \ \Omega \cdot cm^2$ , which were much higher than that of other coatings. Regardless of immersion time, Z8R2P/WEP coating had the largest R<sub>ct</sub> value compared to WEP, Z2R2P/WEP and Z2R6P3/WEP coatings, which indicated that it had the best corrosion protection property.

## 3.4. Salt spray test of the composite coatings

Fig. 8 shows the digital photos of WEP, Z2R2P/WEP, Z2R6P3/WEP and Z8R2P/WEP coatings after salt spray test for 1, 10, 30 and 50 days. After one day of salt spray test, slight rust appeared at the cross scratches on the surface of all the specimens. After 10 days of salt spray test, rust appeared in most areas of WEP and Z2R6P3/WEP. Then some rust occurred around the scratches center of Z2R2P/WEP coating. However, for Z8R2P/WEP coating, slight rust still appeared around the scratches. After 30 days of salt spray test, WEP, Z2R2P/WEP and Z2R6P3/WEP coatings were peeled off, and deep rust appeared, especially for WEP coating. Meanwhile, Z8R2P/WEP coating had the wider and deeper rust compared to that after 10 days of test but retained the relatively complete coating. After 50 days of salt spray test, many cracks appeared in the WEP coating, and the metal substrate even leaked in some areas, which indicated that WEP coating had lost the corrosion protection ability. Z2R2P/WEP coating was peeled off around the center of scratches, while the coating below was still relatively complete. The whole surface of Z2R6P3/WEP coating was covered by massive rusts and the areas of peel off were increased. While Z8R2P/WEP coating showed relatively complete, some slight rusts appeared in local areas except for the rust around the scratches. Regardless of salt spray test time, Z8R2P/WEP coating had the best integrity of coating compared with other coatings, indicating that Z8R2P/WEP coating had the best corrosion protection performance.

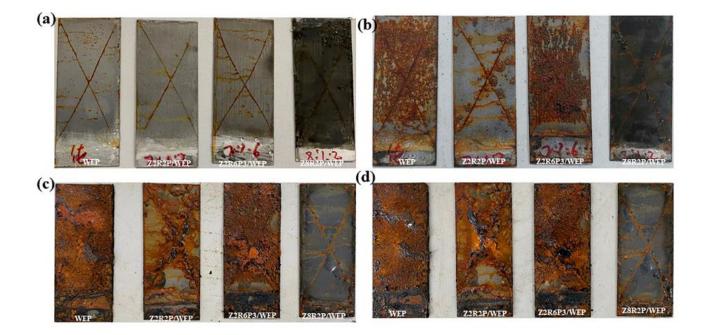


Fig. 8. Digital photos of WEP, Z2R2P/WEP, Z2R6P3/WEP and Z8R2P/WEP coatings after salt spray test for (a)1, (b)10, (c)30 and (d)50 days.

#### 3.5. Corrosion products

To reveal the corrosion protective mechanism of ZnO-RGO-PPy/WEP composite coating, the corrosion products were characterized. In this study, the corrosive products on the mild steel beneath these composites were characterized by FESEM and XRD. The XRD patterns of WEP and Z8R2P/WEP coatings after 10-day immersion in 3.5 wt% NaCl solution are shown in Fig. S2. The patterns of WEP coating appeared at  $2\theta$  =45°, 65° and 82.5°, which mainly came from the Fe element contained in the metal substrate. However, the patterns of Z8R2P/WEP coating appeared at  $2\theta$  =30° and 65°, revealing that the rust layers were composed of Fe<sub>2</sub>O<sub>3</sub> and FeOOH. This indicated that Z8R2P could promote the passive coating on the surface of metal substrate. Fig. S3 shows the FESEM morphologies for WEP and Z8R2P/WEP coatings. WEP coating as shown in Fig. S3(a) shows an obvious delamination. The traces left by grinding and polishing were still clearly observed, then

corrosive media entered the metal surface along these traces. For Z8R2P/WEP coating as shown in Fig. S3(b), the surface appeared excellent distributed nanosheets, which formed a dense barrier layer and thus could effectively prevent corrosive media from entering the metal surface, thus improved the barrier ability of the coating.

#### 3.6. Corrosion protection mechanism

The schematic diagram of corrosion protection mechanism of ZnO-RGO-PPy/WEP composite coating is shown in Fig. 9. During the long-time immersion in 3.5 wt% NaCl solution, corrosive media gradually penetrated into the interior of the coating and reached the interface between the metal substrate and coating, then a series of redox reactions were induced on the metal surface. This destroyed the structure and properties of metal substrate, leading to a gradual loss of its basic properties. As a physical barrier layer, WEP coating protected the metal substrate from corrosive media entering interface between the metal surface and coating. However, with the extension of immersion time, corrosive media gradually permeated through the coating and diffused into the surface of metal substrate, thus inducing the corrosion reaction. The nanosheets contained in Z8R2P were evenly dispersed into the coating system, improved the physical barrier ability of the composite coating owing to the more tortuous path of corrosive media. In addition, ZnO contained in Z8R2P dissociated more Zn<sup>2+</sup> ions, and formed a dense passive film on the metal surface, which effectively prevented the further diffusion of media into the metal surface. This might be the reason why Z8R2P/WEP coating showed the best corrosion resistance property. Moreover, PPy contained in Z8R2P accepted the released electrons from the dissolution of the metal, which was conducive to the formation of passive film

composed of Fe<sub>2</sub>O<sub>3</sub> on the metal surface. Therefore, excellent corrosion resistance of Z8R2P/WEP coating was mainly due to the synergistic effect of RGO, ZnO and PPy.

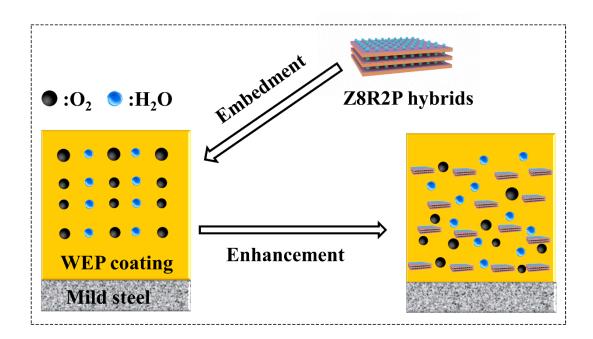


Fig. 9. Schematic representation of protective mechanism of ZnO-RGO-PPy/WEP composite coating.

# 4. Conclusion

In conclusion, the nanohybrids of Z2R2P, Z2R6P3 and Z8R2P were prepared successfully through hydrothermal treatment, as confirmed by the FT-IR, XRD, Raman and FESEM. The corrosion resistance performance of WEP coatings without and with Z2R2P, Z2R6P3 and Z8R2P on mild steels was confirmed by Tafel curves, EIS and salt spray measures. In regards of less immersion period, the composite coating with Z8R2P exhibited the highest value of  $|Z|_{0.01\text{Hz}}$ , the lowest corrosion current density and the largest value of  $R_{ct}$ . Even for 94 days of immersion period, the  $|Z|_{0.01\text{Hz}}$  value of Z8R2P/WEP coating was  $4.45 \times 10^3 \,\Omega \cdot \text{cm}^2$ . It proved that Z8R2P/WEP possessed the long superior

anticorrosive ability. The mechanism of synergistic protection was attributed to the barrier effects of RGO, chemical passivation of ZnO and acceptance of the released electrons by PPy. Our study reveals that this environment friendly ZnO-RGO-PPy can be applied not only in the field of corrosion resistance but also in other industry areas, such as supercapacitor [75-77], conductor [78-81], sensors [82-84], and electromagnetic interference (EMI) shielding [85-87].

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# Declarations

Conflict of interest the authors declare no competing interests.

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